

Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15th MALAYSIA GAMES

Master-Thesis

A thesis submitted in partial fulfillment
of the requirements for the degree of

Master of Engineering in Membrane Structures (M.Eng.)

submitted to

Anhalt University of Applied Sciences

Faculty of Architecture,
Facility Management and Geo Information

by

Siew Moi, Tan

22nd January 1962, Batu Pahat, Malaysia

Matrikel number : 4048307

Submission date: 18 August 2012

First Tutor: Prof. Robert Off

Second Tutor:



Statement

I hereby declare that the work presented in this Master thesis, entitled "Tensile Structure for Indera Mahkota Aquatic Center, Kuantan, 15th MALAYSIA GAMES" , is entirely my own and that I did not use any sources or auxiliary means other than those referenced.

Singapore, 18 August 2012



Tan Siew Moi



CONTENTS

1. INTRODUCTION	5 - 6	8.4 LOADING AND STATICAL ANALYSIS	
1.1 THE REPORT		8.5 LOCAL DESIGN CHECK	
1.2 MALAYSIA		8.6 BIAXIAL TEXT	
1.3 MALAYSIA GAMES - SUKMA		8.7 CUTTING PATTERN	
1.4 PROJECT AND SITE		8.8 SUMMARY OF DETAILS	
2. ARCHITECTURE CONCEPT & DESIGN DEVELOPMENT	7 - 15	9. STEEL ERECTION	48 - 49
2.1 ARCHITECT'S INTENT		9.1 LIFTING CHECK	
2.2 DESIGN DEVELOPMENT		9.2 ERECTION SEQUENCE	
2.3 FINAL DESIGN CONCEPT		10. MEMBRANE INSTALLTION	49 - 50
3. PROJECT ORGANISATION	16 - 17	10.1 MEMBRANE HANDLING	
3.1 FLOW CHART OF PROJECT EXECUTION		10.2 MEMBRANE TENSIONING	
3.2 GEOGRAPHICAL LOCATION OF PROJECT OFFICE		10.3 ERECTION SEQUENCE	
4. GENERAL INFORMATION	18 - 19	11. APPENDIX	51
4.1 PROJECT BRIEF		11.1 WORK PROGRAMME	52 - 53
4.2 REFERENCE DOCUMENT		11.2 ENGINEERING DRAWINGS	54 - 72
4.3 UNIT		11.3 ERECTION SEQUENCE	73 - 80
4.4 DESIGN CODE AND STANDARD		11.4 PHOTO IMAGES OF STEEL WORK	81 - 87
4.5 COORDINATES SYSTEM		11.5 PHOTOS IMAGES OF FABRIC WORK	88 - 94
4.6 MATERIAL		11.6 PHOTO IMAGES OF COMPARISON BEFORE & AFTER ERECTION	95 - 97
4.7 METHOD OF ANALYSIS		11.7 AERIAL VIEW PHASE 1 COMPLETION	98 -99
5. STRUCTURAL SYSTEM	20	11.8 AERIAL VIEW PHASE 1 COMPLETION - IMPRESSION	100 - 101
6. LOADING ASSUMPTION	21 - 23	11.9 NEWS PAPER ARTICLES BEFORE THE GAMES	102 - 103
6.1 SELF WEIGHT		11.10 PHOTO IMAGES DURING THE GAMES	104 - 105
6.2 DEAD LOAD OF CATWALK		11.11 BIAXIAL TEST REPORT	106 - 113
6.3 PRESTRESS LOAD		11.12 DESIGN CALCULATION	114 - 153
6.4 IMPOSED LIVE LOAD			
6.5 WIND LOAD			
7. STEEL ANALYSIS AND DESIGN	24 - 34		
7.1 DESIGN METHOD			
7.2 DESIGN MODEL			
7.3 BASIC LOAD CASES & LOAD COMBINATION			
7.4 BOUNDARY CONDITION			
7.5 DESIGN OF STEEL MEMBER			
7.6 LOCAL DESIGN CHECK			
7.7 SUMMARY OF CONNECTION DETAILS			
8. MEMBRANE ANALYSIS AND DESIGN	35 - 47		
8.1 GENERAL INFORMATION			
8.2 FORM FINDING			
8.3 CONTOUR			



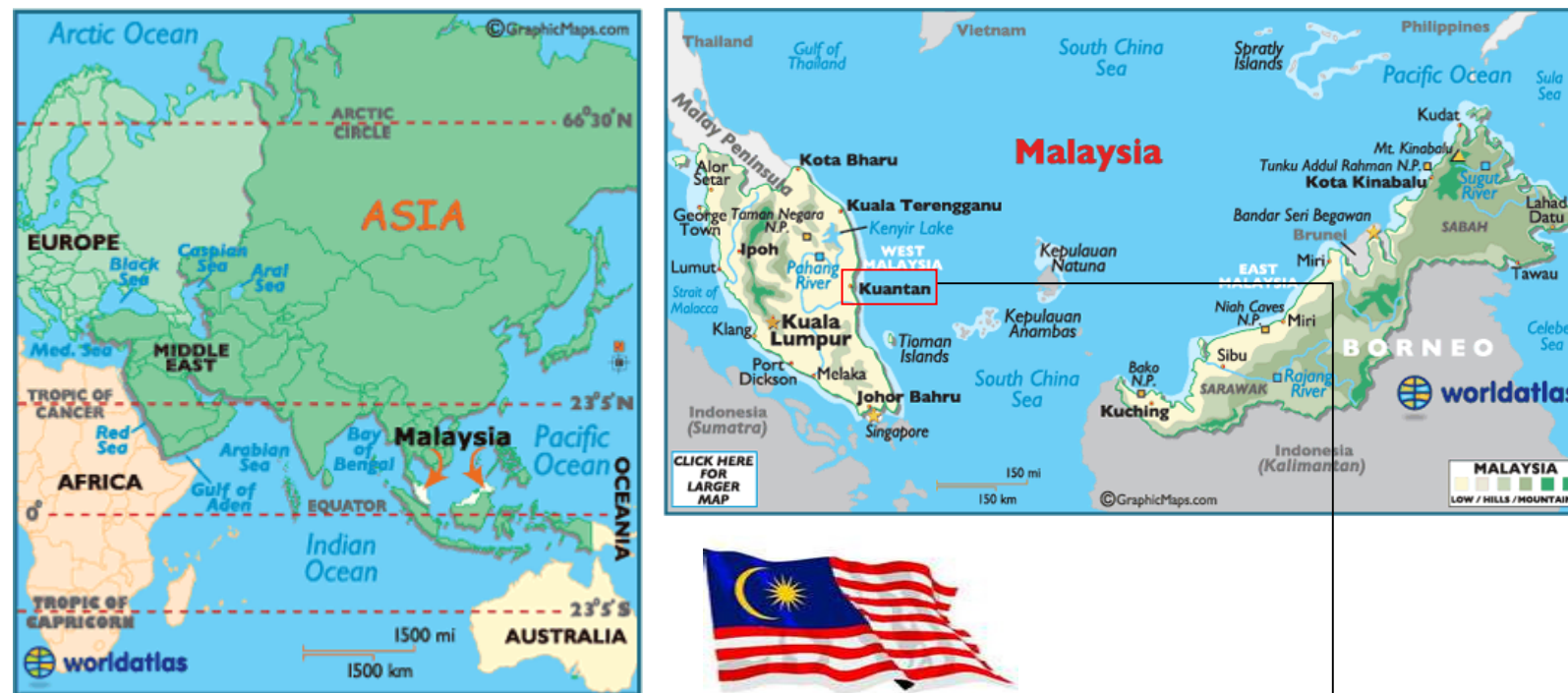
1. INTRODUCTION

1.1 THE REPORT

This report is about the design, analysis, detailing, fabrication and execution of tensile membrane roof over existing Wisma Belia swimming pool at Kuantan for aquatic events for the XV Malaysia Games from 7th July to 16 July 2012.

1.2 MALAYSIA

Malaysia is located in Southeast Asia, just north of the Equator. It comprise of East Malaysia and Peninsula Malaysia. They comprise of 13 states and 3 federal territories. Malaysia is the only federal constitutional monarchy in Southeast Asia.



The population is estimated to be about 29 millions (July, 2011 est.) and represented by the multiple ethnic groups of mainly of Malays 50.4%, Chinese 23.7%, indigenous 11%, Indian 7.1% and others 7.8% (2004 est.). And the official language is Bahasa Malaysia.

1.3 MALAYSIA GAMES - SUKMA

In 1986, Malaysian Games **SUKMA** which is an acronym for Sukan Malaysia in Malay language is introduced to unearth new talents for international competition and also to rapport harmony among the multiple ethnic populations.

It was a biyearly event which was first held in Kuala Lumpur, the capital of Malaysia. It was change to annual event in 2011 and this year 2012 the 15th Malaysia Games is hosted by state of Pahang from 7 July to 16 July. Pahang is on the east coast of Peninsula Malaysia.

At end of 2010, the Pahang state government announced to upgrade building facilities for 2012 Sukma Games. And the existing Wisma Belia swimming Pool at Indera Mahkota (Indera Mahkota Youth Complex), Kuantan is one of the chosen venue for aquatic events.



Published: Monday November 29, 2010 MYT 4:11:00 PM

Pahang upgrading, building facilities for 2012 Sukma Games

KUANTAN: The Pahang government is upgrading and building facilities in preparation for 2012 Sukma Games, said State Youth, Sports and Culture Committee Chairman Datuk Wan Adnan Wan Mamat.

Venues being upgraded include Wisma Belia swimming pool in Indera Mahkota, Indera Mahkota Hockey Stadium, petanque court in Balok, woodball park in Rompin and Pahang Indoor Sports Stadium.

"We are also repairing existing facilities like Indera Mahkota Gymnasium, weightlifting hall in Rompin, Indera Mahkota Indoor Stadium, lawn bowling field, squash court in Taman Gelora and Sultan Haji Ahmad Shah Silver Jubilee Hall in Pekan," he said in reply to a question by Datuk Pang Tsu Ming (BN-Semambu) in the state assembly Monday.

Wan Adnan said new facilities being build include Wisma Belia Hockey Stadium, Temerloh Hockey Mini Stadium, Bentong Hockey Stadium, Indera Mahkota shooting range and a silat court in Temerloh.

He said the State Executive Council had set up a Pahang Sukma 2012 main committee, organising sub-committee and a secretariat.

Meanwhile, State Rural Development and Orang Asli Affairs Committee chairman Datuk Wan Rosdy Wan Ismail said RM11.96mil was spent on housing the hardcore poor under the Ninth Malaysia Plan (9MP).

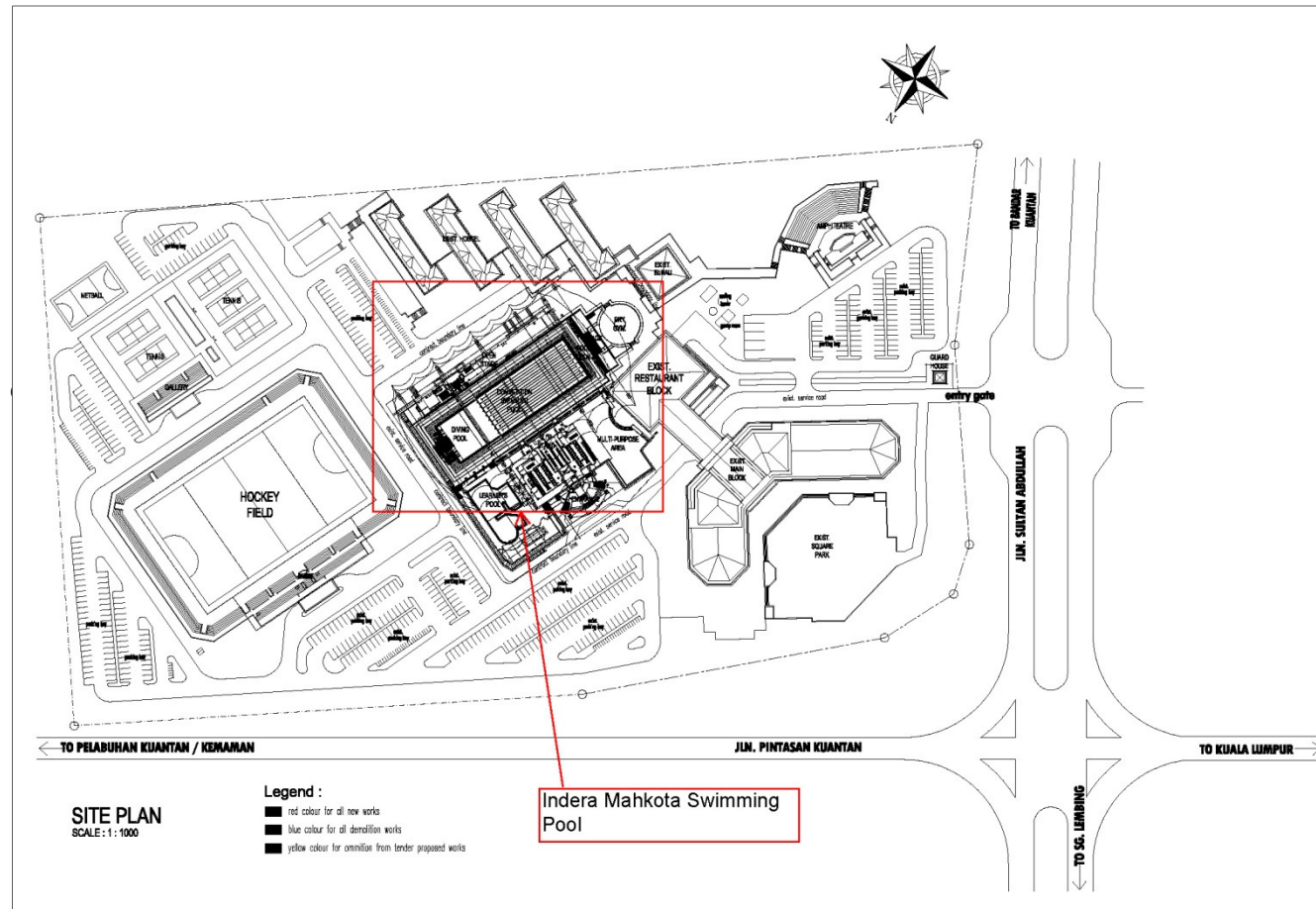
"Some 2,262 houses were built for the orang asli community in Pahang under 9MP," he said in reply to a question by Datuk Mohamed Jaafar (BN-Jenderak). - Bernama



BEAUTIFUL BEACHES OF KUANTAN



1.4 PROJECT AND SITE



SITE PLAN



EVENT SIGNBOARD FOR SWIMMING EVENTS



BANNERS ALONG ROAD TO SITE



MORE BANNERS ALONG ROAD TO SITE



EXISTING POOL LOOKING TO HOCKEY STADIUM AT FAR END



EXISTING POOL LOOKING TO EXISTING RESTAURANT

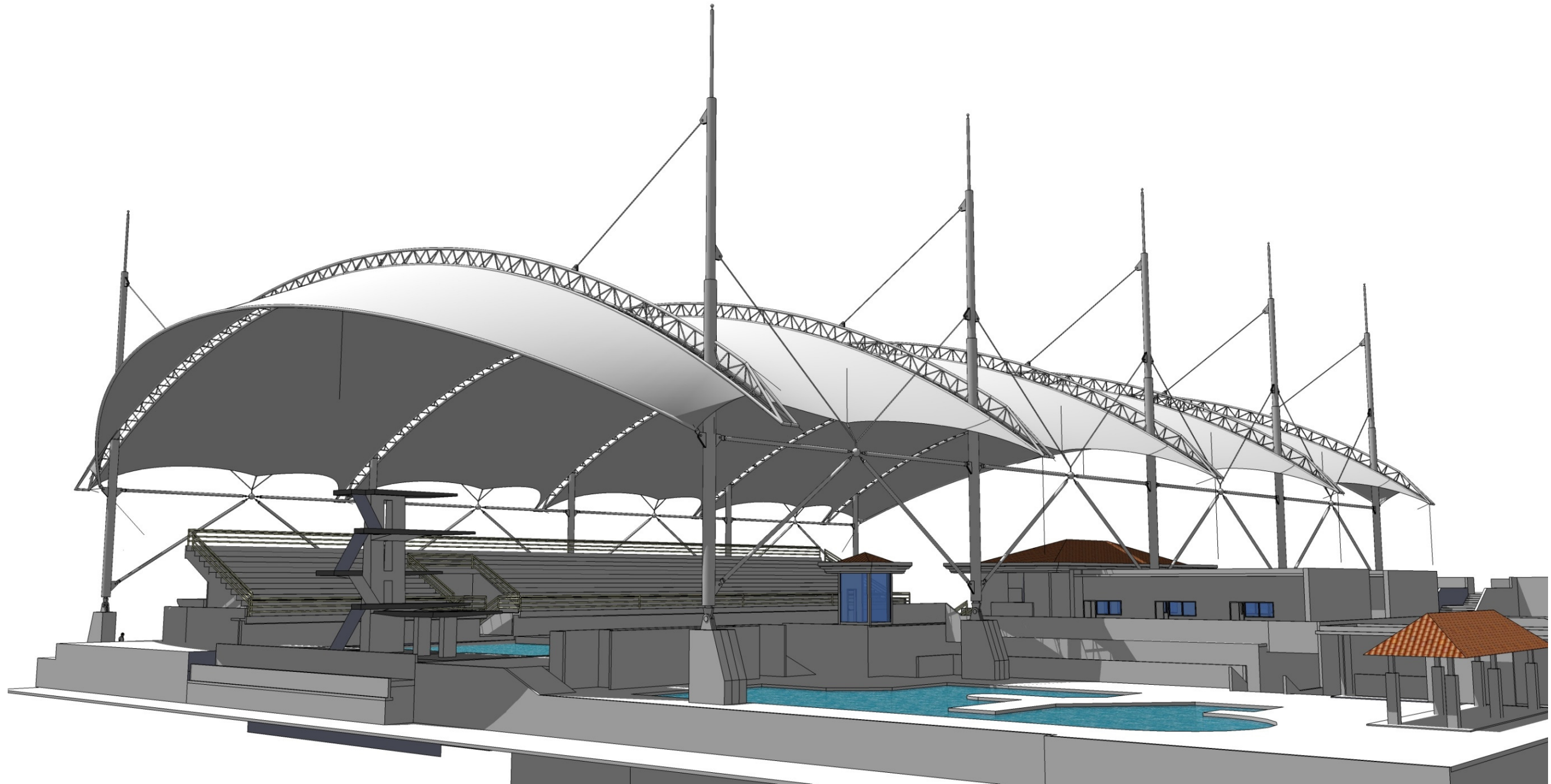


EVENT SIGNBOARD BESIDE ENTRY GATE



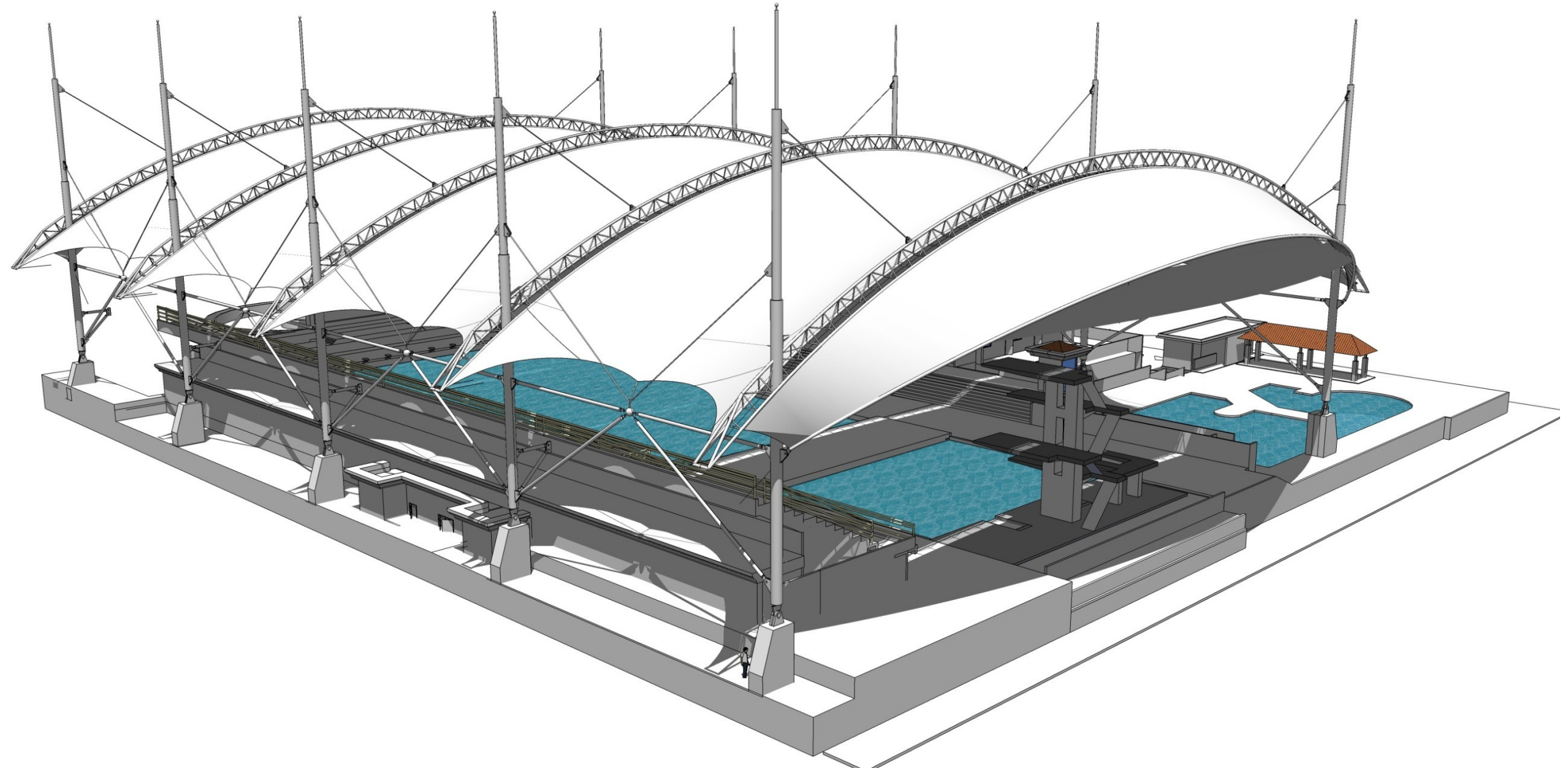
2. ARCHITECTURE CONCEPT & DESIGN DEVELOPMENT

2.1 ARCHITECT'S INTENT



VIEW FROM FRONT

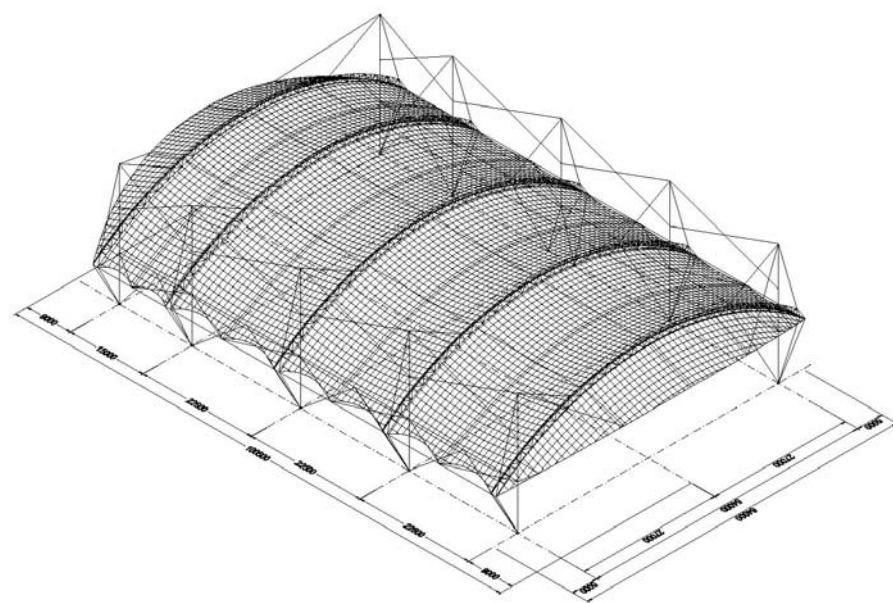
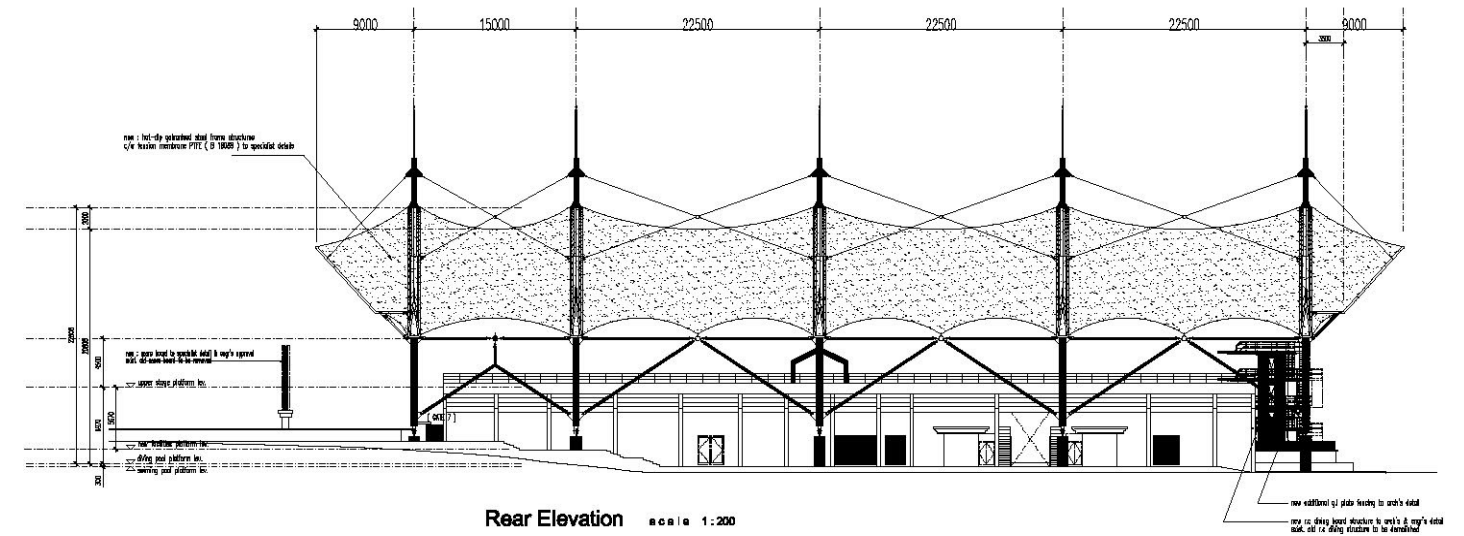
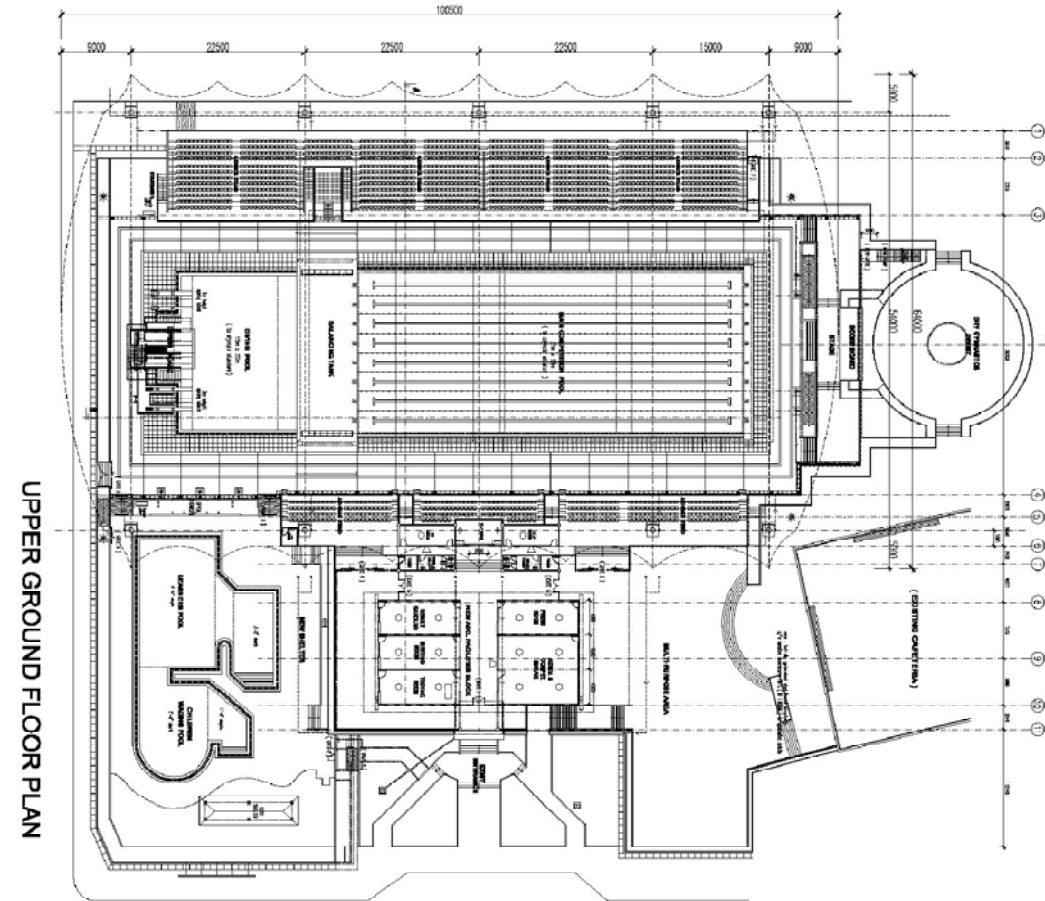




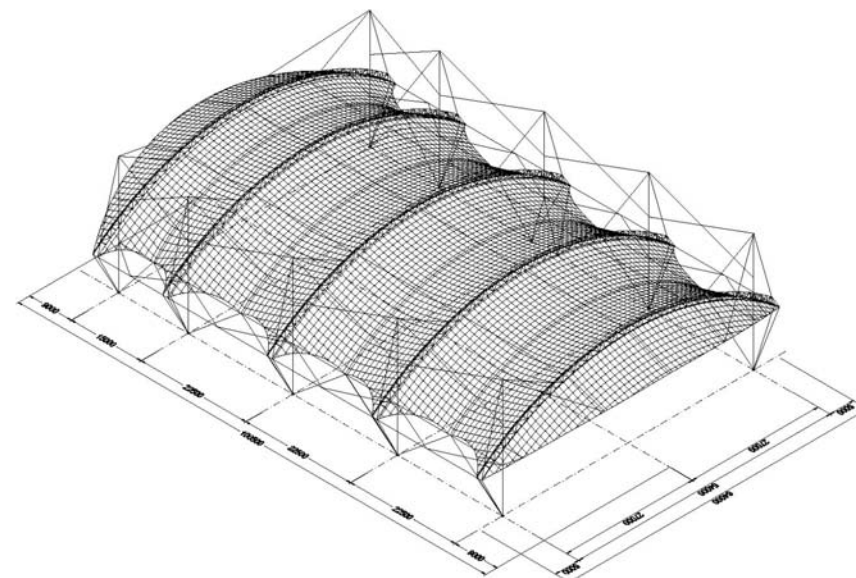
VIEW FROM REAR

2.2 DESIGN DEVELOPMENT

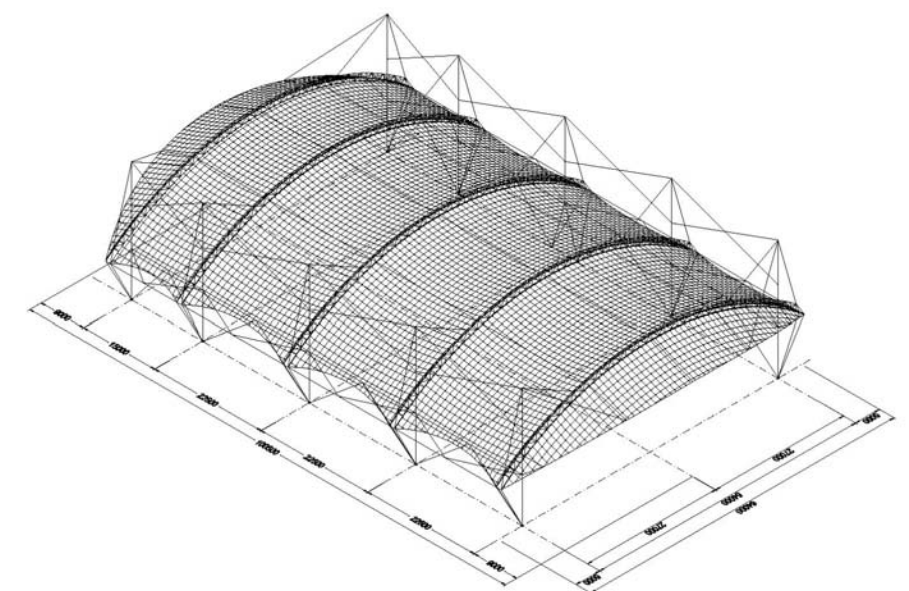
2.2.1 ORIGINAL UNEQUAL GRIDS



OPTION 1 - valley cable to end of truss

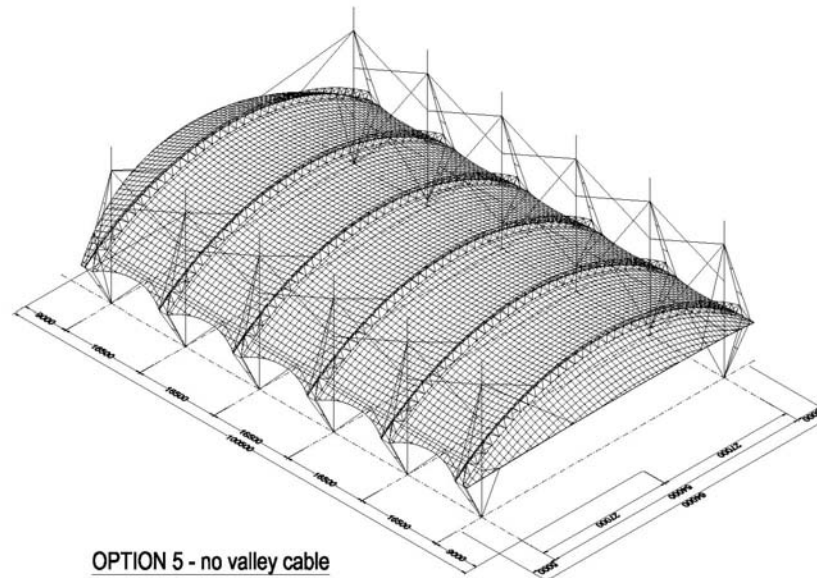
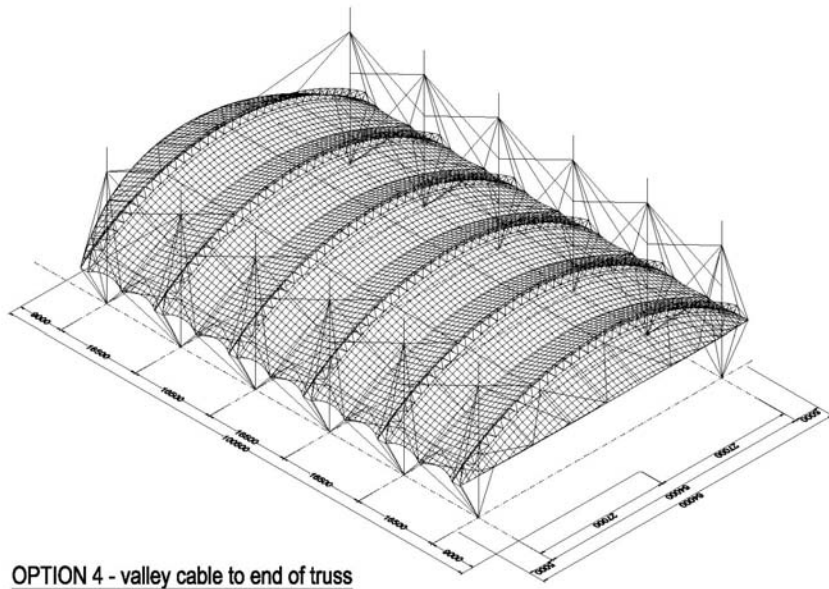
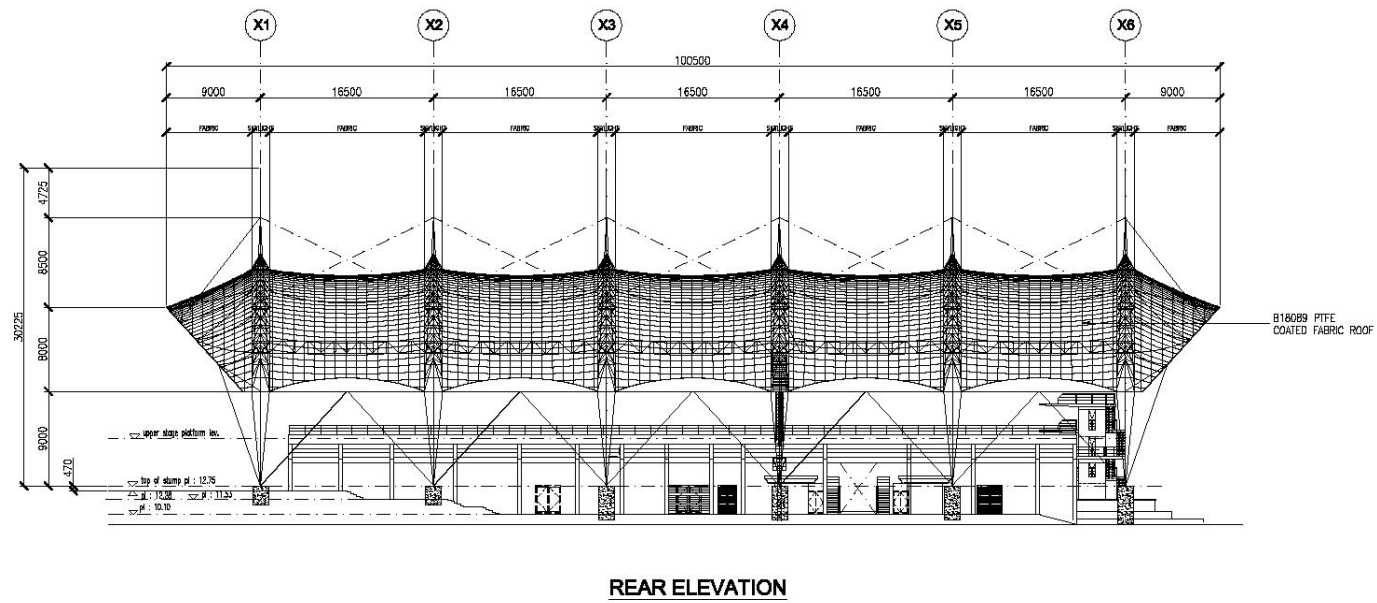
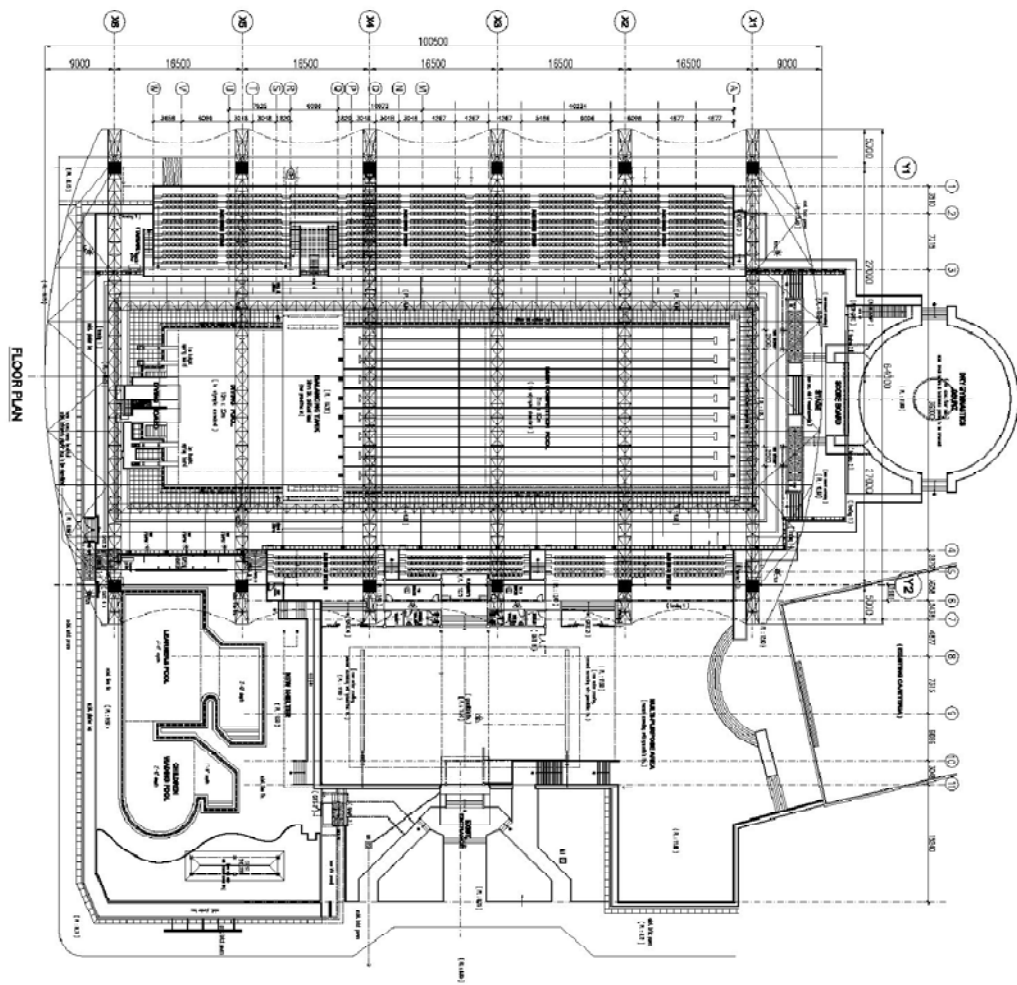


OPTION 2 - valley cable to column line



OPTION 3 - no valley cable

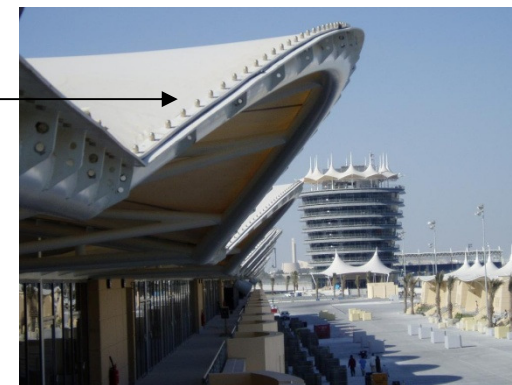
2.2.2 PROPOSED EQUAL GRIDS



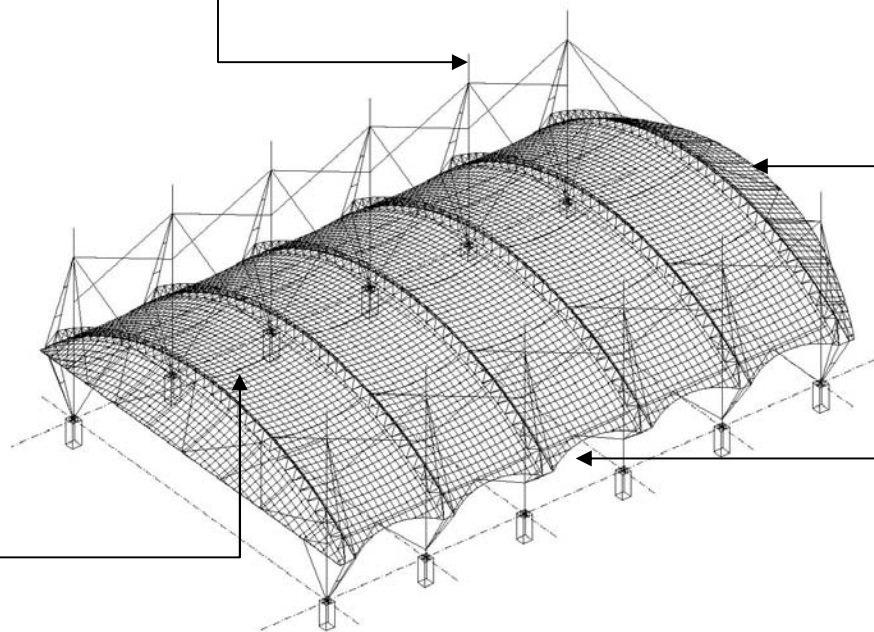
2.2.3 DETAILS AND DESIGN REFERENCE FROM JOB DONE



FRONT HANGER & BACKSTAY DETAIL TO LANGKAWI STADIUM GRANDSTAND CANOPY



END CAP DETAIL TO BAHRAIN PIT BUILDING



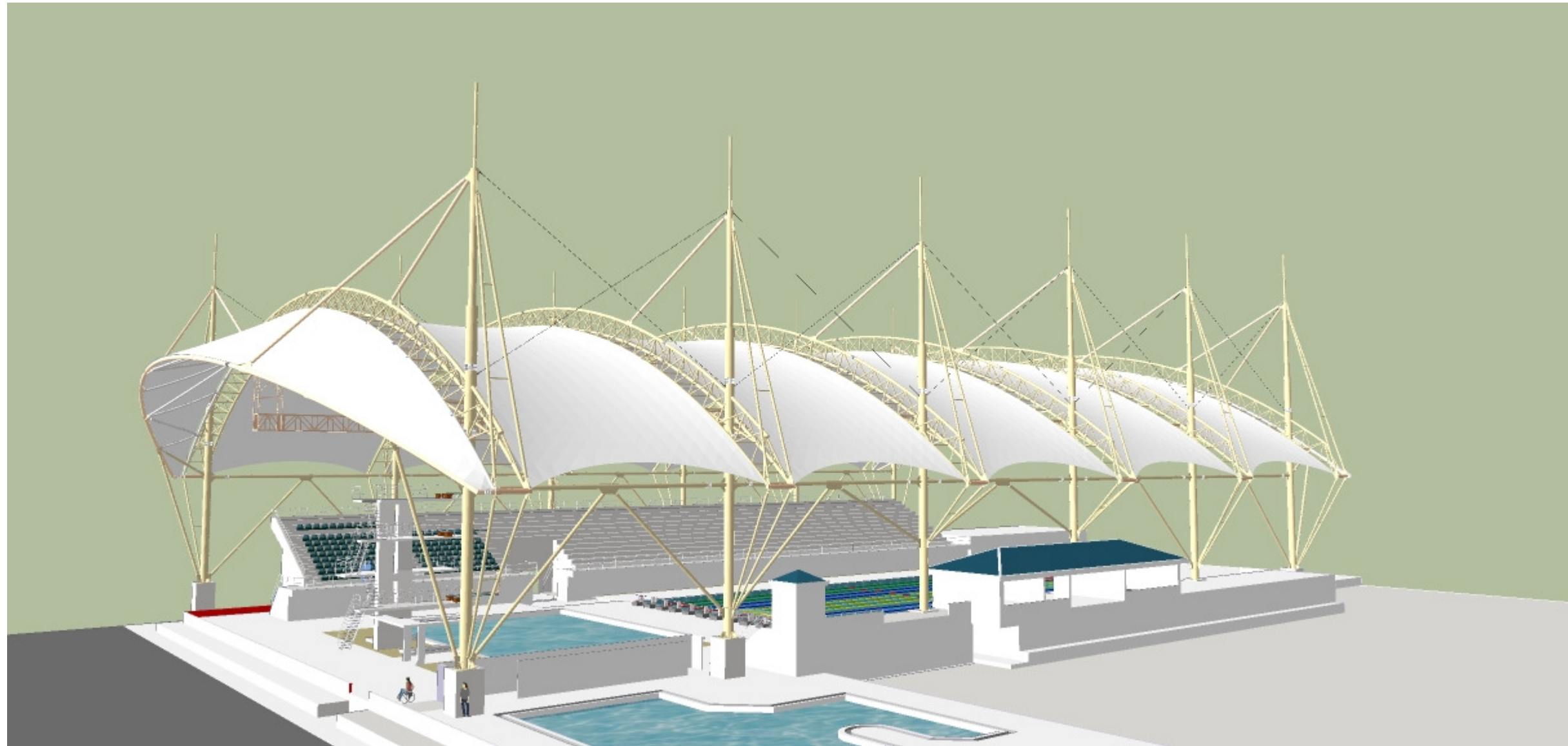
TRUSS TIE SYSTEM TO BUKIT KIARA X-TREME SPORT COMPLEX



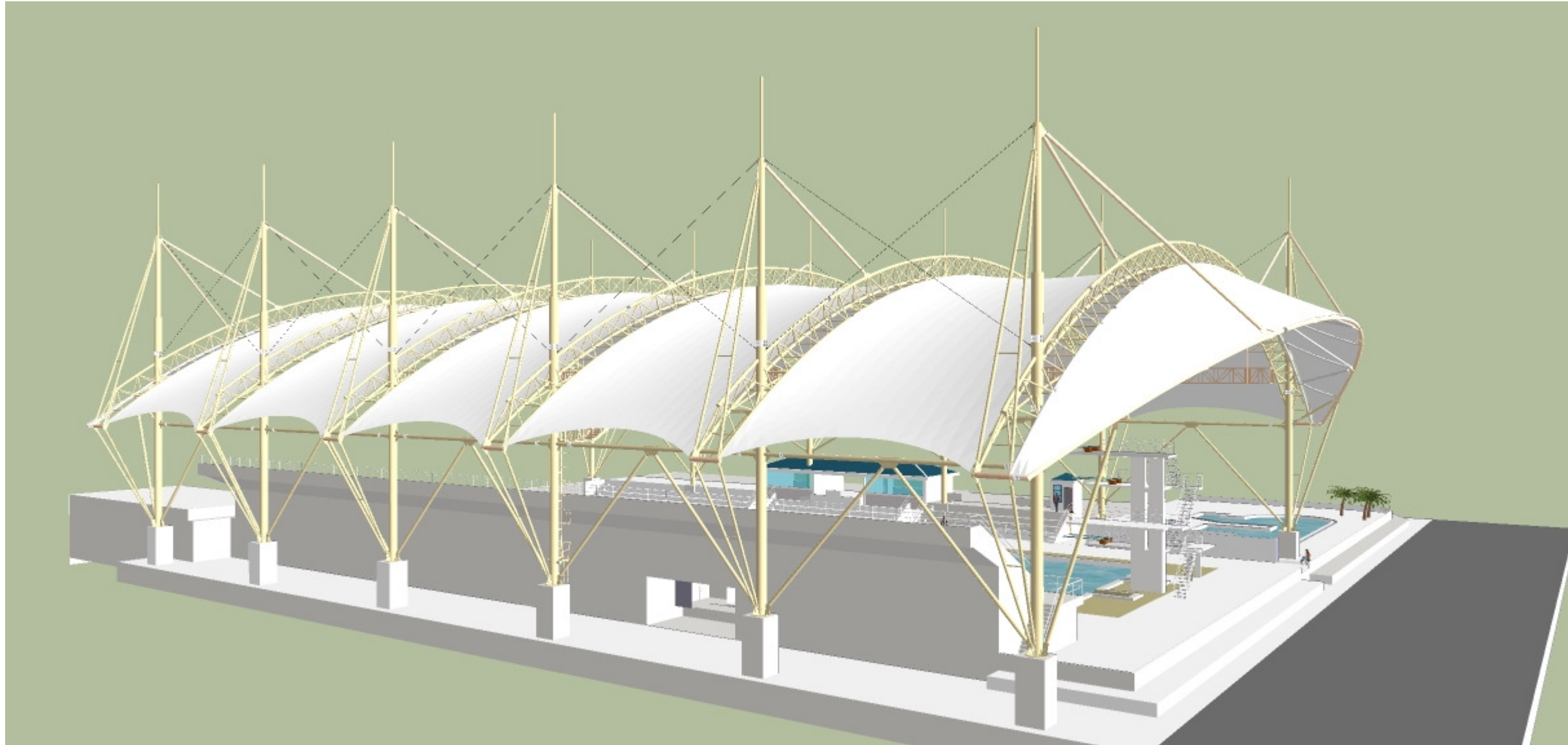
BORDER CABLE AND CORNER PLATE DETAIL TO BAHRAIN MULTI-PURPOSE BUILDING



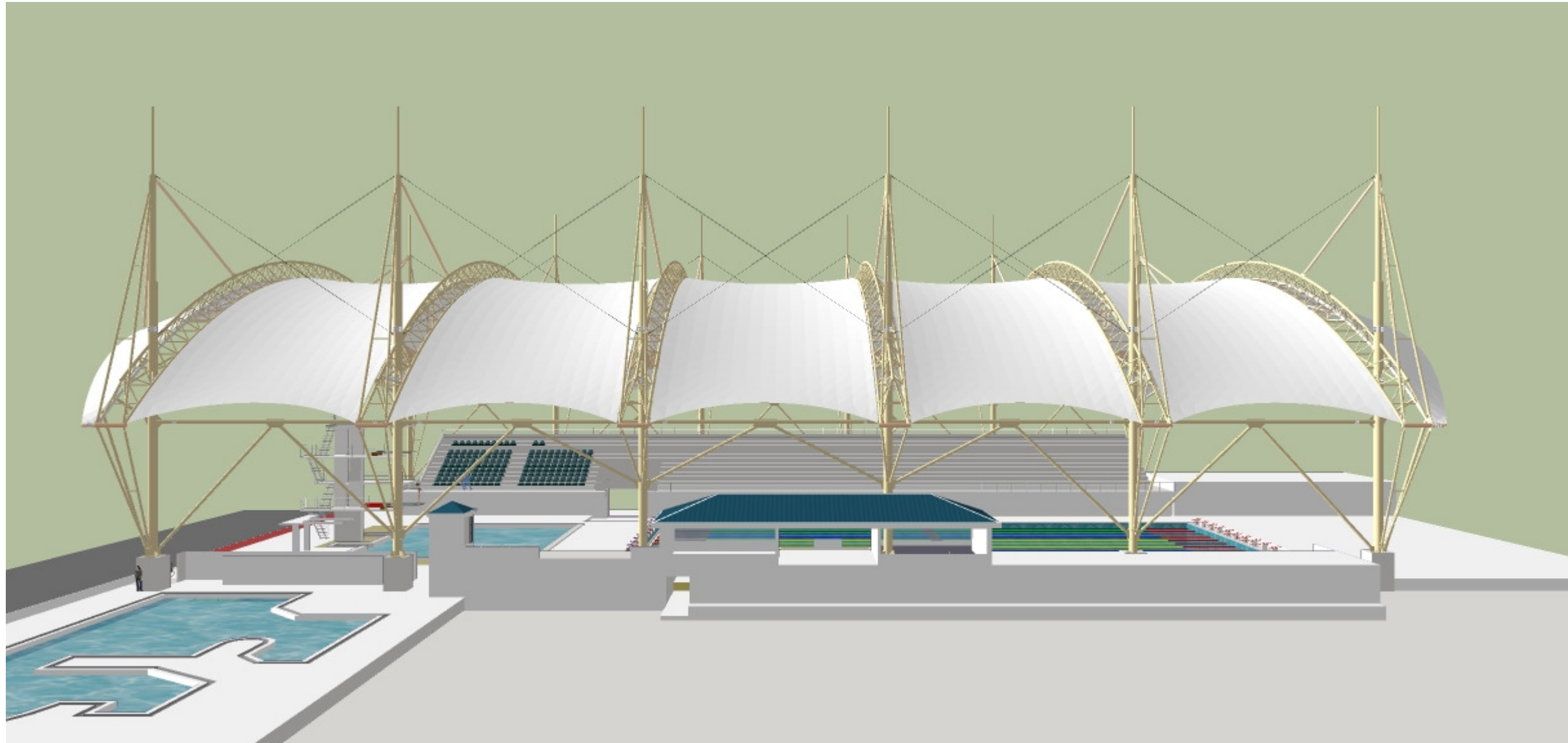
2.3 FINAL DESIGN CONCEPT



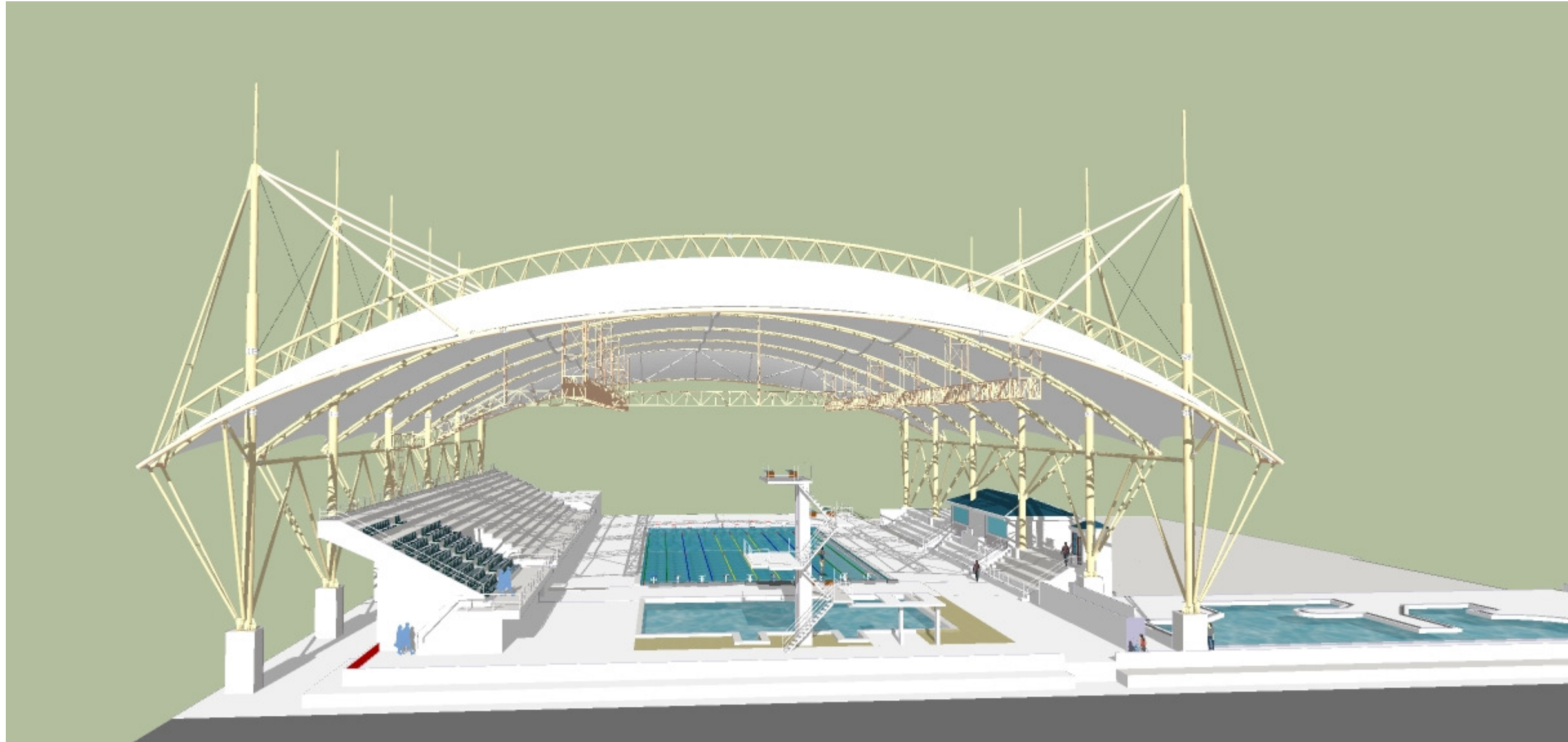
VIEW FROM FRONT



VIEW FROM REAR



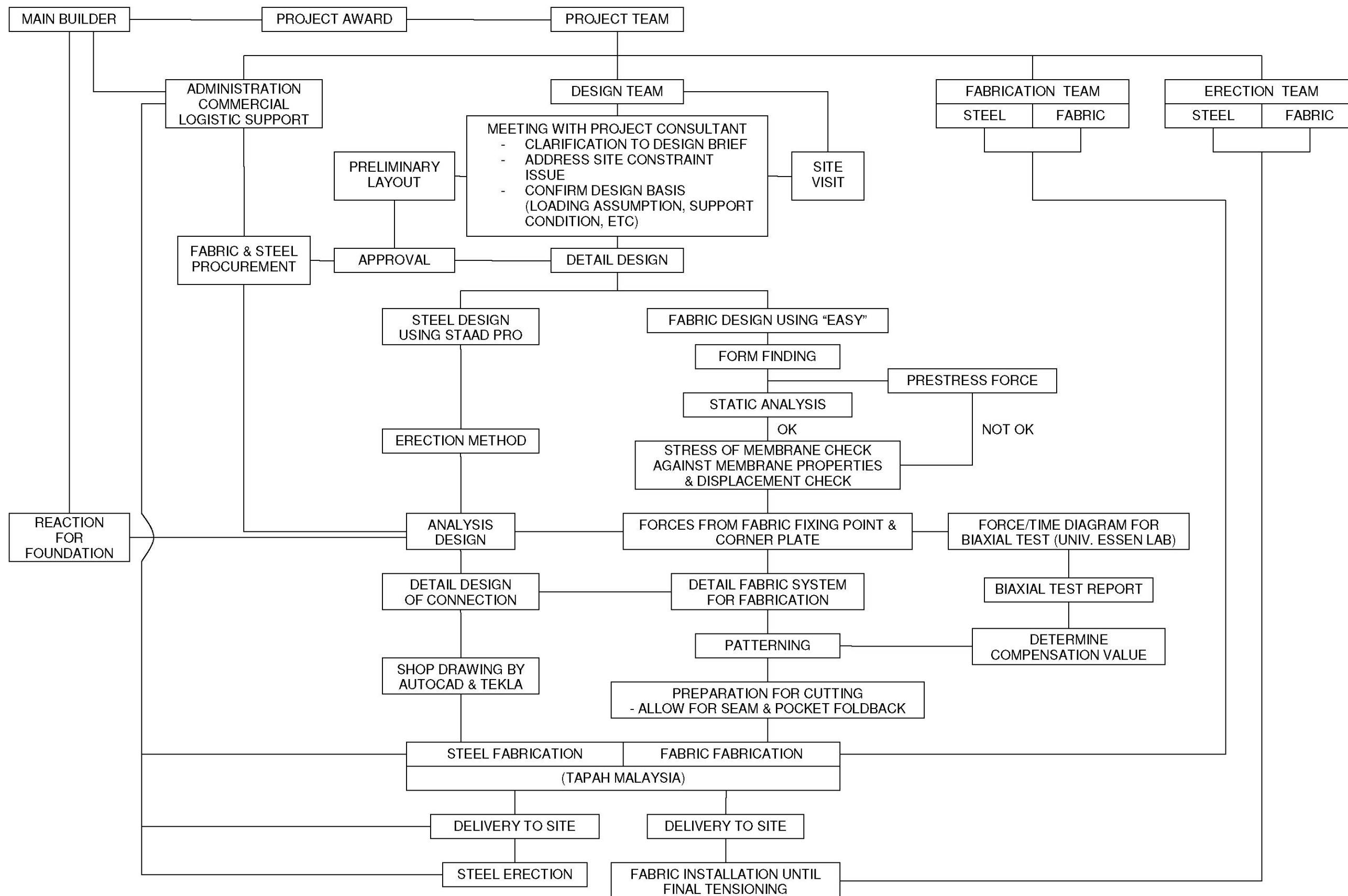
FRONT ELEVATION



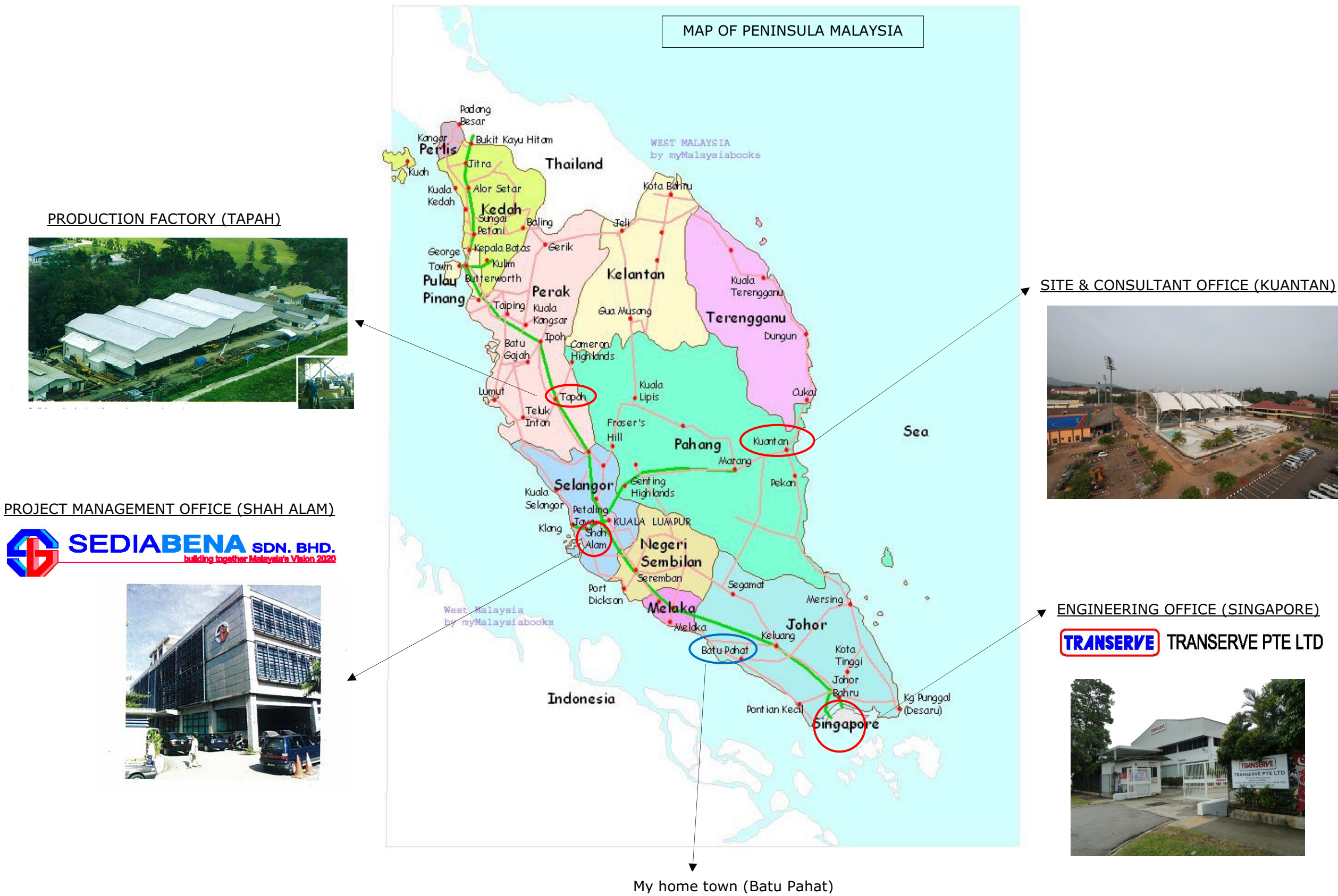
LEFT ELEVATION

3. PROJECT ORGANISATION

3.1 FLOW CHART OF ENGINEERING DESIGN PROCESS IN RELATION TO PROJECT EXECUTION



3.2 GEOGRAPHICAL LOCATION OF PROJECT OFFICE



4. GENERAL INFORMATION

4.1 PROJECT BRIEF

The proposed tensile PTFE (polytetrafluoroethylene) coated glass fiber roof is under the care of the Kuantan Town Council or Majlis Perbandaran Kuantan (MPK) in Malay language. The roof cover a main competition pool of 21m x 50m and a diving pool of 15m x 20m, both are of Olympic standard. The membrane used is B18089 of Verseidag, Germany. The foot print of the roof is approximately 100m x 64m on plan.

The swimming pool roof is a barrel vault like structure of 82.5m length with both end a eyelid canopy cantilevered 9m out and sloped 24 deg downward.

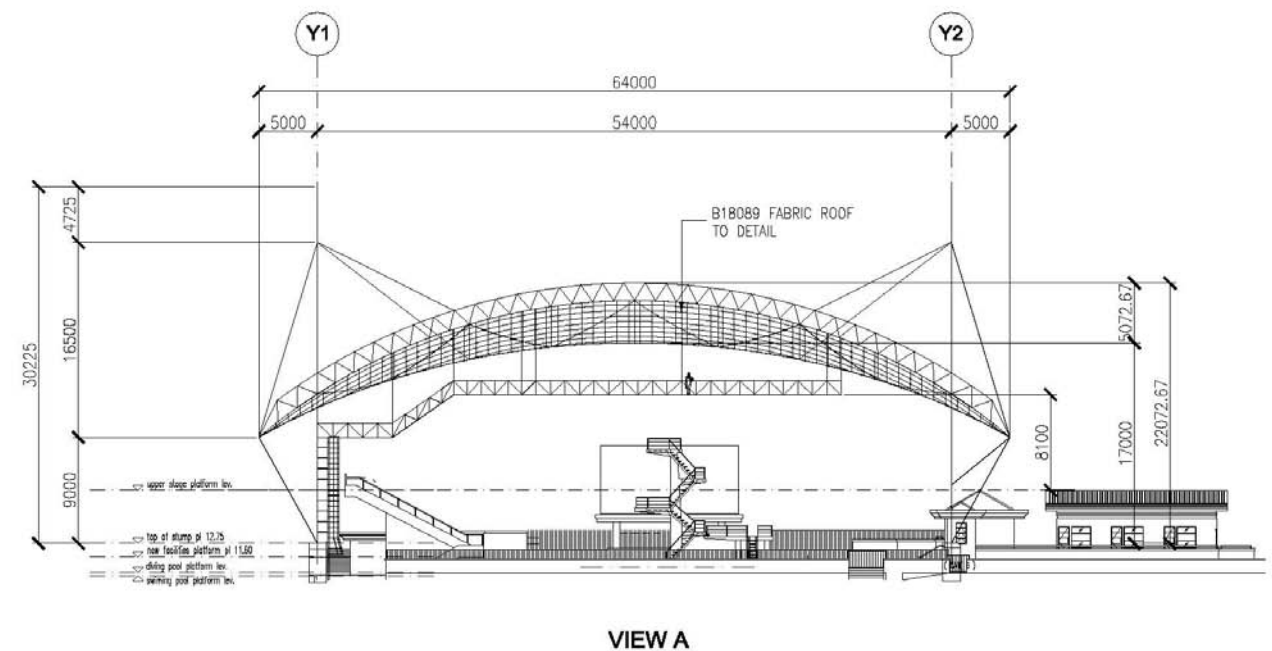
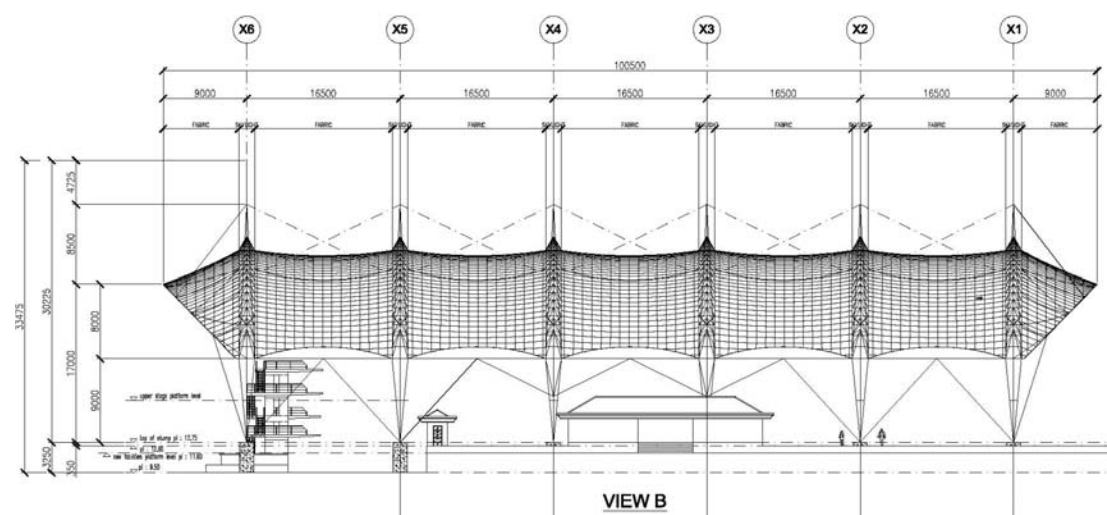
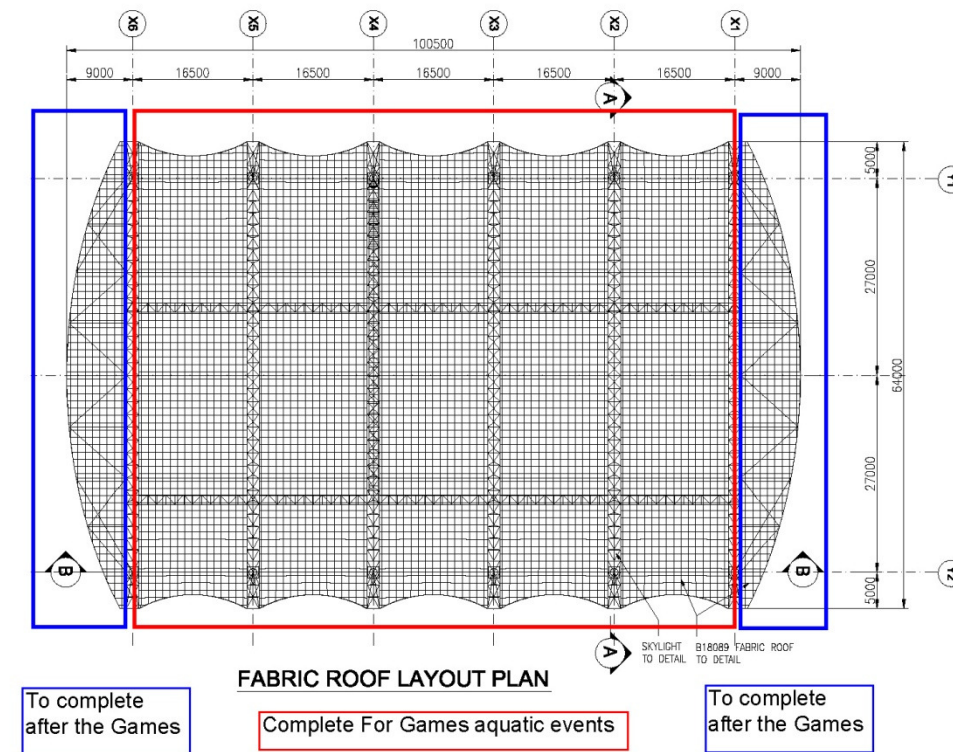
The steel roof structure comprise of 6 nos of 3D triangular truss of 1.7m width x 1.5m constant depth and spaced at 16.5m. Each truss is integrated with steel mast at 54m center to center at both end. The overall height of columns are 30m and top of truss is 22m above the general pool level. These columns are stabilized with front hanger and upper and lower backstay at rear. There are 1 column near the main entrance which 'punch' through the existing roof of the VIP room. The overall structure are braced longitudinally along the column gridline and also 3 single member curved tie beam at 3 location of bottom chord of the 3D truss. The base of column mast is then bolted to the precast holding down bolt to 1.5mx1.5m RC stump. And all steel frame are bolted connections.

Approximately 220m run of 1.2m wide catwalk is hanged from these 3D truss at 15 location to provide access for maintenance of light fitting which is also fixed on the railing of catwalk.

The fabric roof is make up of 5 internal panels and 2 end panels. The internal fabric panel is fixed across the bottom chord of 2 nos of 3D truss at 16.5m center to center and inside of the triangular truss is then fixed with 4mm thick solid polycarbonate sheet.

In summary, the project contract of approximately 6.2 million Malaysia Ringgit is to be completed in 5 months time for 6000m² of membrane, 250 tons of steel frame, and 25 tons of 220m long of catwalk.

In considering the short project time, it is agreed with the client MPK that there will be 2 phase of completion, before the games to finished installed all 5 internal panels from gridline X1 to X6 and after the games to continue to completed the 2 remaining end frame.



4.2 REFERENCE DOCUMENTS

Malaysia Standard MS 1553 : 2002 Code of Practice on Wind Loading For Building Structure

4.3 UNIT

The S.I system shall be used : ie mm, m, KN and etc

4.4 DESIGN CODE AND STANDARD

CP 3 : Chapter V-2 : 1993 Incorporating Amendment Nos. 1, 2, 3, 4 and 5
- Wind Loads

BS 6399 : Part 1 : 1996 – Code of practice for dead and imposed loads

BS 6399 : Part 3 : 1988 – Code of practice for imposed roof loads

BS 5950-1 : 2000 – Code of practice for design – Rolled and welded sections

4.5 COORDINATES SYSTEM

The design model structural axis system is as follow:

- +X from grid line X6 to X1
- +Y from grid line Y2 to Y1
- +Z vertically up

4.6 MATERIAL

4.6.1 STEEL

All circular hollow section to BS EN 10210 S275 or equal and general plates to BS EN 10025 S275 or equal. The corner plate is using S355 material. The choice of material used is subject to availability of material. For analysis and design of the structure steel roof, yield stress of 275 N/mm² is assumed.

4.6.2 CABLE

Border cable use PE coated galvanized steel wire rope, and safety cable is galvanized steel wire rope dry type.

4.6.3 MEMBRANE

PTFE fabric B18089 from Verseidag, Germany.

4.7 METHOD OF ANALYSIS

The analysis of the tensioned membrane structure is done in two parts. Firstly is to do the form finding of the membrane. Then by using the forces from the static analysis of the prestressed membrane and applied to the steel structure and do a design check of the steel structure.

4.7.1 FABRIC ROOF

The task of determining appropriate forms of the membrane based on the given outline is using the software EASY from Germany.

The EASY form finding method is based on the method of force density algorithm. After the equilibrium shape is formed, the form is then applied with external load, ie imposed load, wind load and etc. and static analysis of the fabric is then carried out.

External load which will be applied to the surface of the membrane will be represented by nodal forces.

4.7.2 STRUCTURAL STEEL SYSTEM

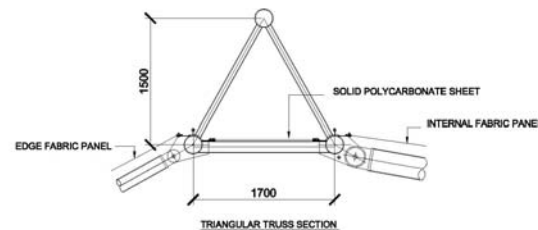
The output forces from the membrane for all the load case from EASY is then extract for use as input forces to the structural steel and then for design purposes.

The finite element software used for the steel analysis is STAAD PRO2007, developed by Research Engineers International, USA.



5. STRUCTURAL SYSTEM

The steel roof structure comprise of 6 nos of 3D triangulated truss of 1 top chord 1.5m height and 2 bottom chord of 1.7m wide. These trusses are spaced at 16.5m and integrated with steel column at 54m center. The overall length of the truss is 64m with 11.6m rise at the center. Each of these integrated truss with column height of 30m is stabilized with 1 front stay and 2 upper and lower backstay.

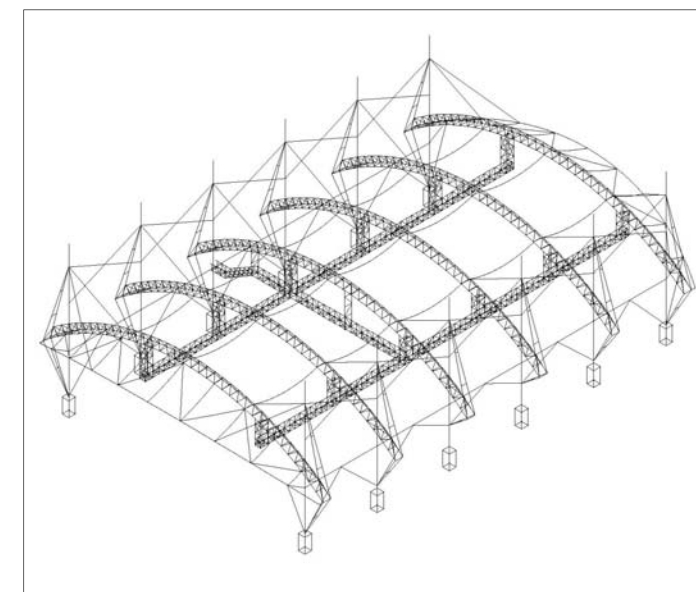


The stability of the structure is dependent on ties and bracing along the column longitudinally. They are also tied quarterly at 3 locations across the bottom chord of the trusses. At the upper part of the column, a pair of crossly brace safety cable is introduced.

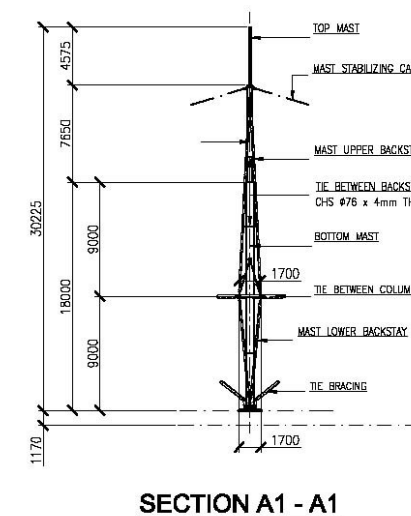
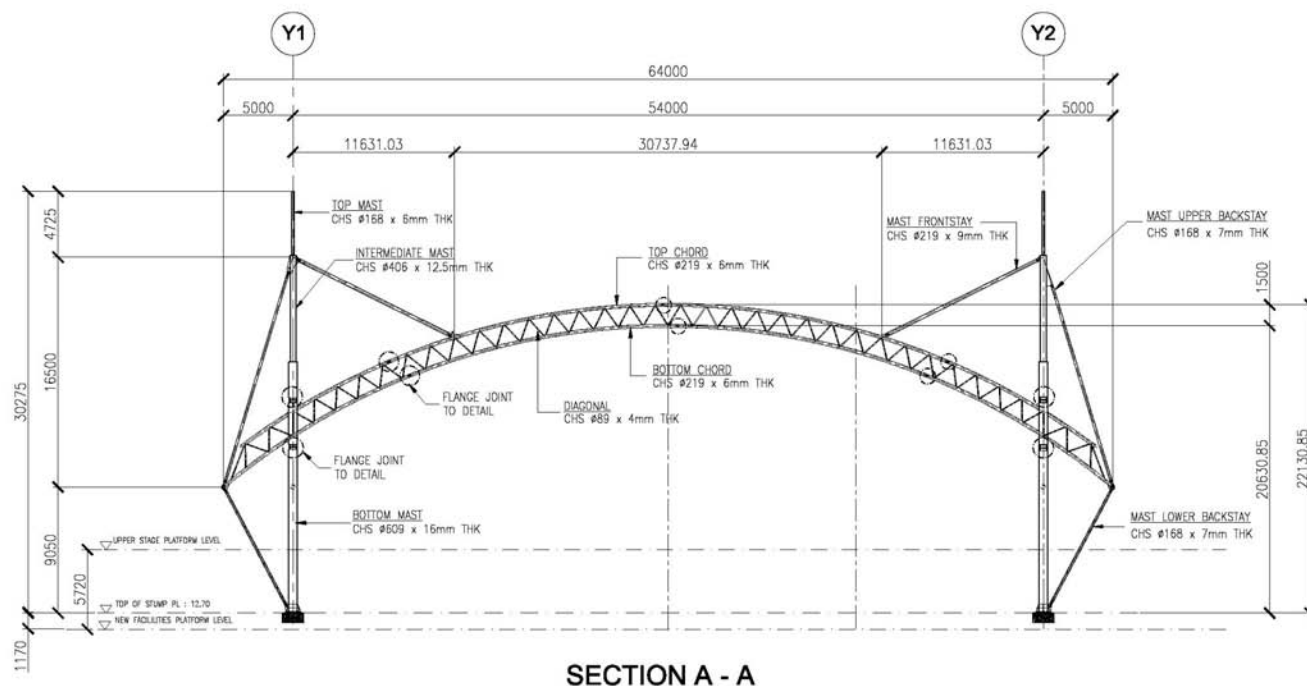
Due to limitation and constrain for site access, the steel structure is designed such that it will be able to be lifted by a small tonnage crane eg. 30 tons and so bolted connection is decided.

The 64m truss is then make up of 4 segment with flange joint connection. The 30m high column is divided into 3segment and connected at just before and after the 3D truss with flange joint. So is the bracing and ties along the columns, and the end canopies frame are also assembled in 3 parts by bolting system.

The 3D trusses is also providing supports to about 220m run of catwalk at 15 location of general 4 hanging point each. There are 2 row of 82.5m long catwalk parallel to and about 15m high from the swimming pool. Between these catwalk, there is interconnecting link along gridline X4. The catwalk is approximately 1.2m wide x 1.2m high.



3D VIEW OF CATWALK SUPPORT BY TRIANGULAR TRUSSES



6. LOADING ASSUMPTION

The fabric roof and steel structure is subjected to the following loading:

- Self weight of steel truss, column, bracing etc.
- Dead load of catwalk
- Prestress force in the membrane
- Imposed live load on membrane roof and catwalk
- Wind load

6.1 Self weight (SW)

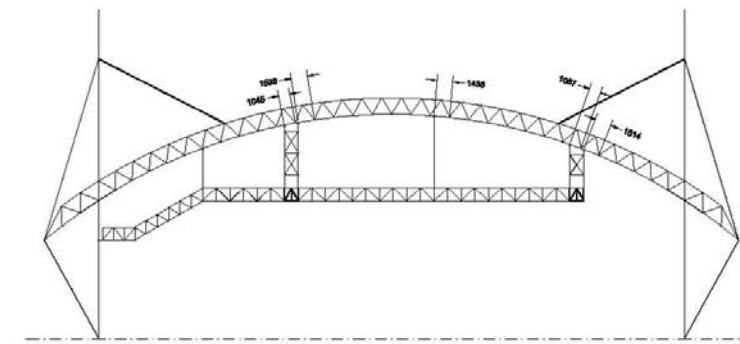
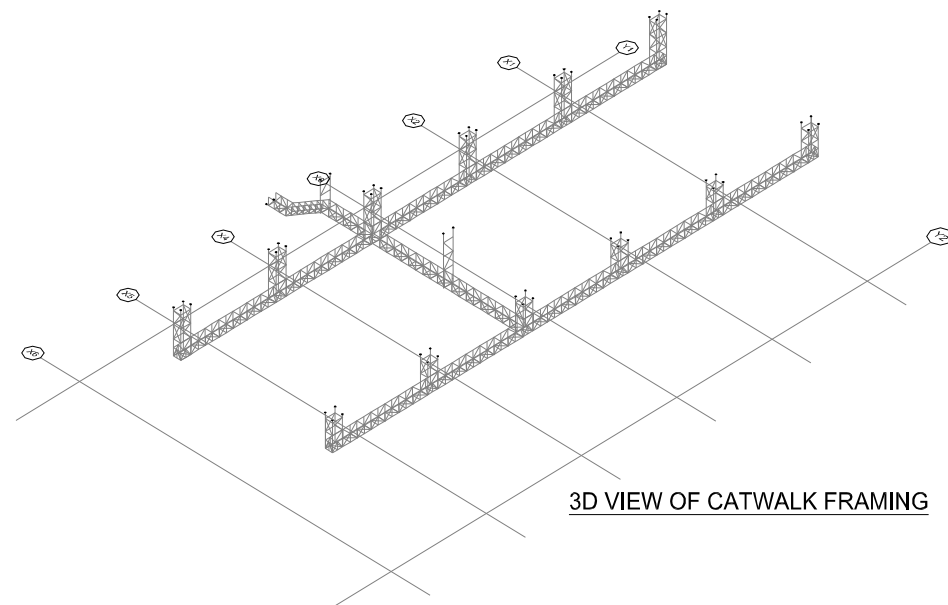
Self weight of steel member = automatically calculated in the software

Self weight of fabric = 1.15 kg/ m^2

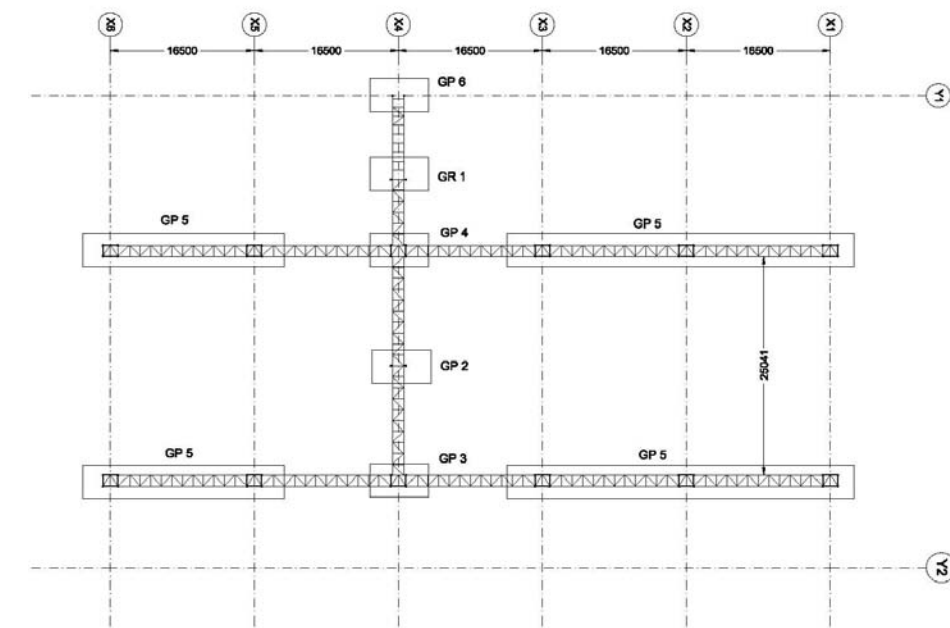
(Insignificant so it is ignored in the membrane load)

6.2 Dead Load of catwalk (DCW)

The catwalk is supported from the 3D truss at 15 Groups of generally 4 point from the bottom chord at $1.7\text{m} \times 1.275\text{m}$ apart each except at gridline X4 where it is the main access.



SECTION VIEW AT GRIDLINE X4



PLAN - GROUP OF APPLIED LOAD FROM CATWALK

The weight of catwalk with expanded mesh + M&E load assumed to be 150 kg/m run

Group 1 load per point = $[(7.544+7.2)/2 \times 150] / 2 = 553 \text{ kg (5.53 KN)}$

Group 2 load per point = $[(25/2) \times 150] / 2 = 937 \text{ kg (9.4 KN)}$

Group 3 load per point = $[(16.5 + 6.25) \times 150] / 4 = 853 \text{ kg (8.53 KN)}$

Group 4 load per point = $[(6.25 + 16.5 + 7.55/2) \times 150] / 4 = 995 \text{ kg (9.95 KN)}$

Group 5 load per point = $(16.5 \times 150) / 4 = 618 \text{ kg (6.2 KN)}$

Group 6 load per point = $[(7.544/2 + 3.3) \times 150] / 2 = 530 \text{ kg (5.3 KN)}$

6.3 Prestress Load (PRE)

Prestress is induced to increase membrane stiffness and obtain a stable form which is in equilibrium. In this case, a prestress force of 3KN/m is assumed for warp and weft direction.

6.4 Imposed Live Load

6.4.1) Membrane roof (VL)

Imposed live load on membrane roof = 0.25 KN/m²

This load is applied vertically downward to the fabric roof.

6.4.2) Catwalk (LCW)

For localized catwalk design, assumed live load = 1.5 KN/m²

For global analysis of the structure roof,
assumed live load applied simultaneously on all catwalk = 0.75 KN/m²

Using the same loading group as in the dead load case,
Live load = 0.75 KN/m² x 1.2m internal clearance of catwalk = 0.9 KN/m

Group 1 load per point = $[(7.544+7.2)/2 \times 0.9] / 2 = 3.32$ KN

Group 2 load per point = $[(25/2) \times 0.9] / 2 = 5.62$ KN

Group 3 load per point = $[(16.5 + 6.25) \times 0.9] / 4 = 5.12$ KN

Group 4 load per point = $[(6.25 + 16.5 + 7.55/2) \times 0.9] / 4 = 5.96$ KN

Group 5 load per point = $(16.5 \times 0.9) / 4 = 3.71$ KN

Group 6 load per point = $[(7.544/2 + 3.3) \times 0.9] / 2 = 3.18$ KN

6.5 Wind Load

Reference to Malaysian Standard MS 1553 :2002 : Code of Practice on wind loading for Building Structure

As Kuantan fall in Zone II as shown in Figure 3.1,
so basic wind speed of 32.5 m/s is adopted for the wind load calculation.

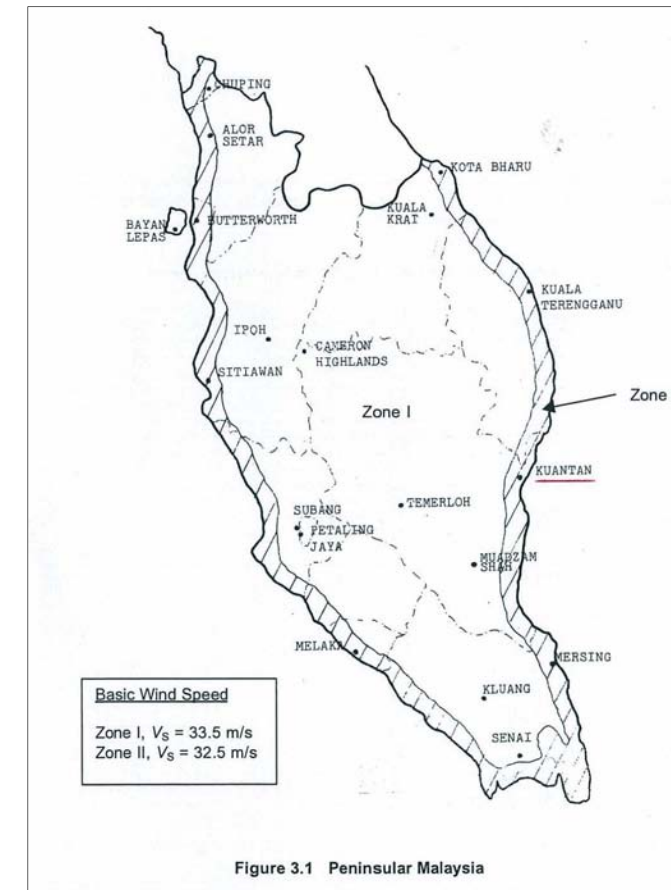


Figure 3.1 Peninsular Malaysia
WIND ZONE MAP OF PENINSULAR MALAYSIA

Reference to CP3 : Chapter V : Part 2 1993 for dynamic wind pressure

Dynamic pressure due to wind is given by :

$$q = k V_s^2 \text{ N/m}^2$$

where $k = 0.613$

$$V_s = V \times S_1 \times S_2 \times S_3$$

Basic wind speed $V = 32.5$ m/s

S_1 - topography factor = 1.0

S_2 - ground roughness, structure size and height above ground factor

Ground roughness = 3

Maximum height = 20 m

Class = C

Therefore $S_2 = 0.85$

S_3 - statistical factor = 1.0

$$V_s = 32.5 \times 1.0 \times 0.85 \times 1.0 = 27.6 \text{ m/s}$$

$$q = 0.613 \times 27.6 \times 27.6 = 467 \text{ N/m}^2 \text{ say } 0.5 \text{ KN/m}^2$$

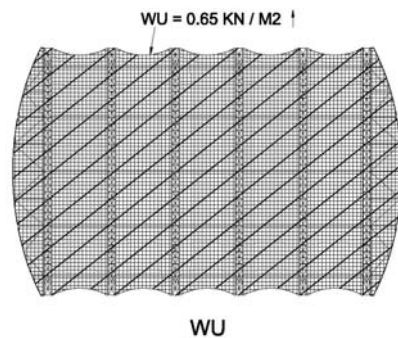
Assumed the fabric roof is duopitch canopy of roof angle approx = 20 deg

Therefore from Table 13,
Assumed the entrance and audience stand is 100% obstruct,

Solidity ratio $\phi = 1$ (obstruct)
Min Overall $C_p = -1.3$ and Max Overall $C_p = +0.6$

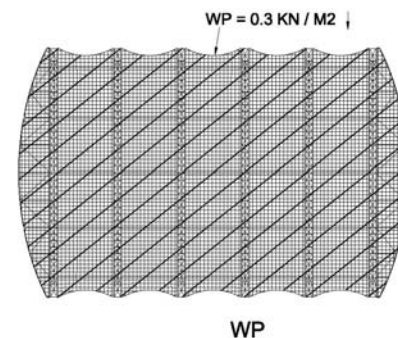
6.5.1) Wind Uplift (WU)

Wind uplift $W_u = -1.3 \times 0.5 = -0.65 \text{ KN/m}^2$



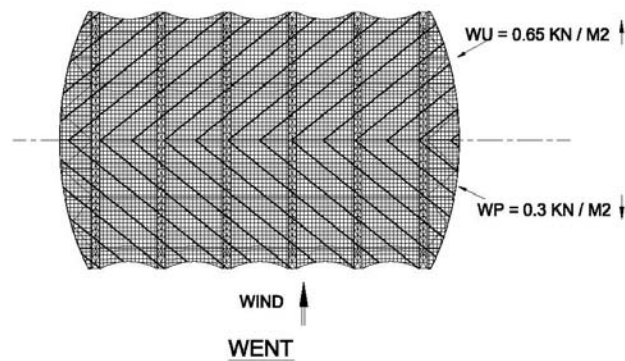
6.5.2) Wind Pressure (WP)

Wind pressure $W_p = +0.6 \times 0.5 = 0.3 \text{ KN/m}^2$



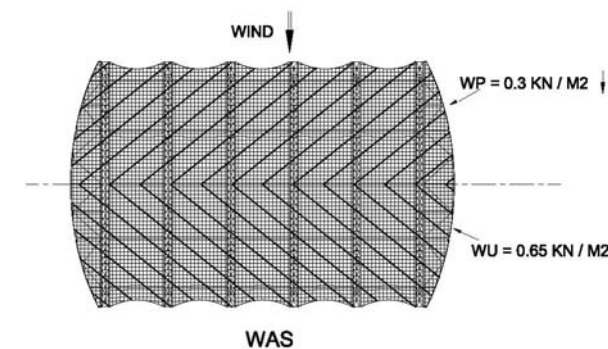
6.5.3) Wind from Entrance (WENT)

Wind Perpendicular to Grid line Y2



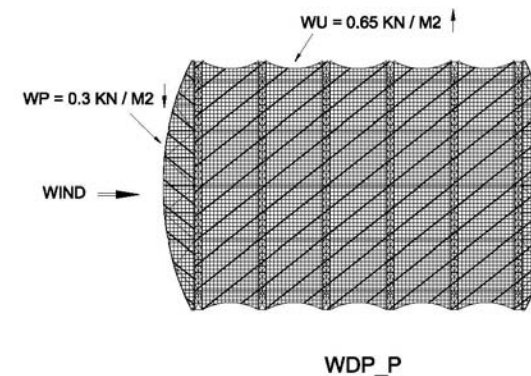
6.5.4) Audience stand (WAS)

Wind Perpendicular to Grid line Y1



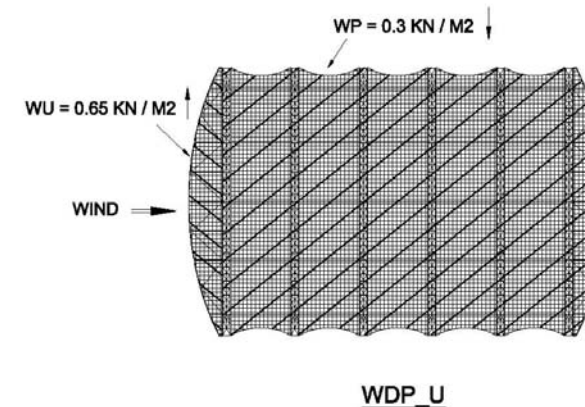
6.5.5) Wind from Driving Pool Side when End bay is Wind Pressure (WDP_P)

Wind Perpendicular to Grid line X6



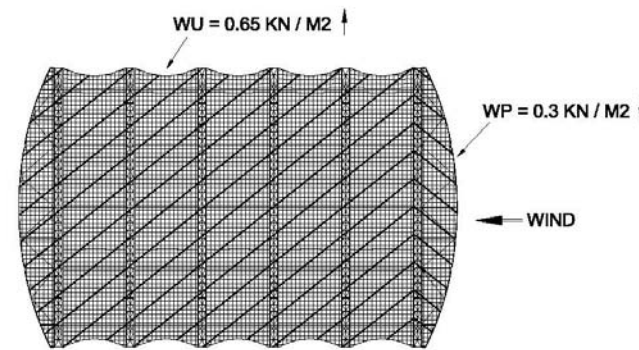
6.5.6) Wind from Driving Pool Side when End bay is Wind Uplift (WDP_U)

Wind Perpendicular to Grid line X6



6.5.7) Wind from Score Board Side when End Bay is Wind Pressure (WSB_P)

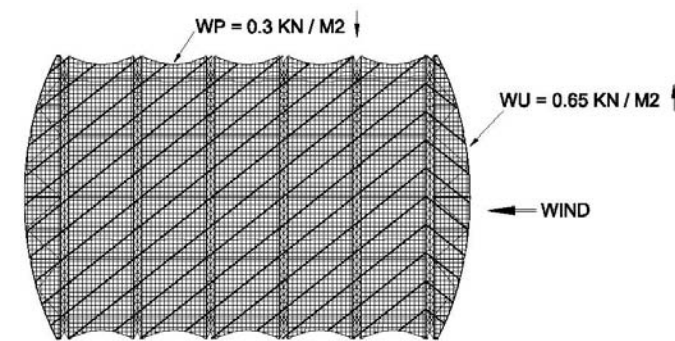
Wind Perpendicular to Grid line X1



WSB_P

6.5.8) Wind from Score Board Side when End Bay is Wind Uplift (WSB_U)

Wind Perpendicular to Grid line X1



WSB_U

7. STEEL ANALYSIS AND DESIGN

7.1 DESIGN METHOD

For the in-placed analysis there will be 2 limit state analysis, service limit state and the ultimate limit state.

The service limit state relate to performance under normal service conditions, e.g deflections. And ultimate limit state are related to safety and load carrying capacity of the structure where the specified loads is multiplied by relevant partial factor.

The design facility available in STAADPRO software shall be used to code check the members for member forces and moment due to the various loading combinations for both limit states.

7.2 DESIGN MODEL

The steel structure has been modeled as a 3 dimensional frame model along the center line of the steel section. The ends of frame member are connected by nodes. All the steel member in this case uses all circular hollow section.

All the steel member are assumed to be frame type except the mast frontstay, backstay, ties between truss and bracings between column. These are assumed to be truss member which will have a bolted connection at both end.

The stabilizing cable between top of mast are assumed to be tension only Member with small diameter solid round bar representing the cables.

The following properties is used for the analysis on the steel member: -

Young's Modulus = $2.10 \times 10^8 \text{ KN/m}^2$

Shear Modulus = $8.0 \times 10^7 \text{ KN/ m}^2$

Poisson Ratio = 0.3

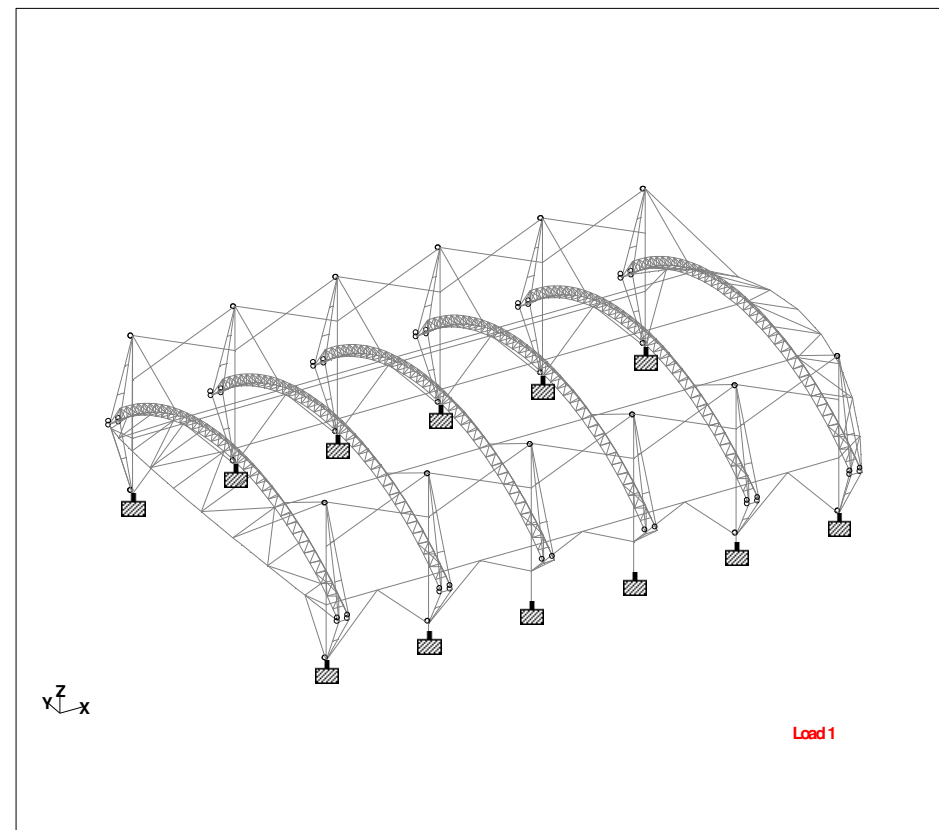
Mass density of steel = 7850 kg/m^3

Gravitational acceleration = 9.81 m/s^2

Coefficient of thermal expansion = $11.7 \times 10^{-6} / \text{deg C}$

For ease of reference, the steel member of the design model has been group as follow;

- a) member 1 to 456 = bottom curved chord of 3D truss
- b) member 457 to 536 = edge member of eyelid canopy
- c) member 537 to 782 = bottom horizontal chord of 3D truss
- d) member 783 to 992 = top curved chord of 3D truss
- e) member 993 to 1928 = diagonal chord of 3D truss
- f) member 1929 to 1962 = bracing and prop member to eyelid canopy
- g) member 1963 to 1977 = tie member between 3D truss
- h) member 1978 to 2041 = lower, intermediate and upper mast
- i) member 2042 to 2061 = tie member at between lower masts
- j) member 2062 to 2077 = mast front stay
- k) member 2078 to 2193 = mast backstay
- l) member 2194 to 2227 = internal short tie of backstay
- m) member 2228 to 2255 = longitudinal bracing between lower mast
- n) member 2256 to 2275 = stabilizing cable at intermediate mast



STEEL DESIGN MODEL

7.3. BASIC LOAD CASES & LOAD COMBINATION

The membrane roof and steel structure system are analyzed based on the following load cases and load combinations.

7.3.1 BASIC LOAD CASES

LOAD 1 (SW) = Self weight of steel structure automatically calculated by the software

LOAD 2 (DCW) = Dead load of catwalk + ME load

LOAD 3 (LCW) = Imposed Live Load on catwalk

LOAD 4 (PRE) = Prestress load from membrane roof WITHOUT any external load

The following external load is applied on to a stable and prestressed membrane form. So the following load case actually consist of prestressing load.

LOAD 5 (VL) = Imposed Live Load on membrane roof

LOAD 6 (WU) = Wind Uplift on membrane roof

LOAD 7 (WP) = Wind Pressure on membrane roof

LOAD 8 (WENT) = Wind from Entrance side (Y2)

LOAD 9 (WAS) = Wind from Audience Stand (Y1)

LOAD 10 (WDP_P) = Wind from Driving Pool side (X6), End bay wind pressure

LOAD 11 (WDP_U) = Wind from Driving Pool side (X6), End bay wind uplift

LOAD 12 (WSB_P) = Wind from Score Board side (X1), End bay wind pressure

LOAD 13 (WSB_U) = Wind from Score Board side (X1), End bay wind uplift

And all the above load case are unfactored load.

7.3.2. SERVICE LOAD COMBINATION

$$\begin{aligned} \text{LOAD 100} &= \text{SW} + \text{DCW} + \text{PRE} \\ \text{LOAD 101} &= \text{SW} + \text{DCW} + \text{LCW} + \text{VL} \\ \text{LOAD 102} &= \text{SW} + \text{DCW} + \text{WU} \\ \text{LOAD 103} &= \text{SW} + \text{DCW} + \text{WP} \\ \text{LOAD 104} &= \text{SW} + \text{DCW} + \text{WENT} \\ \text{LOAD 105} &= \text{SW} + \text{DCW} + \text{WAS} \\ \text{LOAD 106} &= \text{SW} + \text{DCW} + \text{WDP_P} \\ \text{LOAD 107} &= \text{SW} + \text{DCW} + \text{WDP_U} \\ \text{LOAD 108} &= \text{SW} + \text{DCW} + \text{WSB_P} \\ \text{LOAD 109} &= \text{SW} + \text{DCW} + \text{WSB_U} \end{aligned}$$

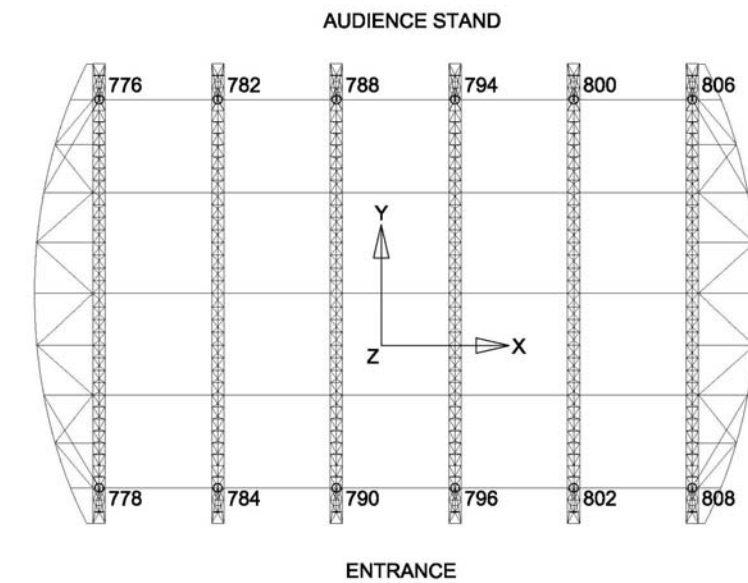
7.3.3 ULTIMATE LOAD COMBINATION

$$\begin{aligned} \text{LOAD 200} &= 1.4(\text{SW} + \text{DCW} + \text{PRE}) \\ \text{LOAD 201} &= 1.4(\text{SW} + \text{DCW}) + 1.6(\text{LCW} + \text{VL}) \\ \text{LOAD 202} &= 1.0(\text{SW} + \text{DCW}) + 1.4\text{WU} \\ \text{LOAD 203} &= 1.2(\text{SW} + \text{DCW}) + 1.2\text{WP} \\ \text{LOAD 204} &= 1.2(\text{SW} + \text{DCW}) + 1.2(\text{WENT}) \\ \text{LOAD 205} &= 1.2(\text{SW} + \text{DCW}) + 1.2(\text{WAS}) \\ \text{LOAD 206} &= 1.2(\text{SW} + \text{DCW}) + 1.2(\text{WDP_P}) \\ \text{LOAD 207} &= 1.0(\text{SW} + \text{DCW}) + 1.4(\text{WDP_U}) \\ \text{LOAD 208} &= 1.2(\text{SW} + \text{DCW}) + 1.2(\text{WSB_P}) \\ \text{LOAD 209} &= 1.0(\text{SW} + \text{DCW}) + 1.4(\text{WSB_U}) \end{aligned}$$

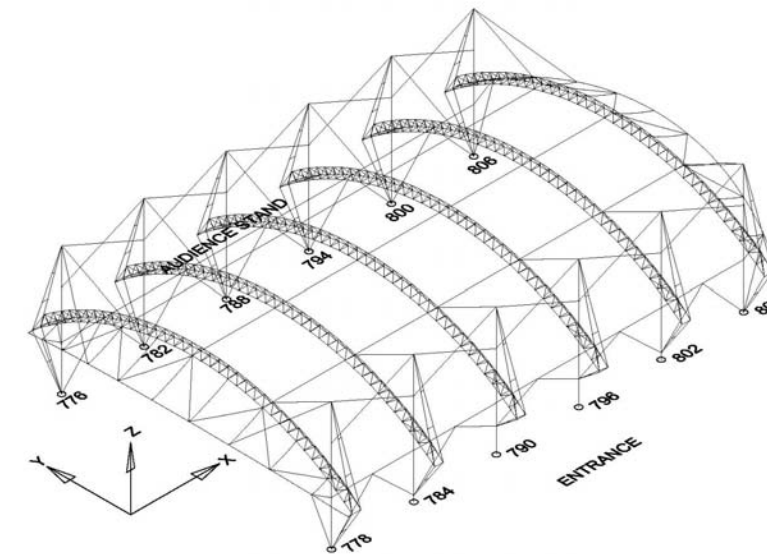
The design of the member sizes are based on the above load combination.

7.4. BOUNDARY CONDITION

The steel structure is supported on top of 12 nos of RC stump at spacing of 16.5m x 54m to each other. The mast base supports are assumed to be fixed condition which restrained in X, Y direction horizontally and Z direction vertically and also restrained in the X, Y and Z moment.



SUPPORT NODE NUMBER LAYOUT PLAN



SUPPORT NODE NUMBER 3D VIEW

7.5. DESIGN OF STEEL MEMBERS

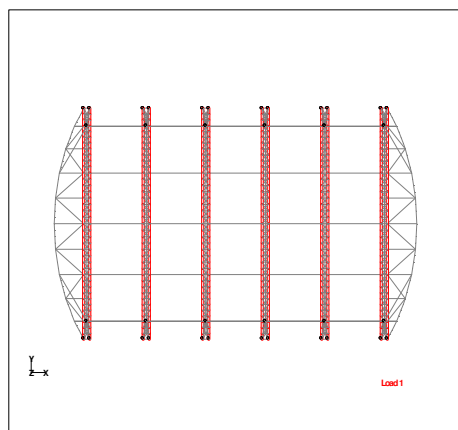
The design of the member size complied to BS5950 where the ultimate strength is used and the relevant load factor is applied to the imposed loading.

For deciding the correct pipe size for every member, compression will be the deciding factor and the compression capacity depends on the slenderness ratio (l/r) and the tension capacity only depends on the sectional area.

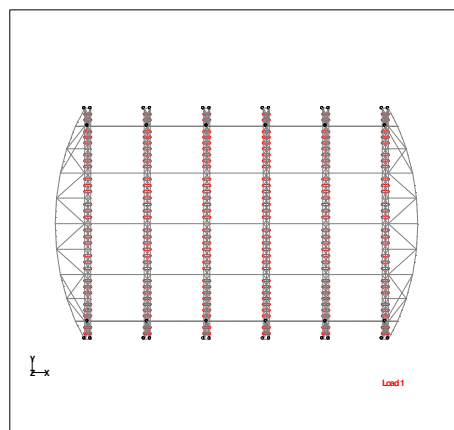
The final member size for individual member are determined from the worst force and moment from the ultimate load combination.

The software is able to check the sizes assigned based on the output from the worst load combination. The member sizes layout is attached for reference.

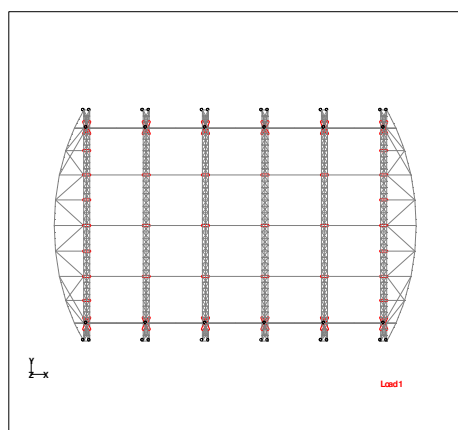
7.5.1 MEMBER SIZES LAYOUT



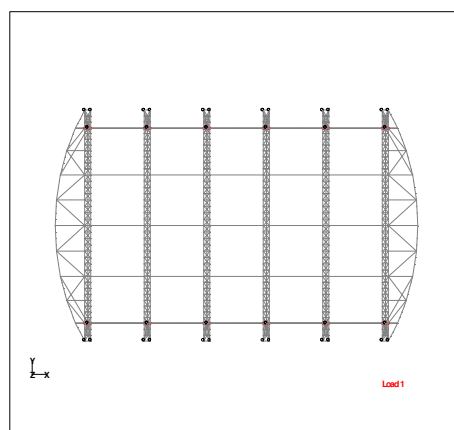
BOTTOM CURVED CHORD - 219Ø X 6



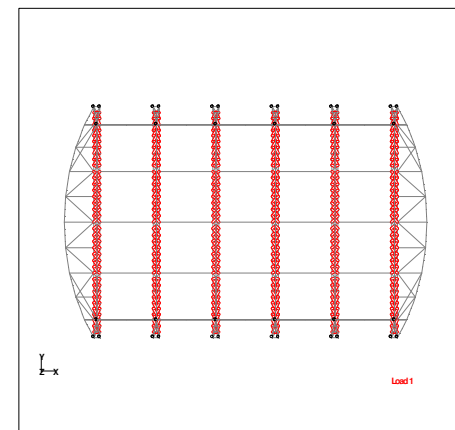
HORIZONTAL BOTTOM - 89Ø X 4



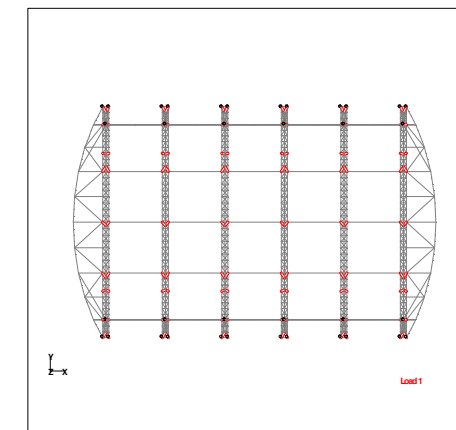
HORIZONTAL BOTTOM & DIAGONAL - 139Ø X 6



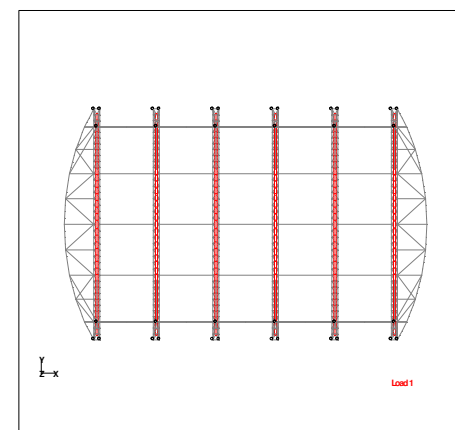
HORIZONTAL BOTTOM - 139Ø X 8



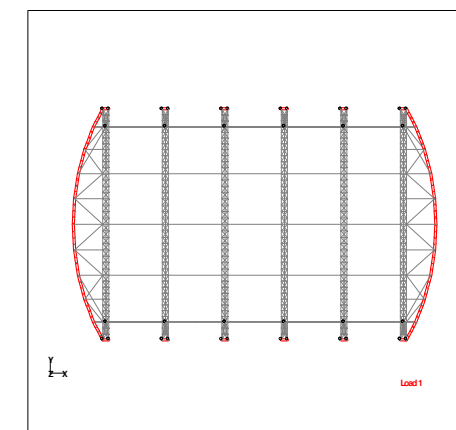
DIAGONAL - 89Ø X 4



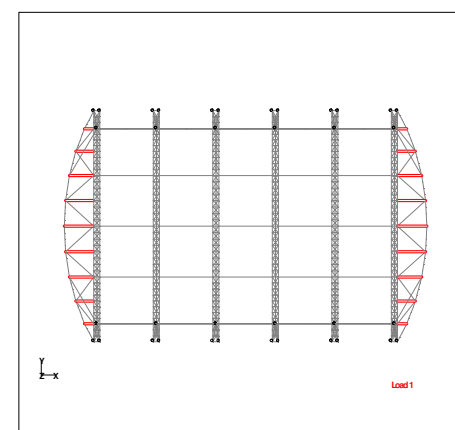
DIAGONAL - 114Ø X 4.5



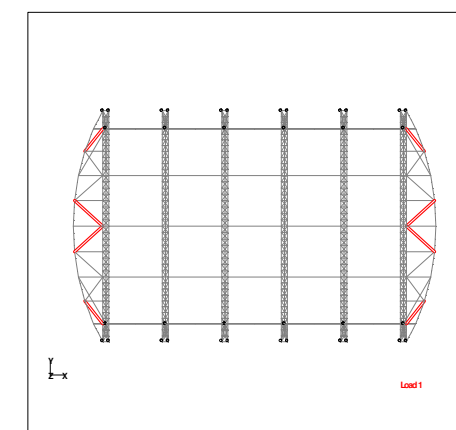
TOP CURVED CHORD - 219Ø X 6



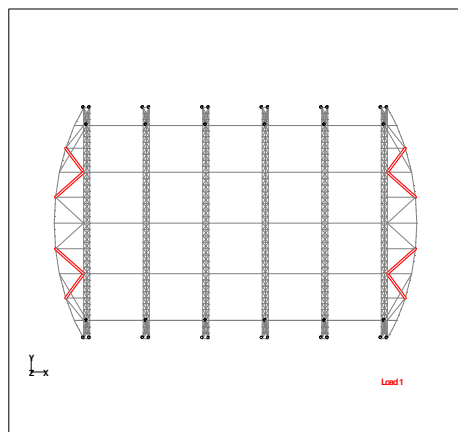
EDGE CHORD - 273Ø X 9.5



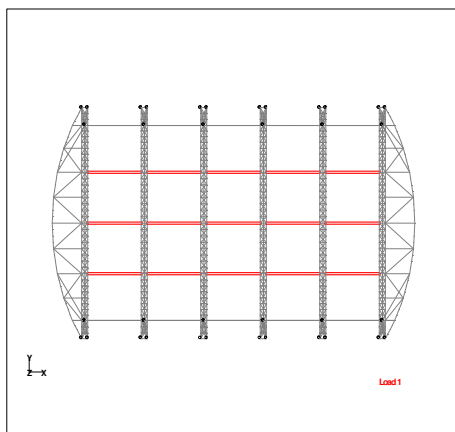
EDGE BRACE - 168.3Ø X 6



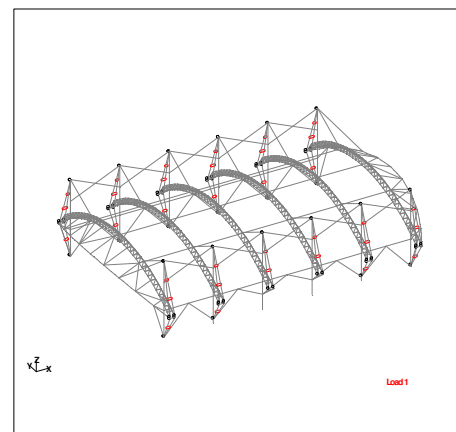
EDGE DIAGONAL BRACE - 168.3Ø X 10



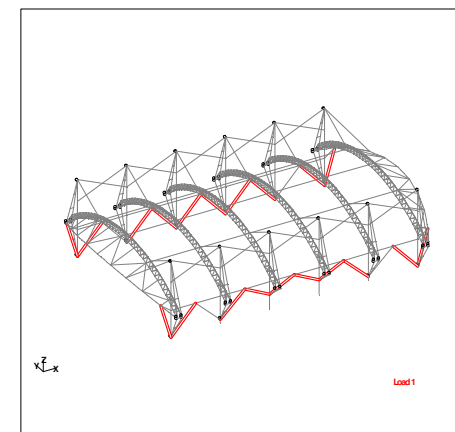
EDGE DIAGONAL BRACE – 168.3Ø X 8



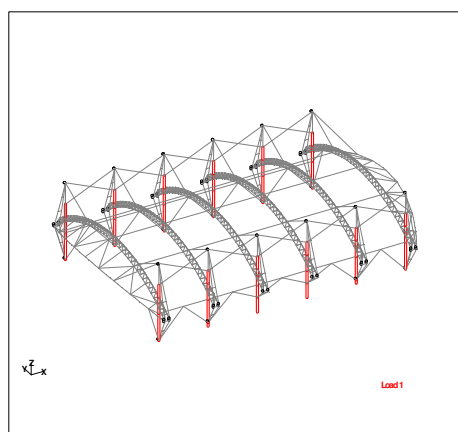
TIE BTW 3D TRUSS – 273Ø X 8



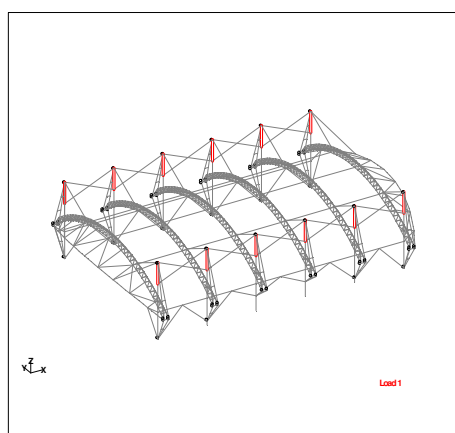
TIE BETWEEN MAST BACKSTAY – 73Ø X 5



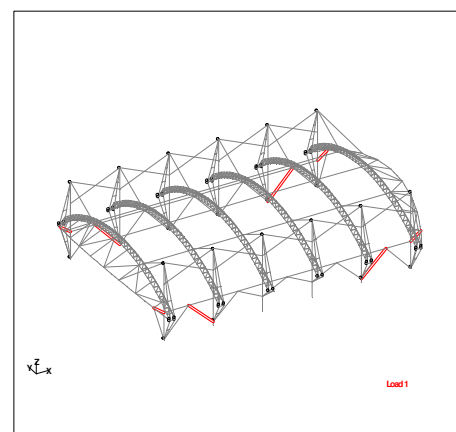
LONGITUDINAL BRACE – 219Ø X 6



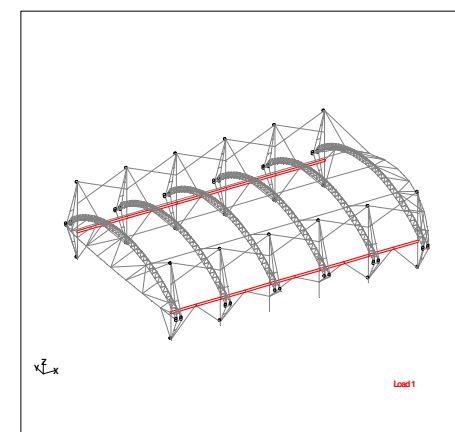
LOWER MAST – 609Ø X 16



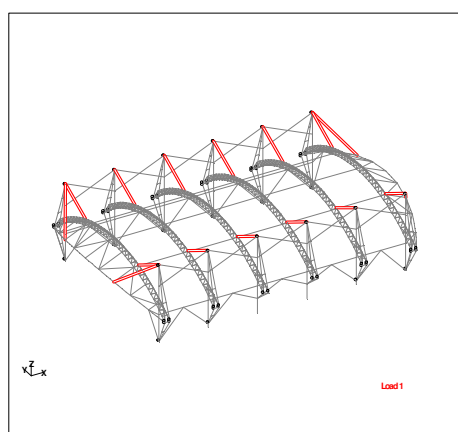
INTERMEDIATE MAST – 406.4Ø X 12.5



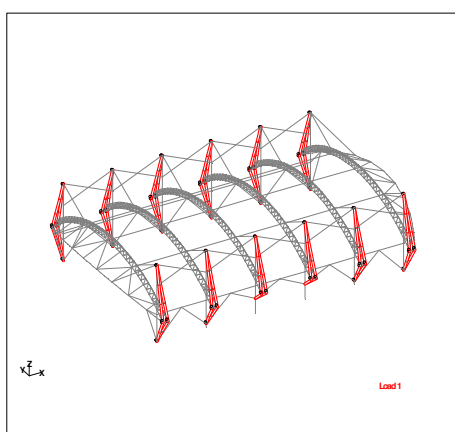
LONGITUDINAL BRACE – 219Ø X 9



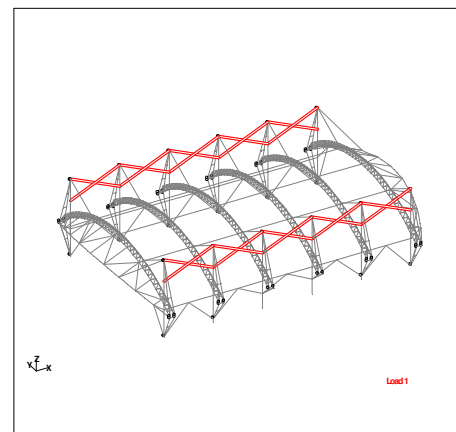
LONGITUDINAL TIE – 273Ø X 9



MAST FRONT STAY – 219Ø X 9



MAST BACKSTAY – 168Ø X 6



SAFETY CABLE BETWEEN MAST – 16Ø

7.6 LOCAL DESIGN CHECK

7.6.1 STABILIZING CABLE AT TOP OF MAST

From the steel structure analysis output,

maximum axial force = 30 KN

Proposed to use 16mm Ø 1x19 galvanized steel wire rope

Min breaking load = 211 KN >> 30 KN

Therefore is ok to use 16mm Ø wire rope.

7.6.2. HOLDING DOWN BOLTS

Reaction summary extracted from analysis output as shown,

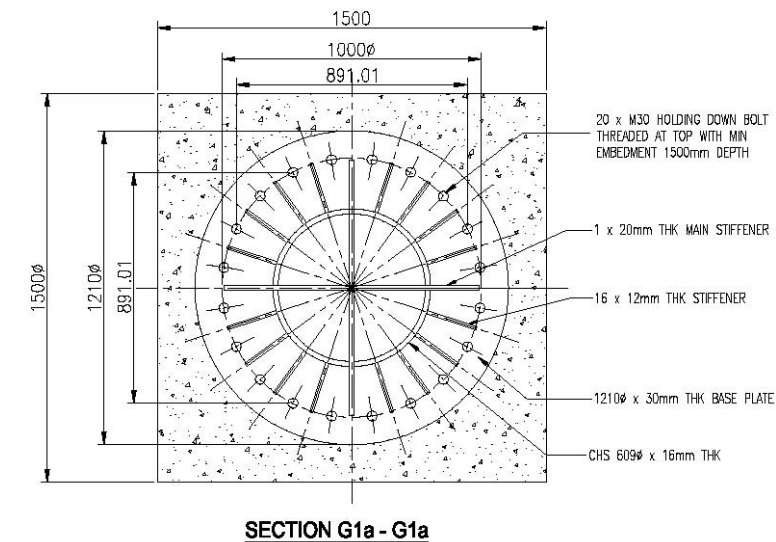
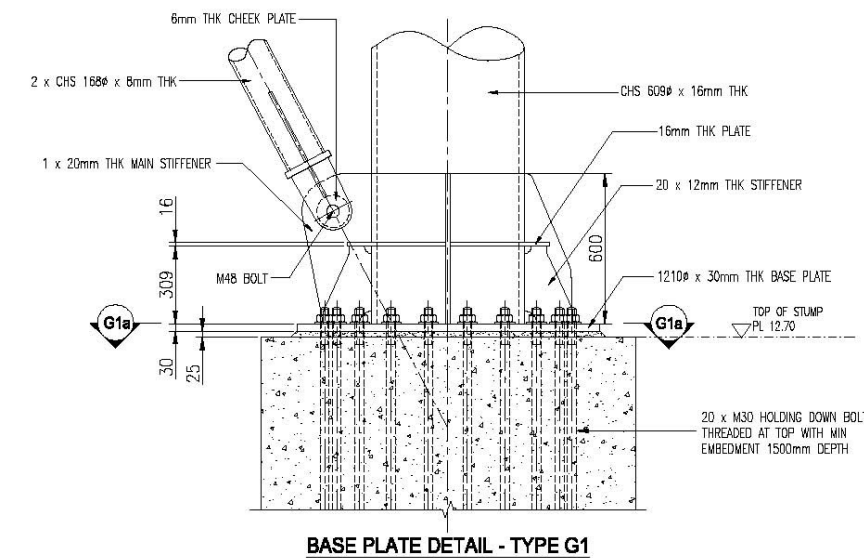
	Node	L/C	Horizontal		Vertical	Moment		
			FX (kN)	FY (kN)	FZ (kN)	MX (kNm)	MY (kNm)	MZ (kNm)
Max FX	800	208:1.2(SW+DCW)+1.2(WSB_P)	232.063	97.654	-23.855	-106.987	62.379	-22.129
Min FX	782	206:1.2(SW+DCW)+1.2(WDP_P)	-232.586	97.637	-23.505	-106.971	-60.596	20.386
Max FY	790	201:1.4(SW+DCW)+1.6(CDW+VL)	-13.887	228.469	507.055	-773.536	-39.192	3.081
Min FY	788	201:1.4(SW+DCW)+1.6(CDW+VL)	-26.716	-228.757	566.764	246.624	-4.373	-1.534
Max FZ	788	201:1.4(SW+DCW)+1.6(CDW+VL)	-26.716	-228.757	566.764	246.624	-4.373	-1.534
Min FZ	776	202:(SW+DCW)+1.4WU	-60.139	160.995	-333.775	-95.690	9.324	62.486
Max MX	788	204:1.2(SW+DCW)+1.2WEN	-42.971	-124.248	88.426	529.380	-7.790	-0.007
Min MX	790	201:1.4(SW+DCW)+1.6(CDW+VL)	-13.887	228.469	507.055	-773.536	-39.192	3.081
Max MY	802	208:1.2(SW+DCW)+1.2(WSB_P)	228.307	-97.765	13.935	171.829	278.833	22.013
Min MY	784	206:1.2(SW+DCW)+1.2(WDP_P)	-228.844	-97.713	14.756	171.682	-278.306	-19.787
Max MZ	808	208:1.2(SW+DCW)+1.2(WSB_P)	63.227	34.256	-60.780	-87.560	-27.936	124.287
Min MZ	806	208:1.2(SW+DCW)+1.2(WSB_P)	63.709	-34.308	-65.863	89.498	-29.237	-124.972

From the reaction forces summary output, max reaction forces are;

$F_x = 233 / -233 \text{ KN}$ $M_x = 530 / -774 \text{ KNm}$
 $F_y = 229 / -229 \text{ KN}$ $M_y = 279 / -279 \text{ KNm}$
 $F_z = 567 / -334 \text{ KN}$ $M_z = 125 / -125 \text{ KNm}$

Note : +ve Fz is the compression and -ve Fz is the tensile force

Proposed 20 x M30 grade 8.8 in a circular arrangement at 1m diameter, and assumed only 4 bolts on each side at 0.89m apart are resisting;



$$F_t \text{ due to } M_x \text{ per bolt} = 774 / (4 \times 0.89) = 217.4 \text{ KN}$$

$$\text{Direct } F_t \text{ per bolt} = 334 / 20 = 16.7 \text{ KN}$$

$$\text{Total tensile per bolt } F_t = 217.4 + 16.7 = 234.1 \text{ KN}$$

$$F_s \text{ due to } M_z \text{ per bolt} = 125 / (4 \times 0.89) = 35.1 \text{ KN}$$

$$\text{Direct } F_s \text{ per bolt} = (233^2 + 229^2)^{1/2} / 20 = 16.3 \text{ KN}$$

$$\text{Total } F_s \text{ per bolt} = 35.1 + 16.3 = 51.4 \text{ KN}$$

$$\text{Tensile strength of Grade 8.8 bolt} = 450 \text{ N/mm}^2$$

$$\text{Shear strength of Grade 8.8 bolt} = 375 \text{ N/mm}^2$$

$$f_t = 234.1 \times 3 / 561 = 417 \text{ N/mm}^2 < 450 \text{ N/mm}^2 \text{ OK}$$

$$f_s = 51.4 \times 3 / 561 = 92 \text{ N/mm}^2 < 375 \text{ N/mm}^2 \text{ OK}$$

$$\text{Combined stress check,}$$

$$417/450 + 92/375 = 1.172 < 1.4 \text{ OK}$$

7.6.2.1 Embedment length check,

$$f_{bu} = \beta (f_{cu})^{1/2}$$

Where f_{bu} = design ultimate anchorage bond stress
 β = 0.28 for plain bar
 f_{cu} = 35 N/mm² for concrete grade

$$f_{bu} = 0.28 (35)^{1/2} = 1.656$$

$$\text{anchorage force} / (\pi \times \phi \times L) = f_{bu}$$

$$\begin{aligned} \text{embedment length } L &= \text{anchorage force} / (\pi \times \phi \times f_{bu}) \\ &= 234.1 \times 10^3 / (\pi \times 30 \times 1.656) \\ &= 1500 \text{ mm} \end{aligned}$$

Therefore provide minimum 1500mm embedment length is OK.

7.6.2.2 Base plate thickness check

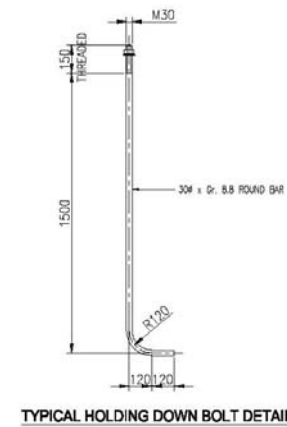
Assumed the plate is bend in double curvature over the width of 590mm for 4 bolts and ignored the 16mm and 20mm thk stiffener plate,

$$M = 234.1 \times (1.0 - 0.609) / 2 \times 1/2 = 22.88 \text{ KNm}$$

$$Z_{\text{provide}} = 1/6 \times 590 \times 30^2 = 88500 \text{ mm}^3$$

$$f_b = 22.88 \times 10^6 / 88500 = 258 \text{ N/mm}^2 < 275 \text{ N/mm}^2 \text{ OK}$$

Therefore use 30mm thk base plate with stiffener plate is OK.

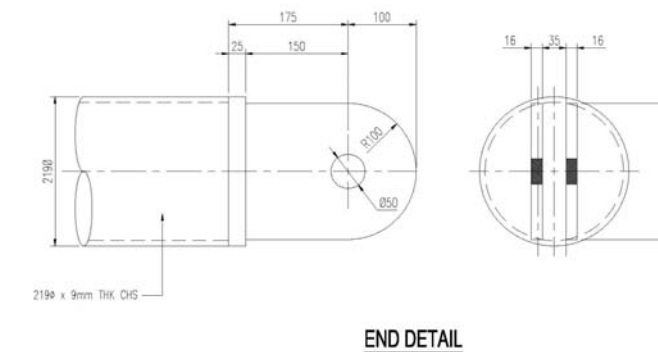


TYPICAL HOLDING DOWN BOLT DETAIL

7.6.3 DESIGN OF PIN CONNECTIONS

7.6.3.1 MAST FRONT HANGER

Max axial force as extracted from analysis output = 217 KN



END DETAIL

Proposed to use 1 x M48 grade 8.8 bolt with 16mm thick tongue plate,

Tensile strength of Grade 8.8 bolt = 450 N/mm²

Shear strength of Grade 8.8 bolt = 375 N/mm²

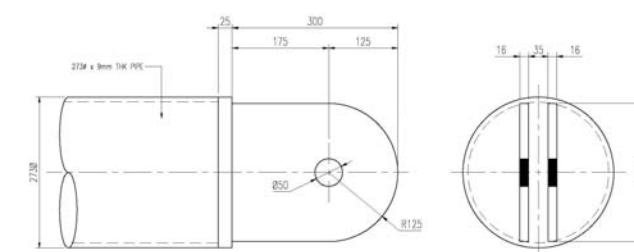
$$f_s = [(217/2 \times 10^3)] / 1470 = 74 \text{ N/mm}^2 < 375 \text{ N/mm}^2 \text{ OK}$$

$$\begin{aligned} \text{bearing stress of tongue plate, } f_{bs} &= [(217/2) \times 10^3] / (48 \times 16) \\ &= 141 \text{ N/mm}^2 < 460 \text{ N/mm}^2 \text{ OK} \end{aligned}$$

Where 460 N/mm² is the bearing strength for S275 plate.

7.6.3.2 TIE BETWEEN 3D TRUSS

Max axial force as extracted from analysis output = 323 KN



END PLATE FOR 2730 PIPE

Proposed to use 1 x M48 grade 8.8 bolt with 16mm thick tongue plate,

Tensile strength of Grade 8.8 bolt = 450 N/mm²

Shear strength of Grade 8.8 bolt = 375 N/mm²

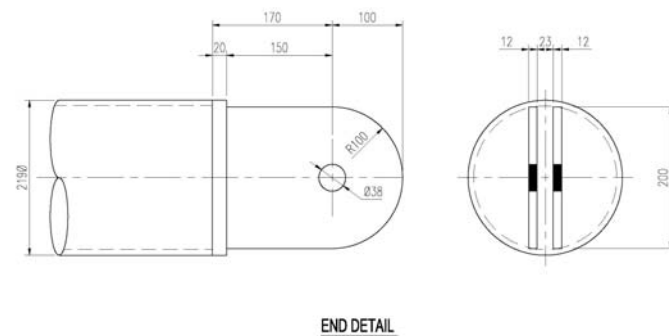
$$f_s = [(323/2) \times 10^3] / 1470 = 110 \text{ N/mm}^2 < 375 \text{ N/mm}^2 \text{ OK}$$

$$\begin{aligned} \text{bearing stress of tongue plate, } f_{bs} &= [(323/2) \times 10^3] / (48 \times 16) \\ &= 210 \text{ N/mm}^2 < 460 \text{ N/mm}^2 \text{ OK} \end{aligned}$$

Where 460 N/mm^2 is the bearing strength for S275 plate.

7.6.3.3 BRACE AT LOWER MAST

Max axial force as extracted from analysis output = 365 KN



Proposed to use 1 x M36 grade 8.8 bolt with 12mm thick tongue plate,

Tensile strength of Grade 8.8 bolt = 450 N/mm^2

Shear strength of Grade 8.8 bolt = 375 N/mm^2

$$f_s = [(365/2) \times 10^3] / 817 = 224 \text{ N/mm}^2 < 375 \text{ N/mm}^2 \text{ OK}$$

$$\begin{aligned} \text{bearing stress of tongue plate, } f_{bs} &= [(365/2) \times 10^3] / (36 \times 12) \\ &= 422 \text{ N/mm}^2 < 460 \text{ N/mm}^2 \text{ OK} \end{aligned}$$

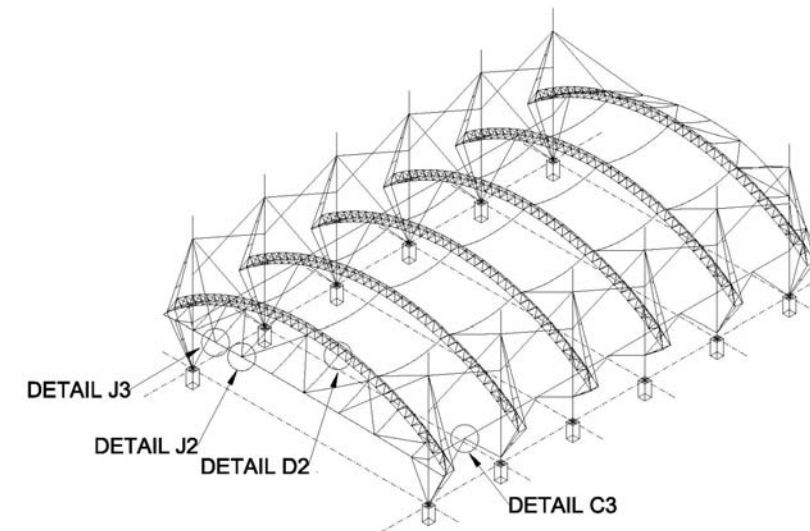
Where 460 N/mm^2 is the bearing strength for S275 plate.

7.6.4 PLATE CONNECTION TO CHS

For the tensile structure, there is a lot of connection with plate welded to circular hollow section for fixing of fabric, for bolting of bracing member and etc. To check the influences of forces to these plate and main member is quite complex, so a finite element model (FEM) is done for some typical connection to verify the von mises stresses or equivalent stress is not to exceed the yield stress of main member and plates.

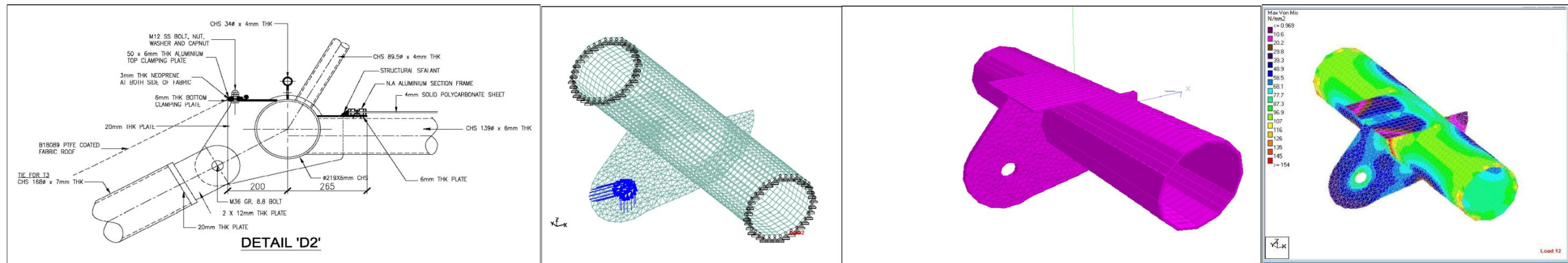
The von mises stress shall not exceed 90% of the material yield stress. Therefore the connection stresses shall not exceed $0.9 \times 275 \text{ N/mm}^2 = 247.5 \text{ N/mm}^2$

Extract 4 finite element model done at four connections as shown and attached for information. And max von mises stress is 237 N/mm^2 at Detail J2.



KEY PLAN FOR CONNECTION DESIGN

7.6.4.1 JOINT AT 3D TRUSS BOTTOM CHORD TO EDGE FRAME BRACE MEMBER



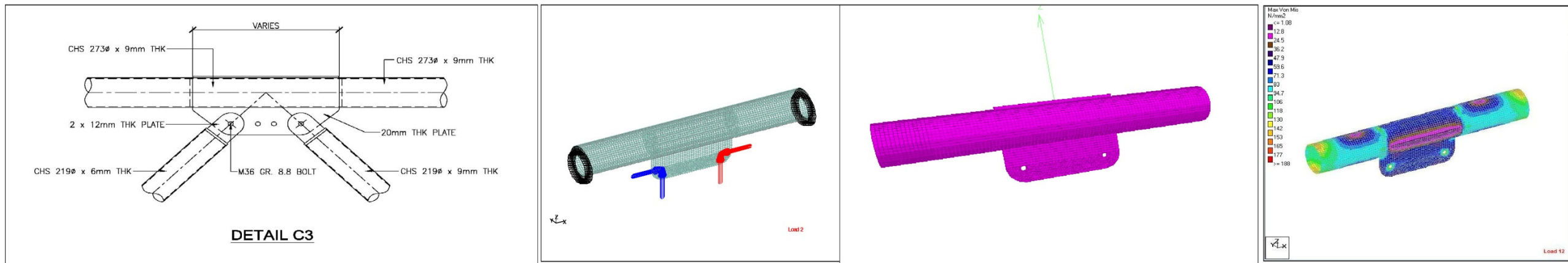
INFORMATION ON THE JOINT

FEM WITH FORCE @ BOLT HOLE

3D RENDERED

MAX VON MISES OUTPUT

7.6.4.2 JOINT AT LOWER MAST HORIZONTAL TIE & BRACE MEMBER



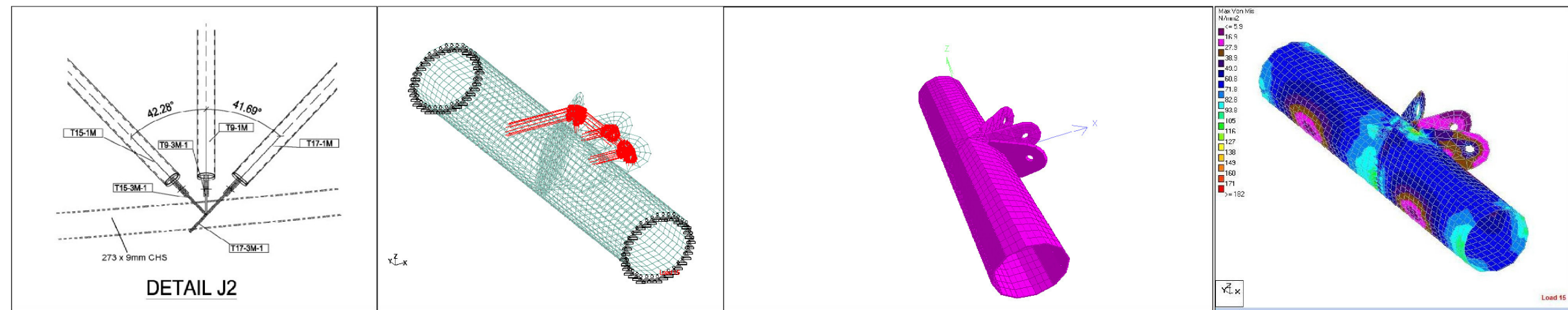
INFORMATION ON THE JOINT

FEM WITH FORCES @ BOLT HOLES

3D RENDERED

MAX VON MISES OUTPUT

7.6.4.3 JOINT AT EDGE FRAME WITH 3 BRACE MEMBER



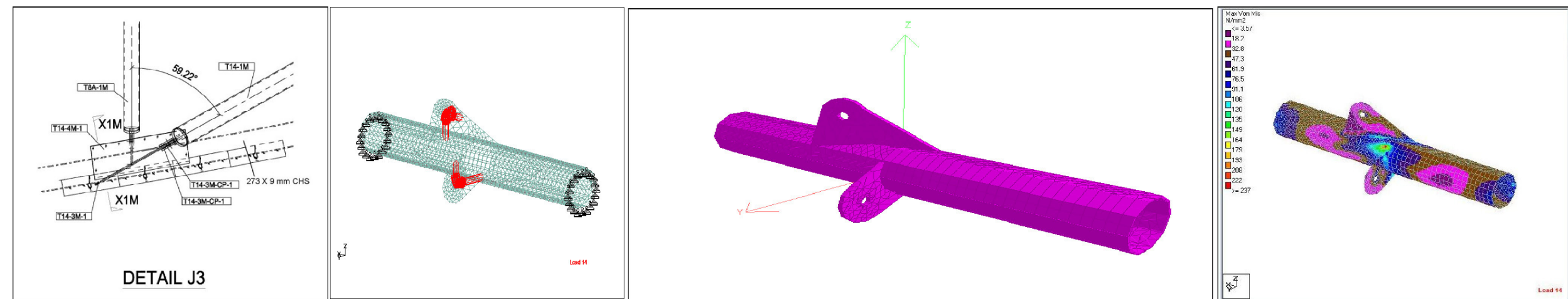
INFORMATION ON THE JOINT

FEM WITH FORCES

3D RENDERED

MAX VON MISES OUTPUT

7.6.4.4 JOINT AT FRONT HANGAR TO EDGE FRAME WITH BRACE MEMBER



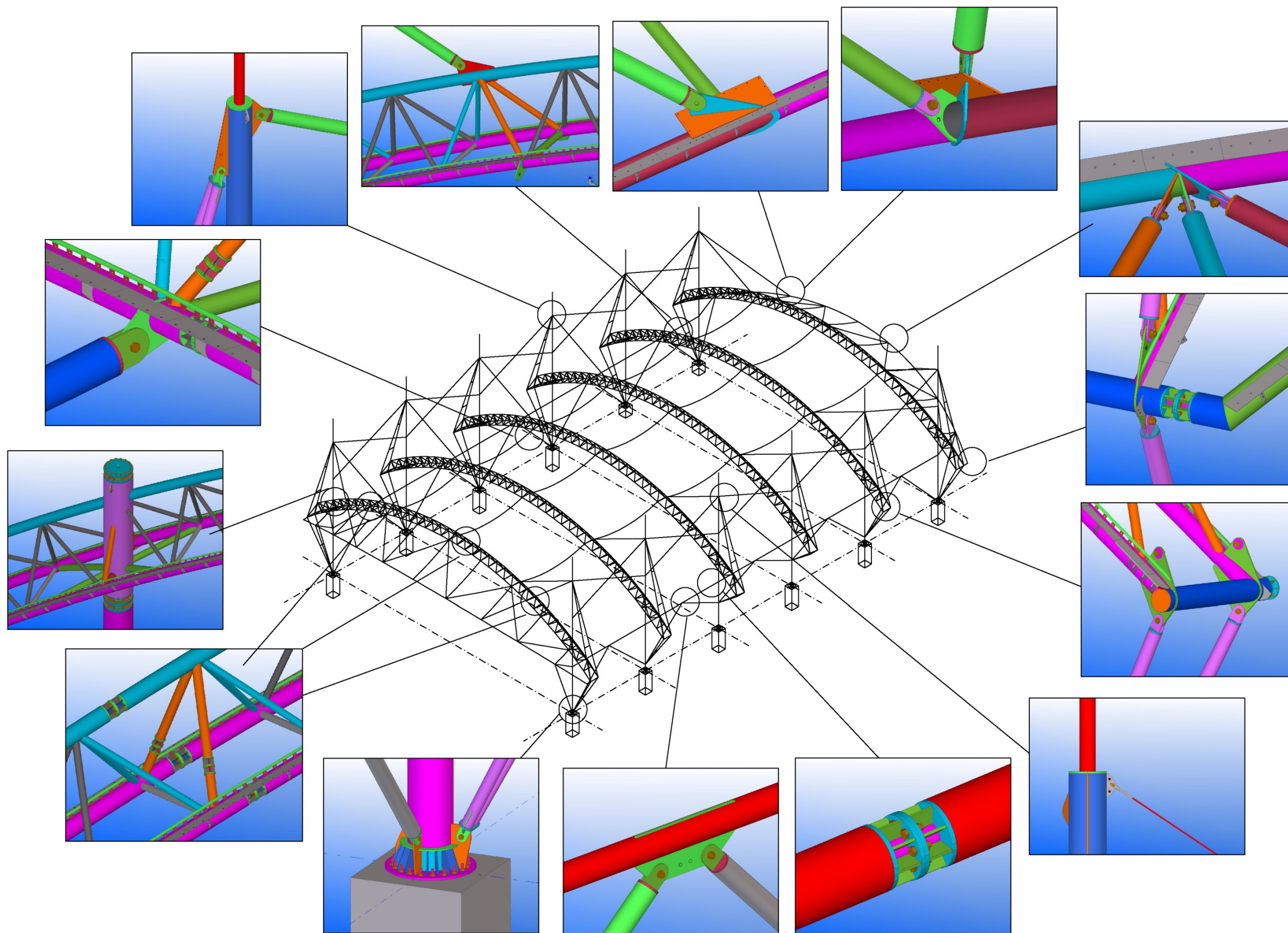
INFORMATION ON THE JOINT

FEM WITH FORCES

3D RENDERED

MAX VON MISES OUTPUT

7.7 SUMMARY OF CONNECTION DETAILS



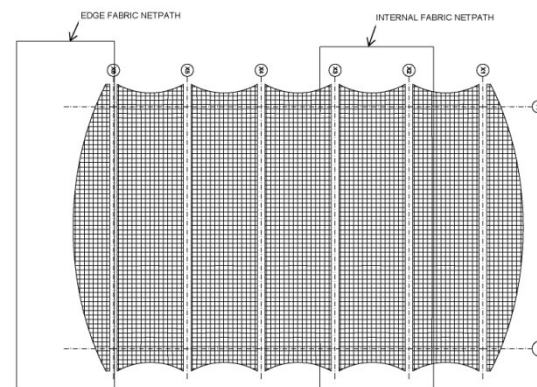
8. MEMBRANE ANALYSIS AND DESIGN

8.1 GENERAL INFORMATION

The fabric material is represented by a network of mesh formed by membrane link represented by segment of lines. For membrane design, firstly is to do a form finding to study the feasibility of the proposed shape with assumed material type and sizes. Secondly is to study the proposal when various loading is applied onto the stable form and check for the displacement and stresses in the membrane for all possible load combination and not forgetting to make sure the proposed form will not have any water ponding possibility. And lastly is to do a cutting pattern based on the available width of proposed fabric used with compensation value adopted from the result of the biaxial test and also typical production practice ie seam width and pocket allowance. And then finally the individual pattern can then be used for production.

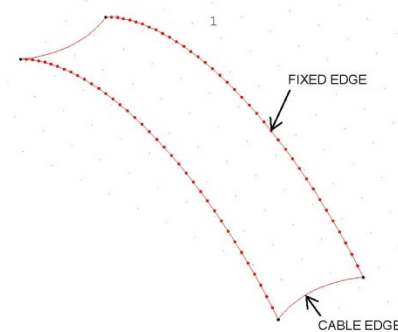
8.2 FORM FINDING

8.2.1) To identify the different netpath for the project and for the shape of this structure, there is only 2 type of netpath ie the internal panel and the edge panel as shown.

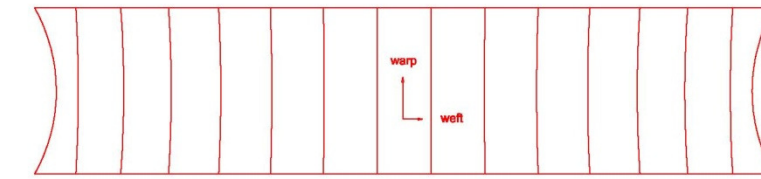


8.2.2) Prepare the boundary in cad program and then import into EASY and assign sag ratio to the cable edge and radius or sag ratio for the curved beam. Check the fixity of the boundary points for form find and also for static analysis.

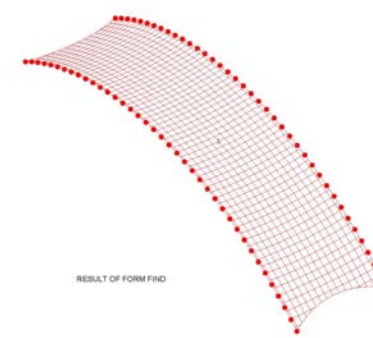
In this case, the sag ratio used is 12.5% for the border cable edge and 18% or 50m radius for the curved fixing edge.



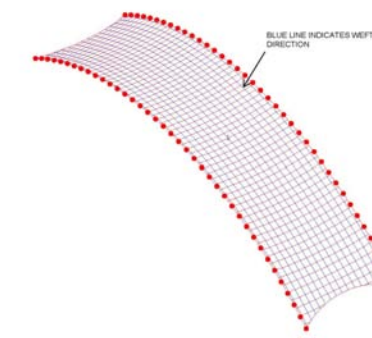
8.2.3) Then form find based on the assigned value. The warp and weft direction have to be decided based on the intended cutting pattern configuration as these will affect the static analysis result later.



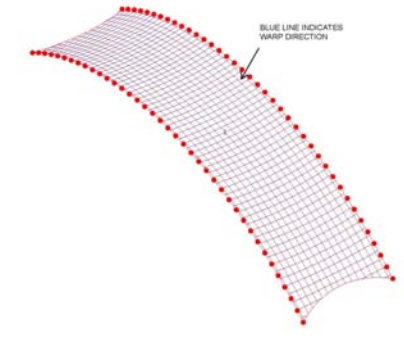
PROPOSED CUTTING PATTERN LAYOUT



Result of form finding



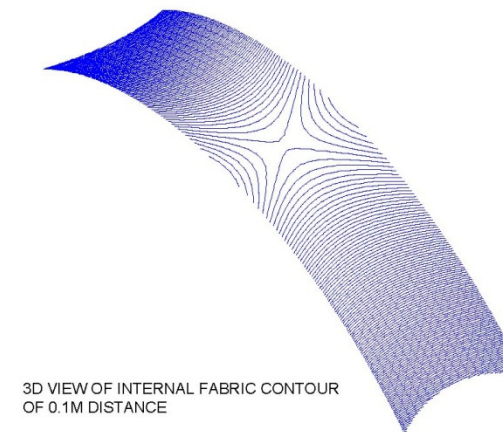
Weft is along the curved edge



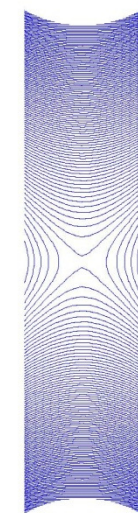
Ward is across curve edge

8.3 CONTOUR

A contour line of 0.1m is plotted and it show there will not be any water stagnate problem due to the shape of the structure.



3D VIEW OF INTERNAL FABRIC CONTOUR OF 0.1M DISTANCE

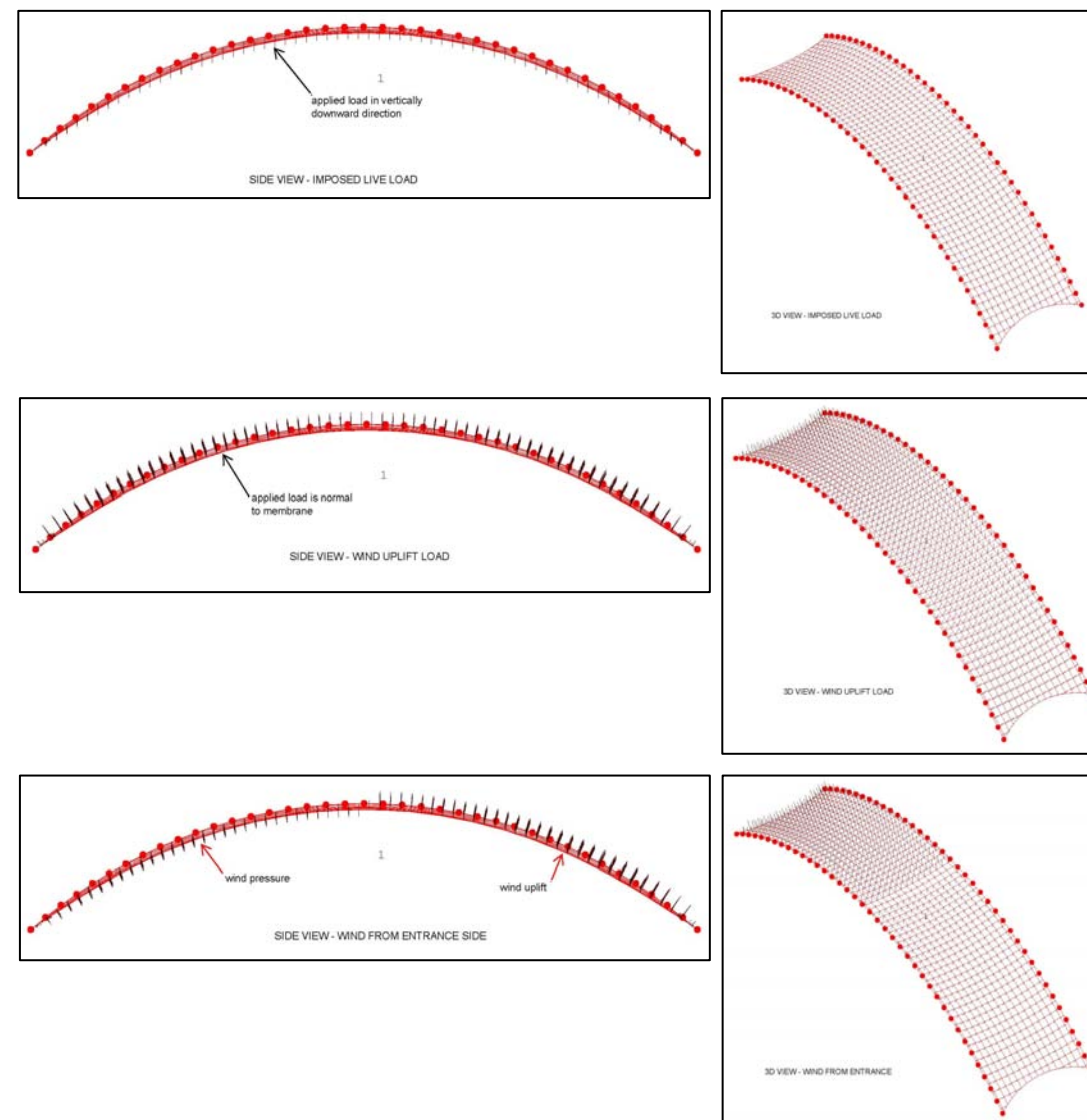


PLAN VIEW OF INTERNAL FABRIC CONTOUR OF 0.1M DISTANCE

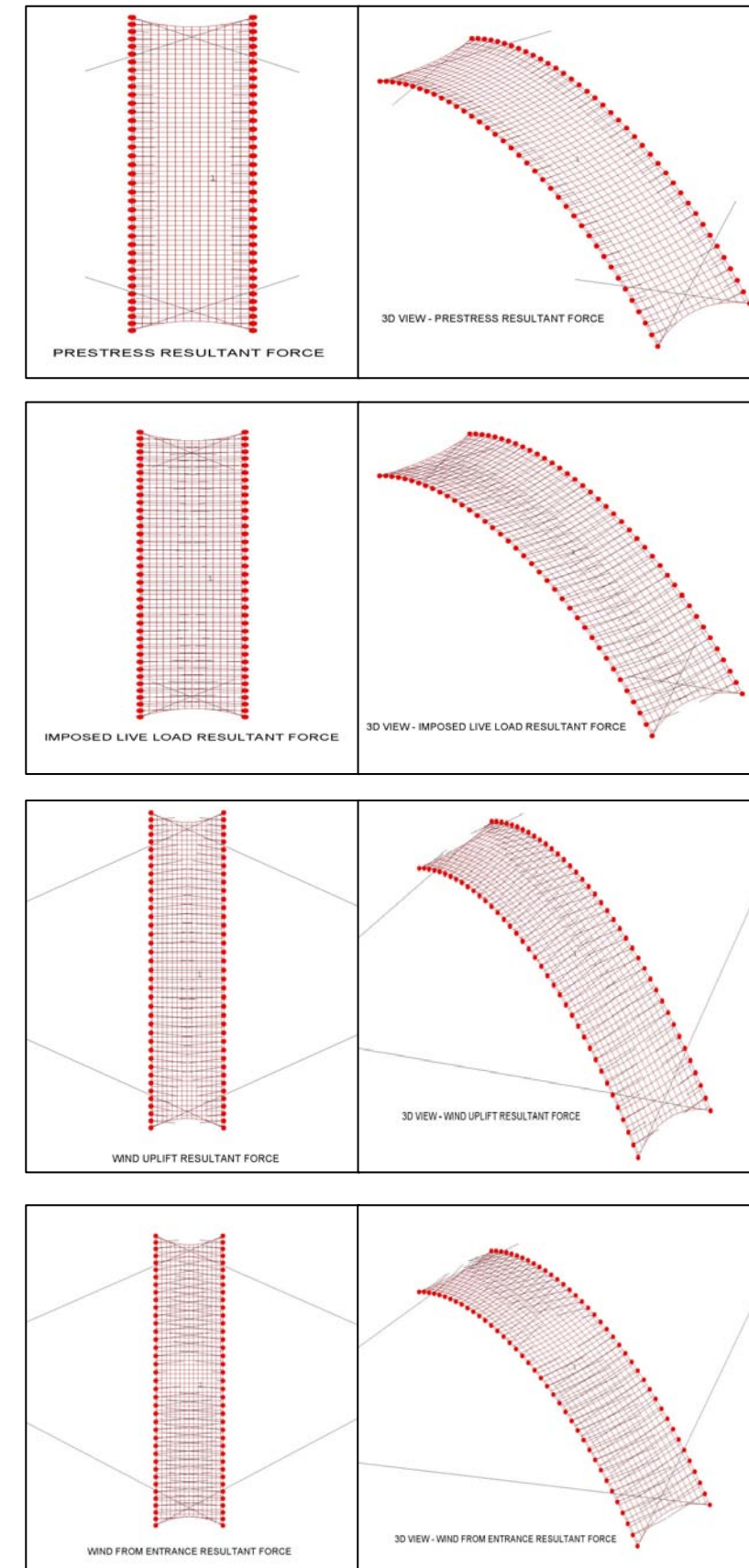
8.4 LOADING AND STATIC ANALYSIS

8.4.1) Assumed a prestress force for the final form and load the form with the calculated various loading ie. wind load or live load by creating load case. A prestress force of 3 KN/m for warp and weft is adopted for this project.

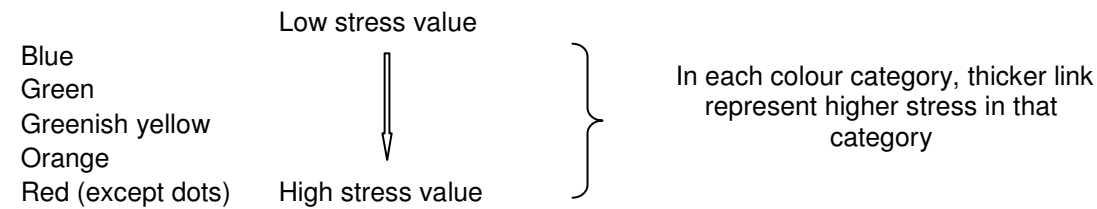
The surface load is applied as nodal load to the nodes in the mesh. And all wind load are applied normal to the membrane surface, except the imposed live load which is vertically to the surface of the membrane. Extract some applied load diagram for reference.



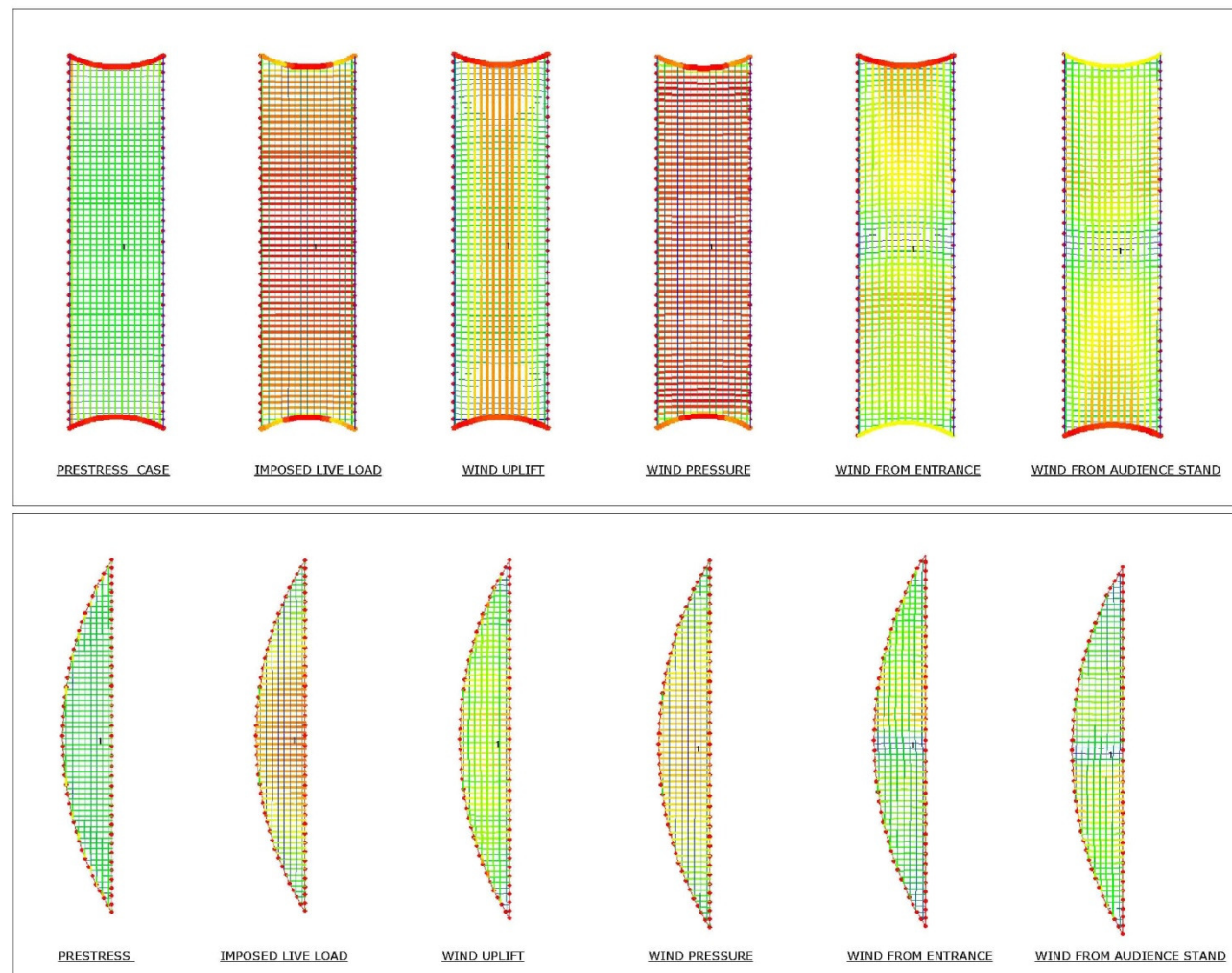
8.4.2) Then view the analysis results ie reactions at the fixing point. These are the forces that are then extract and apply to the steel structure.



8.4.3) To perform static structural analysis, correct stiffness value have to assumed for the membrane link. In this case, 2000 and 1000 is assumed for warp and weft membrane links and 5000 assumed for cable link. Upon completion of the analysis of a typical load cases, there will be a stressed pattern shown in these membrane link. The magnitude of stresses is expressed in colour as well as width of membrane link in the following order,



Red dots seen in any stress pattern represent fixed point of fabric for design analysis. For each load case, there will be a overall stress pattern shown where the highest stressed area can be located. The following membrane stress value are not shown for clarity.



8.5 LOCAL DESIGN CHECK

8.5.1 MEMBRANE

Summary of Membrane Stress and Border Cable Force

Load Case	Membrane Link Stress		Cable Link Force
	Critical Low	Critical High	Critical High
Internal Fabric			
Prestress	2.224	5.056	42
Imposed Live	1.005	9.045	18
Wind Uplift	3.056	24.144	231
Wind Pressure	0.896	10.464	32
Wind from Entrance	1.923	17.307	165
Wind from Grandstand	1.953	17.577	168
Edge Fabric			
Prestress	2.442	5.098	-
Imposed Live	1.67	8.47	-
Wind Uplift	4.176	15.424	-
Wind Pressure	1.433	11.137	-
Wind from Entrance	3.132	15.948	-
Wind from Grandstand	3.214	15.886	-

From the tabulated summary, the max membrane stress is 24 KN/m from wind uplift case.

From the technical data of B18089 from Verseidag, ,

Tensile strength (N/5cm) warp/ weft = 7000 / 6000

And the max stress is along the weft direction, = 120 KN/m

$$\text{Safety factor} = 120 / 24 = 5.0$$

Therefore the chosen membrane is ok to use for this span.

8.5.2 BORDER CABLE

From the tabulated summary, the max cable force is 231KN from wind uplift case.

Proposed to use 28mm Ø 6 x 37 IWRC galvanized steel ire rope,

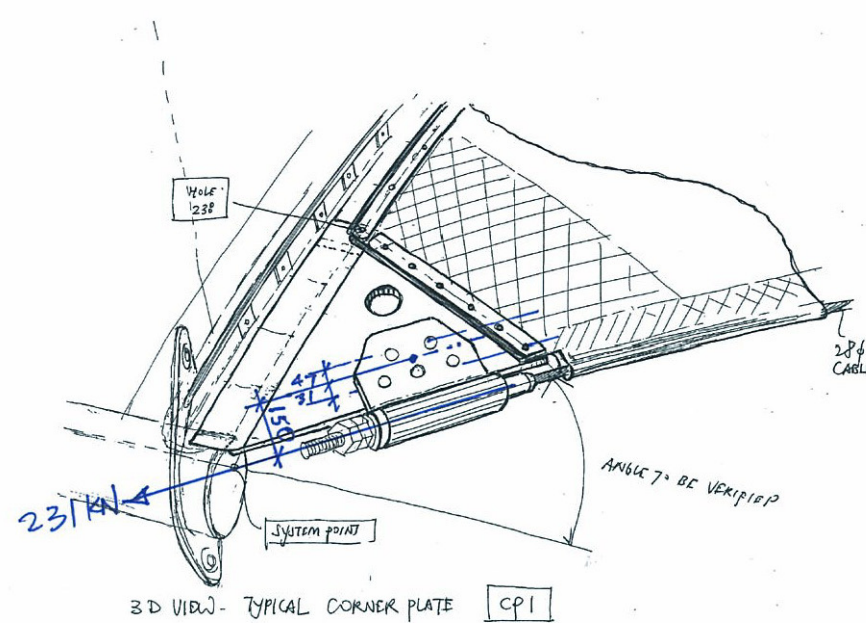
Min breaking load = 49600 kg = 506 KN

$$\text{Safety factor} = 506 / 231 = 2.2$$

Therefore is ok to use 28mm Ø wire rope.



8.5.3 CORNER PLATE



The 28mm diameter border cable is fix on to a double layer 16mm thk 'burger' welded to 89 ϕ x 11.3mm thk x 300mm long pipe section.

Max border cable force = 231 KN (unfactored load)
Assumed load factor of 1.4 due to wind uplift, $F = 231 \times 1.4 = 323.4$ KN

Center of group of 5 x M36 G8.8 bolts to center of cable fitting = 155mm
Moment due to cable force, $M = 323.4 \times 0.155 = 50$ KNm

This moment is to resist by the 5 bolts about the center of bolts in shear force F_s ,

Therefore $2 F_s \times 0.047 = 50$ KNm
 F_s due to moment = $50 / (2 \times 0.047) = 532$ KN

Or $3 F_s \times 0.031 = 50$ KNm
 F_s due to moment = $50 / (3 \times 0.031) = 538$ KN

Direct shear force per bolt = $323.4 / 5 = 64.7$ KN
Therefore maximum shear force per bolt = $538 + 64.7 = 602.7$ KN

Proposed to use 5 x M36 grade 8.8 bolt with 16mm thick double plate,

Tensile strength of Grade 8.8 bolt = 450 N/mm²
Shear strength of Grade 8.8 bolt = 375 N/mm²

$f_s = [(602.7 / 2) \times 10^3] / 817 = 369$ N/mm² < 375 N/mm² OK

bearing stress of the double 'burger' plate, $f_{bs} = [(602.7 / 2) \times 10^3] / (36 \times 16) = 523$ N/mm² < 550 N/mm² OK

Where 550 N/mm² is the bearing strength for S355 plate.

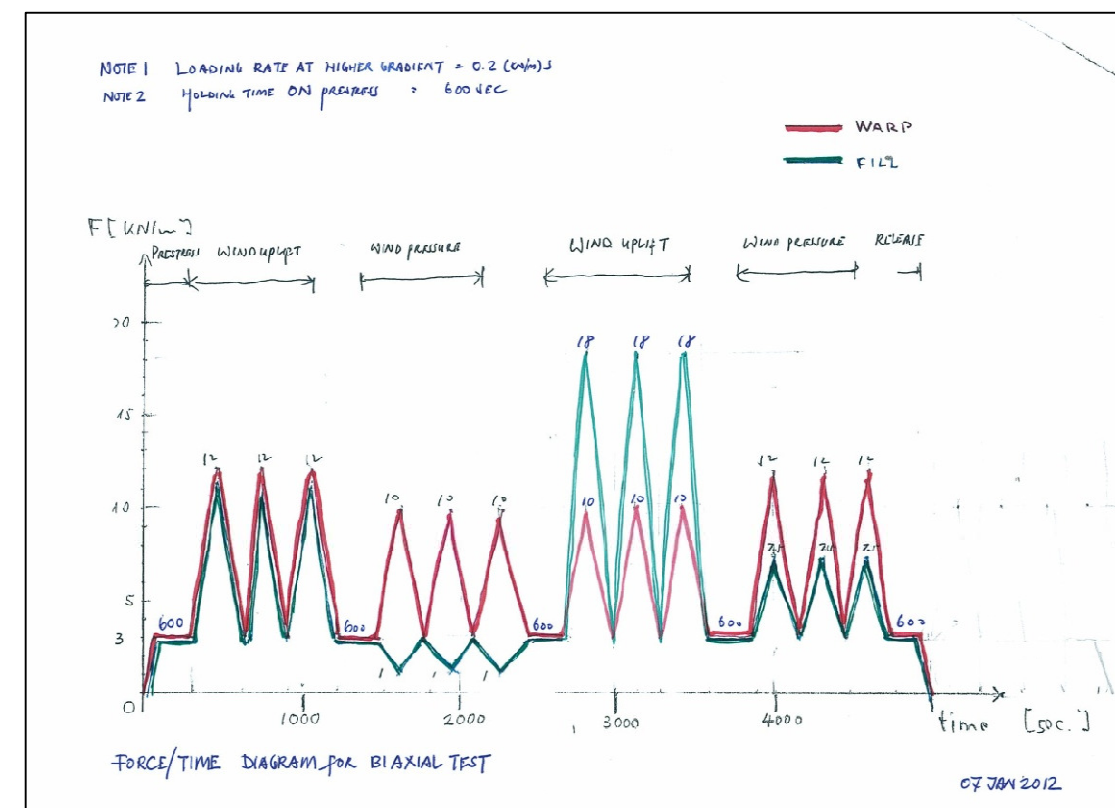
8.6 BIAXIAL TEST

From the membrane stress pattern, a suitable value is decided for carry out the biaxial test. In this case, a value of about 70% of the maximum stress is used for various load case is tabulated as follow. And the test is carried out by University of Essen, Germany.

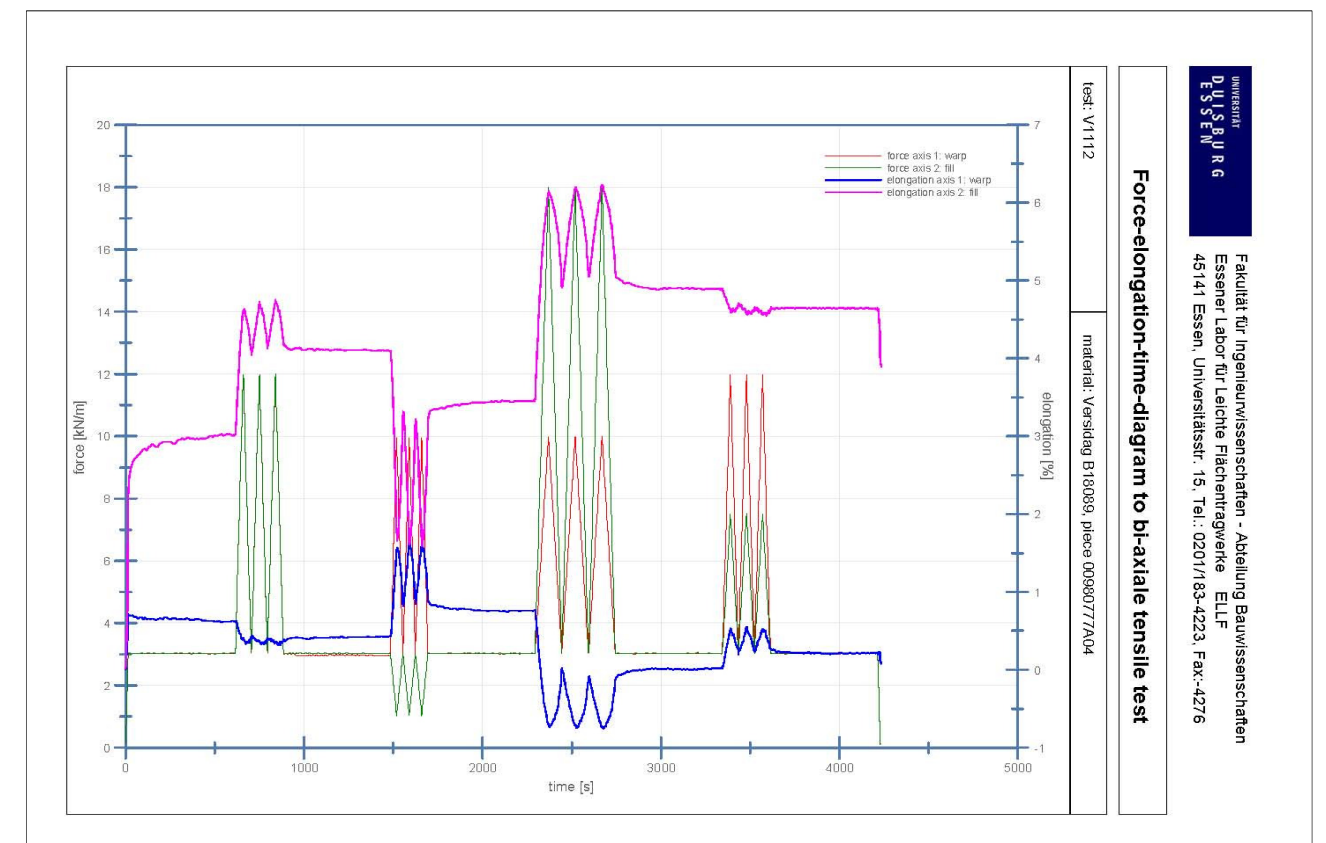
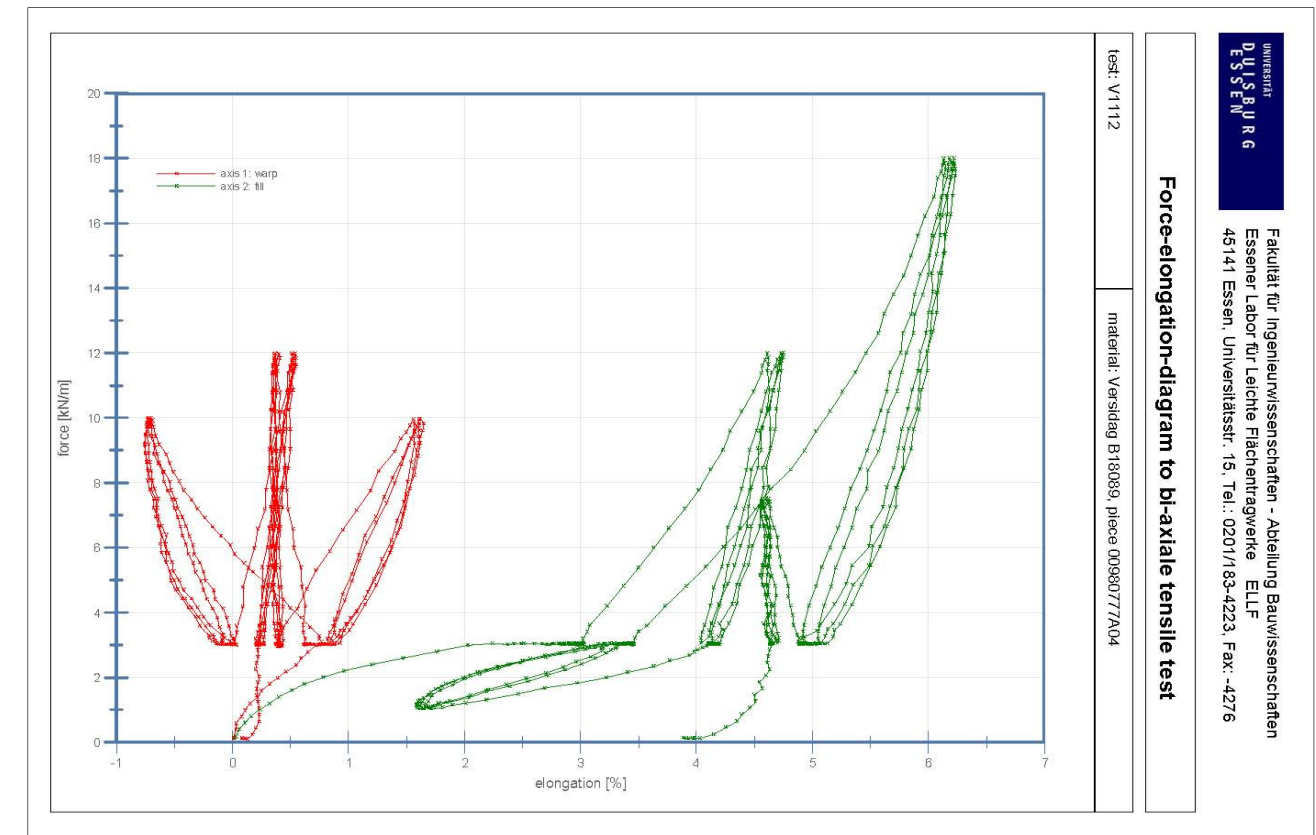
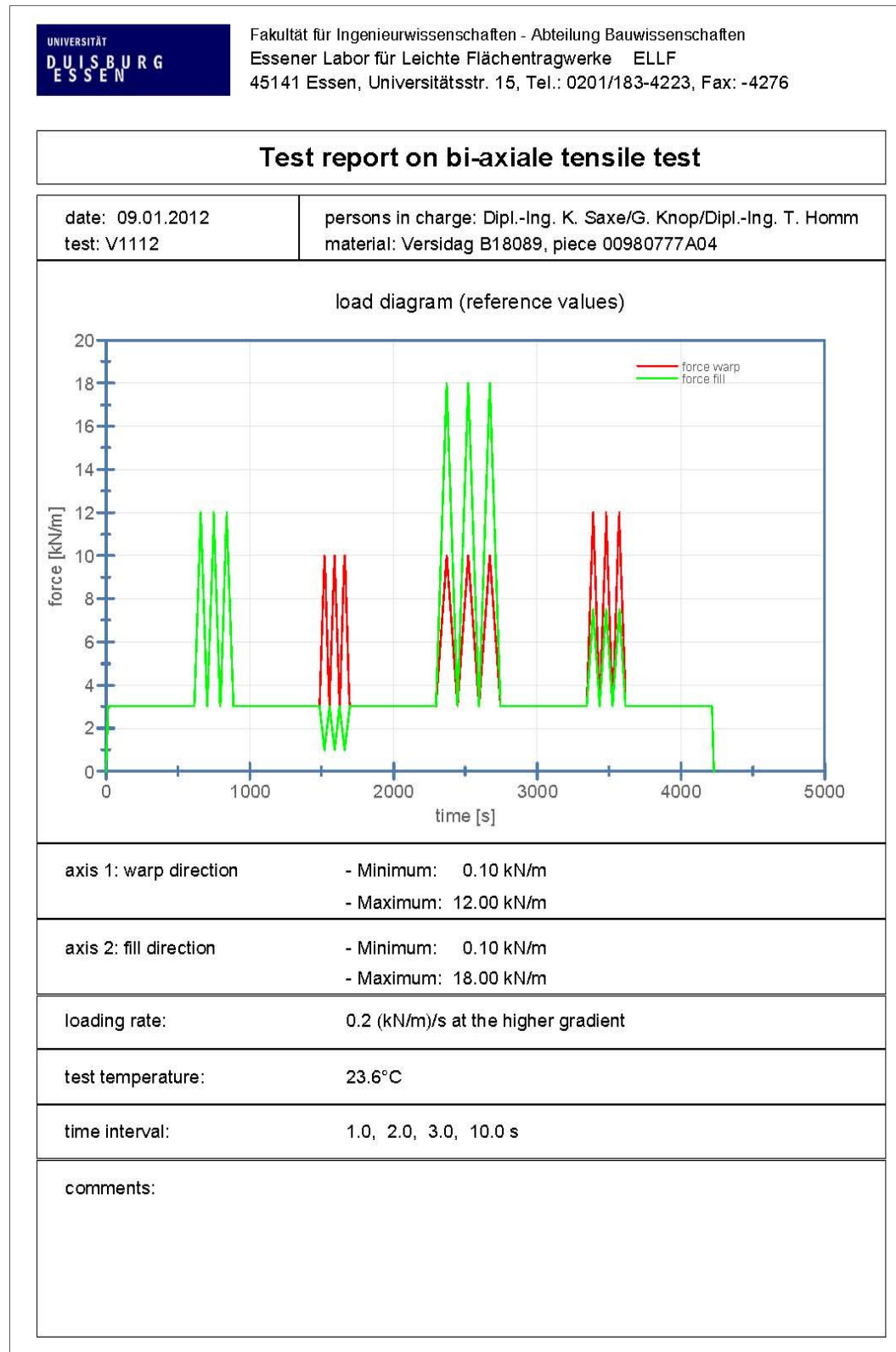
These values are extracted from the membrane analysis based on wind speed of 38 m/s which is later revised to 32 m/s in the final design.

S/N	LOAD CASE	WARP DIRECTION (KN/m)	WEFT DIRECTION (KN/m)
1	PRESTRESS	3.0	3.0
2	VERTICAL LIVE LOAD	7.5	1.4
3	WIND PRESSURE	10.0	1.0
4	WIND UPLIFT	10.0	18.0
5	WIND UPRESSURE + UPLIFT		
	PRESSURE SIDE	12.0	7.5
	UPLIFTSIDE	12.0	12.0

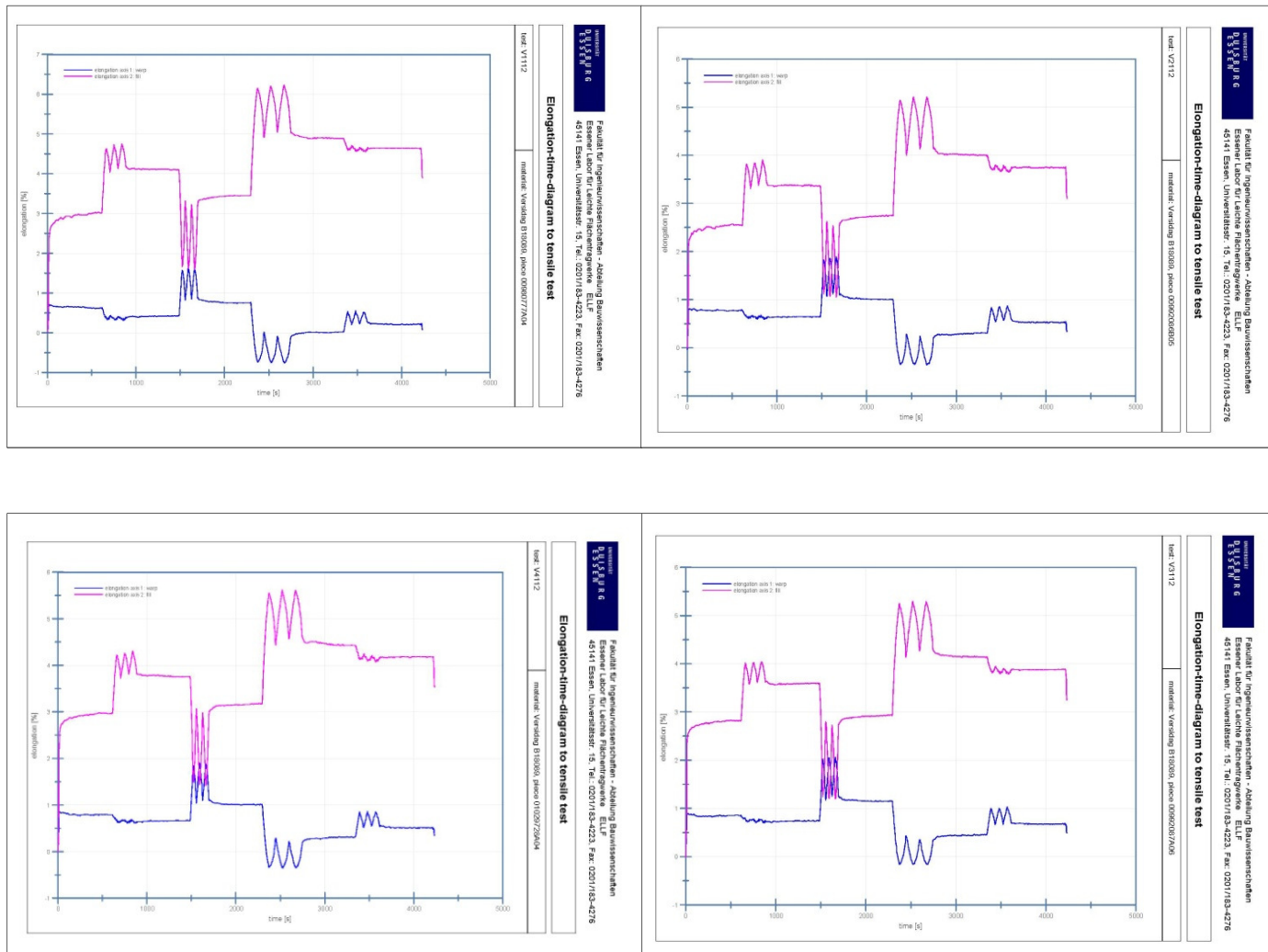
The following sketch is the force-time diagram proposed to University of Essen for the load ratio and sequences and the numbers of loads.



In this particular project, there are FOUR batch of material from Verseidag, so FOUR biaxial test is done. Extract here some pages from one of the test for information.



The elongation result of the 4 batch of material is summarized as follow;



As the result was based on higher wind speed as opposed to the design wind speed of 32m/s, when deciding a suitable value for compensation for cutting pattern, some reduction is considered from the tested result.

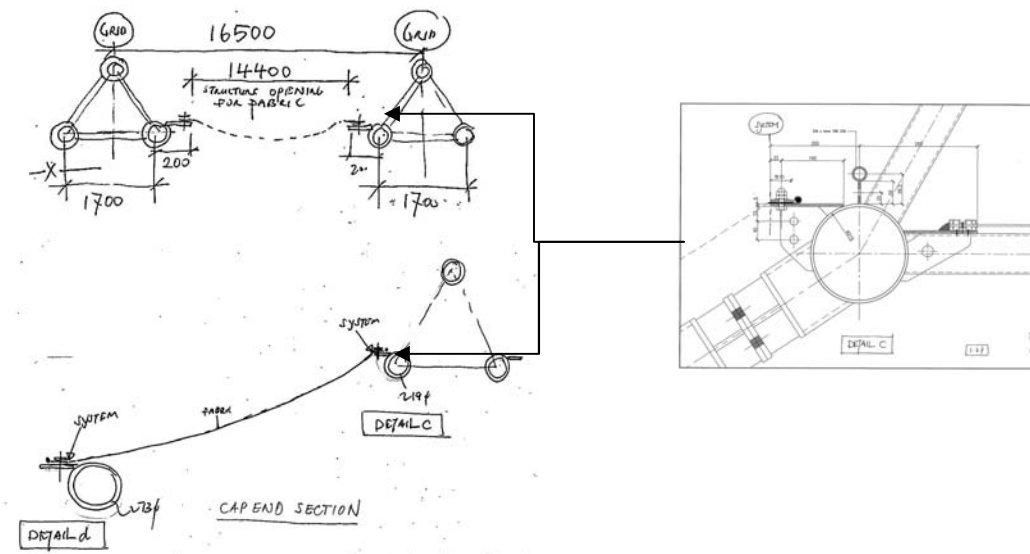
Based on past experience with Verseidag's PTFE material and the above result, we have used compensation value of 2.8% for the weft and 0.6% for the warp. Whereas the fixed side which is along the weft direction 1.2% is used instead of 2.8% as shrinkage is expected at welded seam for the keder pocket.

8.7 CUTTING PATTERN

8.7.1 FABRIC SYSTEM POINT

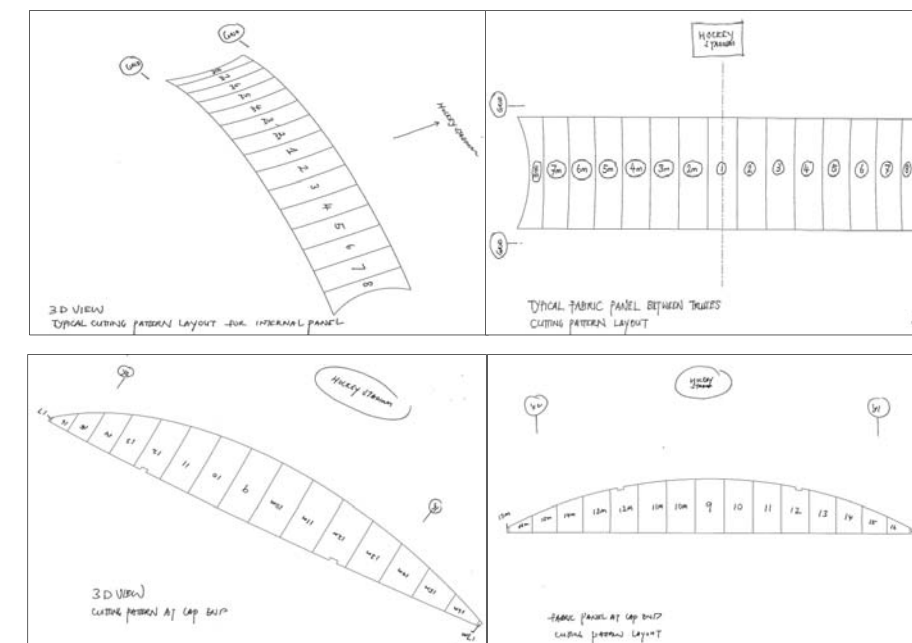
After the compensation value is established, some typical details ie. seam width, clamping detail, border cable pocket size are then finalized to prepared the cutting pattern. Also the roll width of the membrane is also known to decide how many strips of cutting pattern.

For fabric patterning, the system is different from the steel structure system, example the distance between 2 steel arch center is 16.5m, but fabric system is smaller than that and is 14.4m instead.



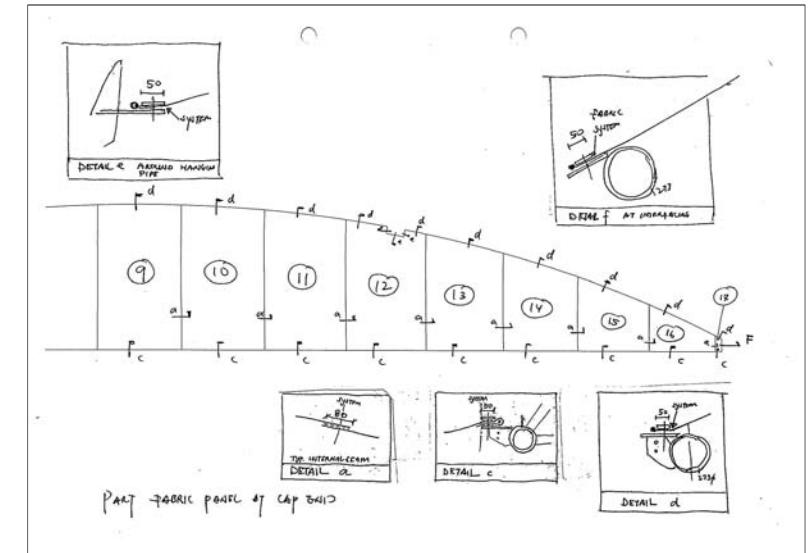
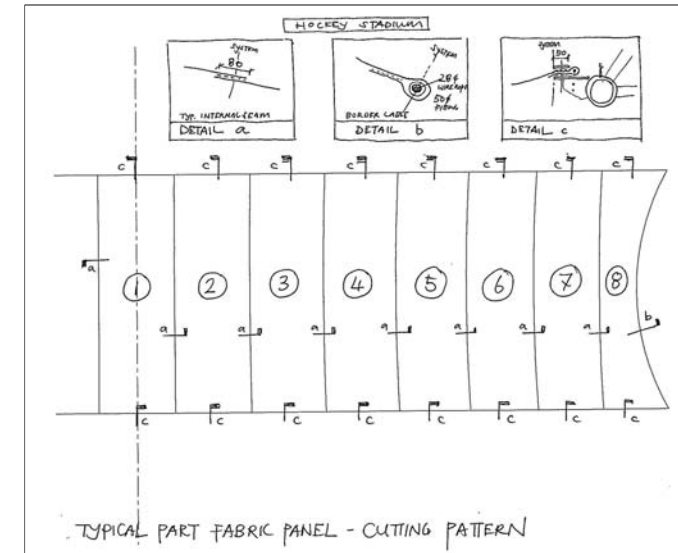
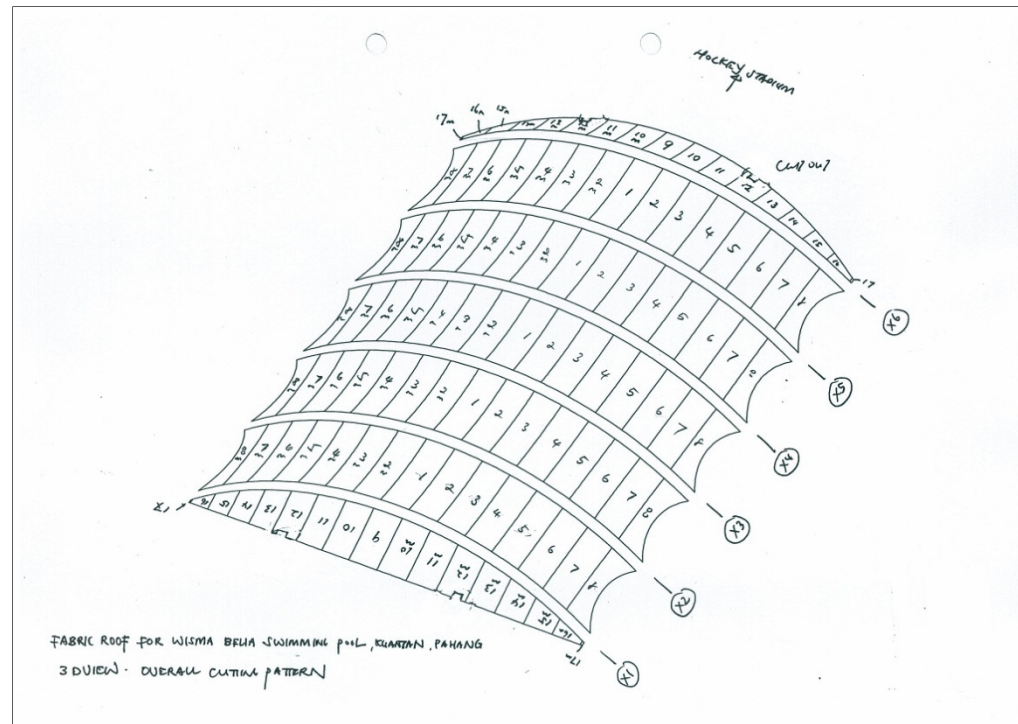
The width of B18089 is 4.7m, so maximum width of the patterning at system is 4.6m after deducting the overlapped seam of 80mm and trimming of 10mm on each side of the width of membrane.

So total nos of strip for internal panel is about $68m/4.6 = 15$ and end panel 17 strip, and they are symmetrical about the centerline, so only 17 cutting pattern need to be done.

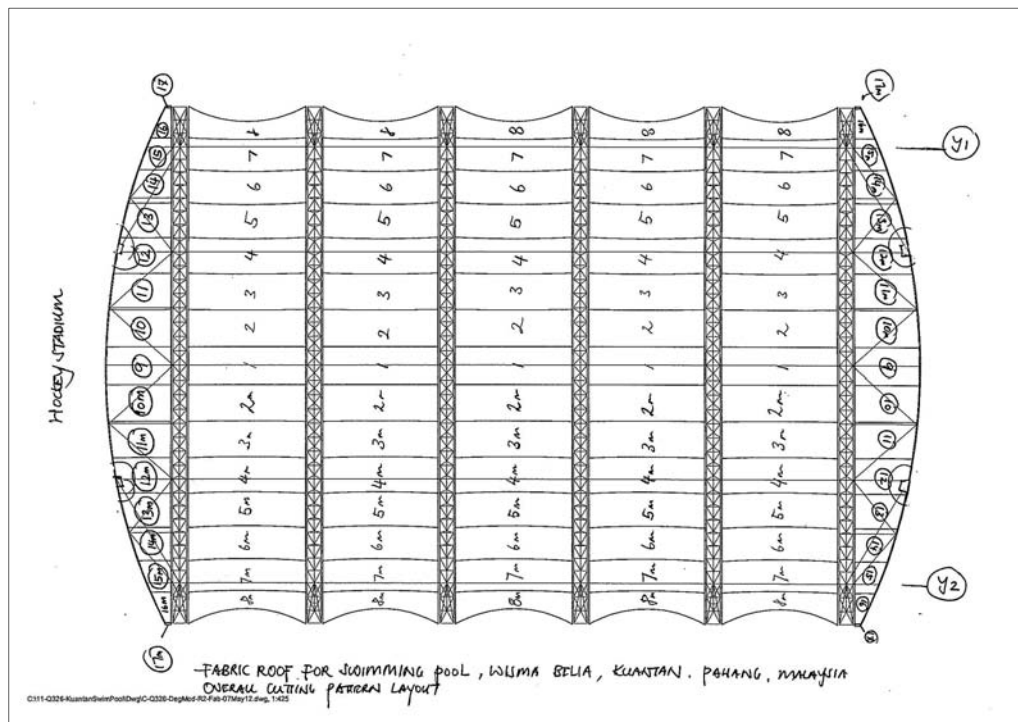


8.7.2 COMPENSATED CUTTING PATTERN

Therefore the overall cutting pattern for the swimming pool membrane roof are as follow;



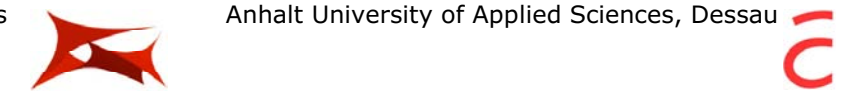
The compensated cutting pattern Strip 1 to 17 based on fabric system are attached for info.

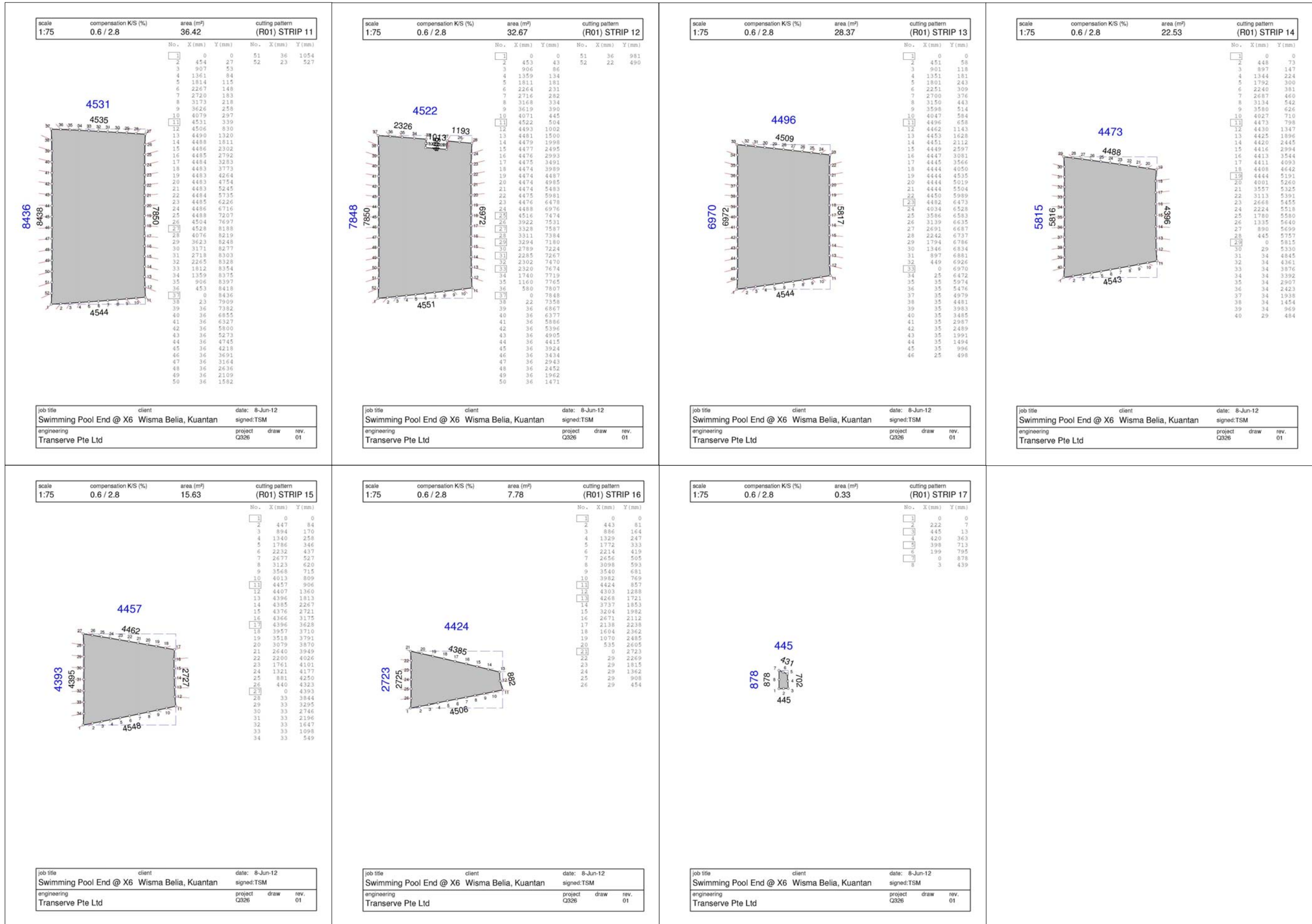


scale	compensation K/S (%)	area (m²)	cutting pattern		
1:90	0.6 / 2.8	64.04	STRIP 1		
			No.	X (mm)	Y (mm)
			1	0	5
			2	455	4
			3	909	2
			4	1364	0
			5	1819	0
			6	2273	0
			7	2728	0
			8	3183	0
			9	3637	2
			10	4092	4
			11	4546	6
			12	4502	519
			13	4513	1032
			14	4503	1545
			15	4502	2058
			16	4500	2571
			17	4498	3084
			18	4496	3597
			19	4495	4110
			20	4494	4623
			21	4493	5136
			22	4492	5650
			23	4492	6163
			24	4492	6676
			25	4491	7189
			26	4492	7702
			27	4492	8215
			28	4492	8728
			29	4493	9241
			30	4494	9754
			31	4495	10267
			32	4497	10780
			33	4498	11293
			34	4500	11806
			35	4502	12320
			36	4504	12833
			37	4513	13346
			38	4530	13859
			39	4546	14372
			40	4092	14374
			41	3637	14376
			42	3182	14377
			43	2728	14377
			44	2273	14377
			45	1819	14377
			46	1364	14377
			47	909	14375
			48	455	14373
			49	0	14372
			50	17	13859

scale	compensation K/S (%)	area (m²)	cutting pattern		
1:90	0.6 / 2.8	63.91	STRIP 2		
			No.	X (mm)	Y (mm)
			1	0	5
			2	455	3
			3	909	3
			4	1364	2
			5	1819	0
			6	2273	0
			7	2728	1
			8	3183	0
			9	3637	0
			10	4092	3
			11	4546	5
			12	4526	518
			13	4506	1031
			14	4493	1544
			15	4487	2057
			16	4482	2570
			17	4477	3083
			18	4472	3597
			19	4468	4110
			20	4464	4623
			21	4462	5136
			22	4459	5649
			23	4457	6162
			24	4456	6675
			25	4456	7188
			26	4456	7701
			27	4457	8215
			28	4459	8728
			29	4462	9241
			30	4465	9754
			31	4468	10267
			32	4473	10780
			33	4477	11293
			34	4482	11806
			35	4487	12319
			36	4493	12833
			37	4506	13346
			38	4526	13859
			39	4546	14372
			40	4092	14374
			41	3637	14376
			42	3182	14376
			43	2728	14376
			44	2273	14376
			45	1818	14376
			46	1364	14375
			47	909	14373
			48	455	14373
			49	0	14371
			50	14	13858

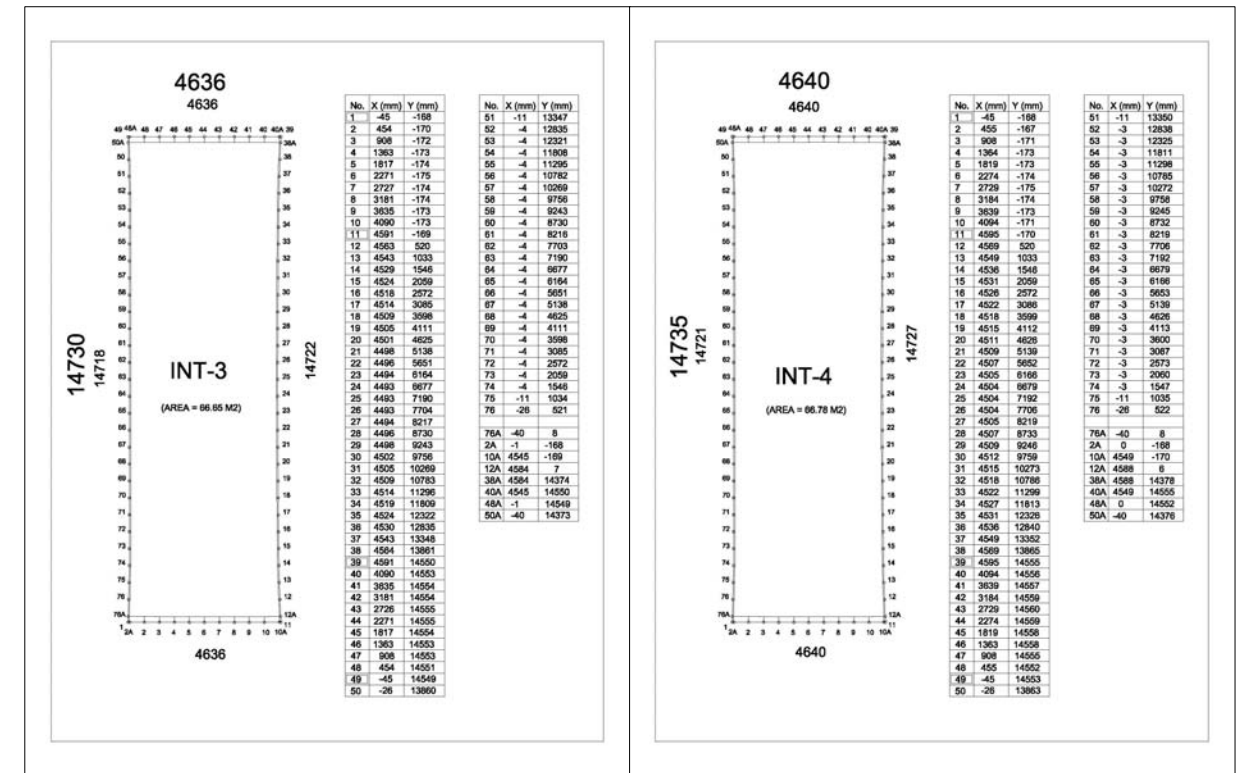
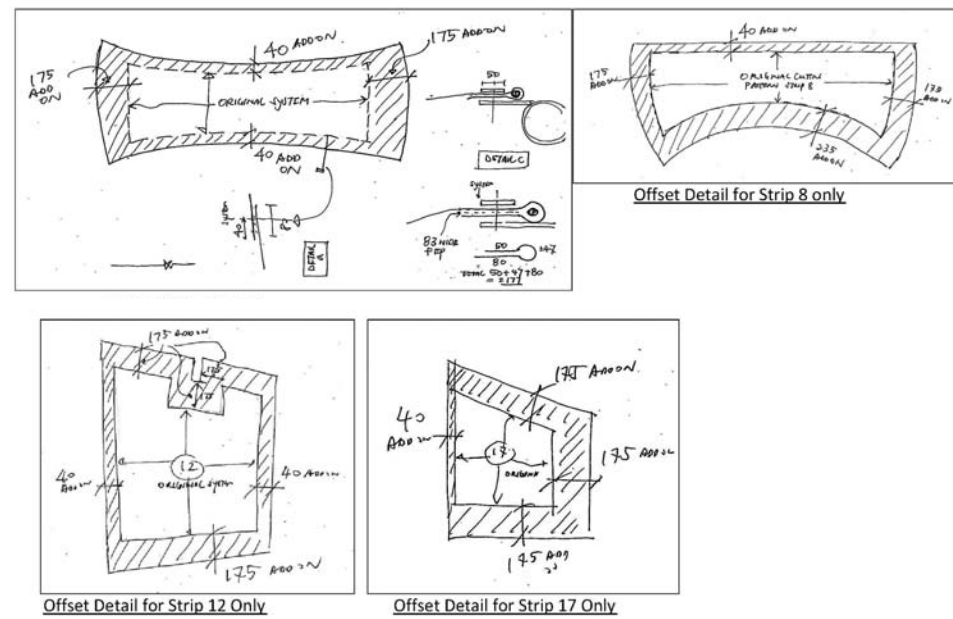
<p>scale 1:90 compensation K/S (%) 0.6 / 2.8 area (m²) 63.88 cutting pattern STRIP 3</p> <p>job title Swimming Pool (Internal) client Wisma Belia, Kuantan date: 5 Apr 12 engineering Transerve Pte Ltd project Q326 draw rev. 0</p>	<p>scale 1:90 compensation K/S (%) 0.6 / 2.8 area (m²) 64.01 cutting pattern STRIP 4</p> <p>job title Swimming Pool (Internal) client Wisma Belia, Kuantan date: 5 Apr 12 engineering Transerve Pte Ltd project Q326 draw rev. 0</p>	<p>scale 1:90 compensation K/S (%) 0.6 / 2.8 area (m²) 64.00 cutting pattern STRIP 5</p> <p>job title Swimming Pool (Internal) client Wisma Belia, Kuantan date: 5 Apr 12 engineering Transerve Pte Ltd project Q326 draw rev. 0</p>	<p>scale 1:90 compensation K/S (%) 0.6 / 2.8 area (m²) 63.89 cutting pattern STRIP 6</p> <p>job title Swimming Pool (Internal) client Wisma Belia, Kuantan date: 5 Apr 12 engineering Transerve Pte Ltd project Q326 draw rev. 0</p>
<p>scale 1:90 compensation K/S (%) 0.6 / 2.8 area (m²) 64.01 cutting pattern STRIP 7</p> <p>job title Swimming Pool (Internal) client Wisma Belia, Kuantan date: 5 Apr 12 engineering Transerve Pte Ltd project Q326 draw rev. 0</p>	<p>scale 1:90 compensation K/S (%) 0.6 / 2.8 area (m²) 46.91 cutting pattern STRIP 8</p> <p>job title Swimming Pool (Internal) client Wisma Belia, Kuantan date: 5 Apr 12 engineering Transerve Pte Ltd project Q326 draw rev. 0</p>	<p>scale 1:75 compensation K/S (%) 0.6 / 2.8 area (m²) 39.19 cutting pattern (R01) STRIP 9</p> <p>job title Swimming Pool End @ X6 Wisma Belia, Kuantan date: 7-Jun-12 engineering Transerve Pte Ltd project Q326 draw rev. 01</p>	<p>scale 1:75 compensation K/S (%) 0.6 / 2.8 area (m²) 38.49 cutting pattern (R01) STRIP 10</p> <p>job title Swimming Pool End @ X6 Wisma Belia, Kuantan date: 8-Jun-12 engineering Transerve Pte Ltd project Q326 draw rev. 01</p>



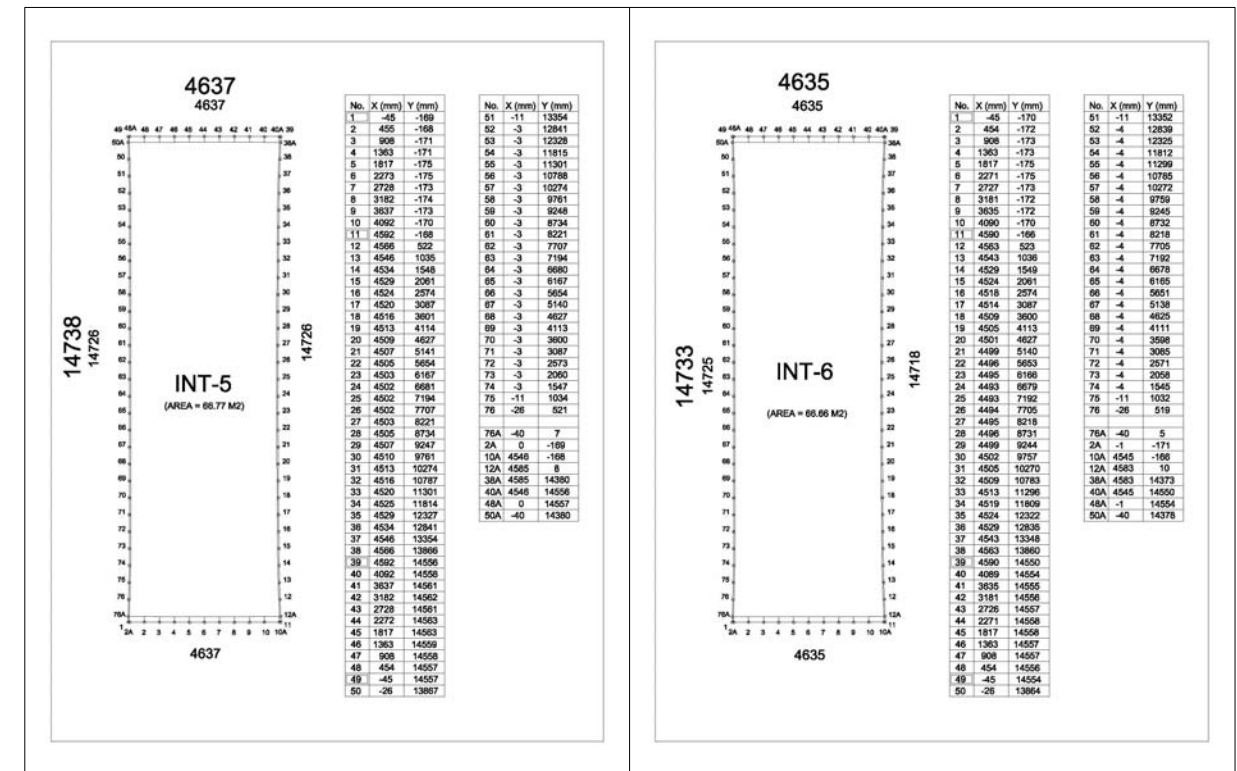
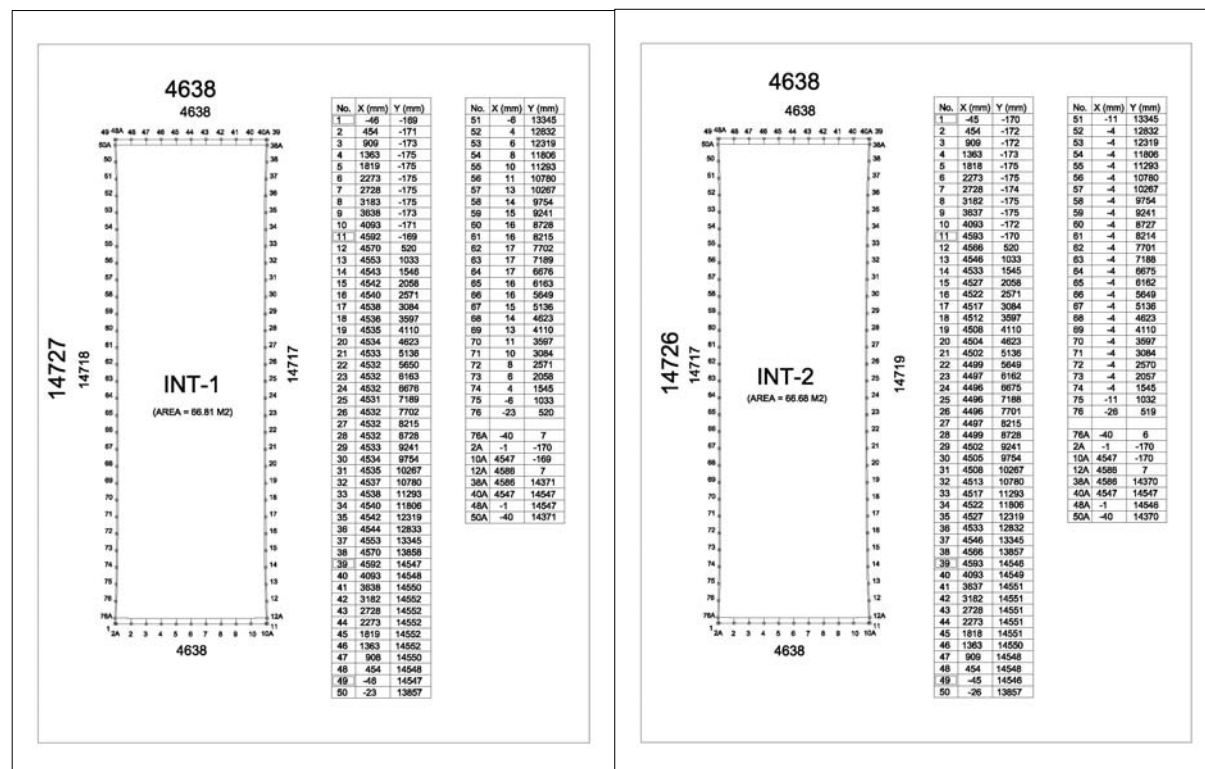


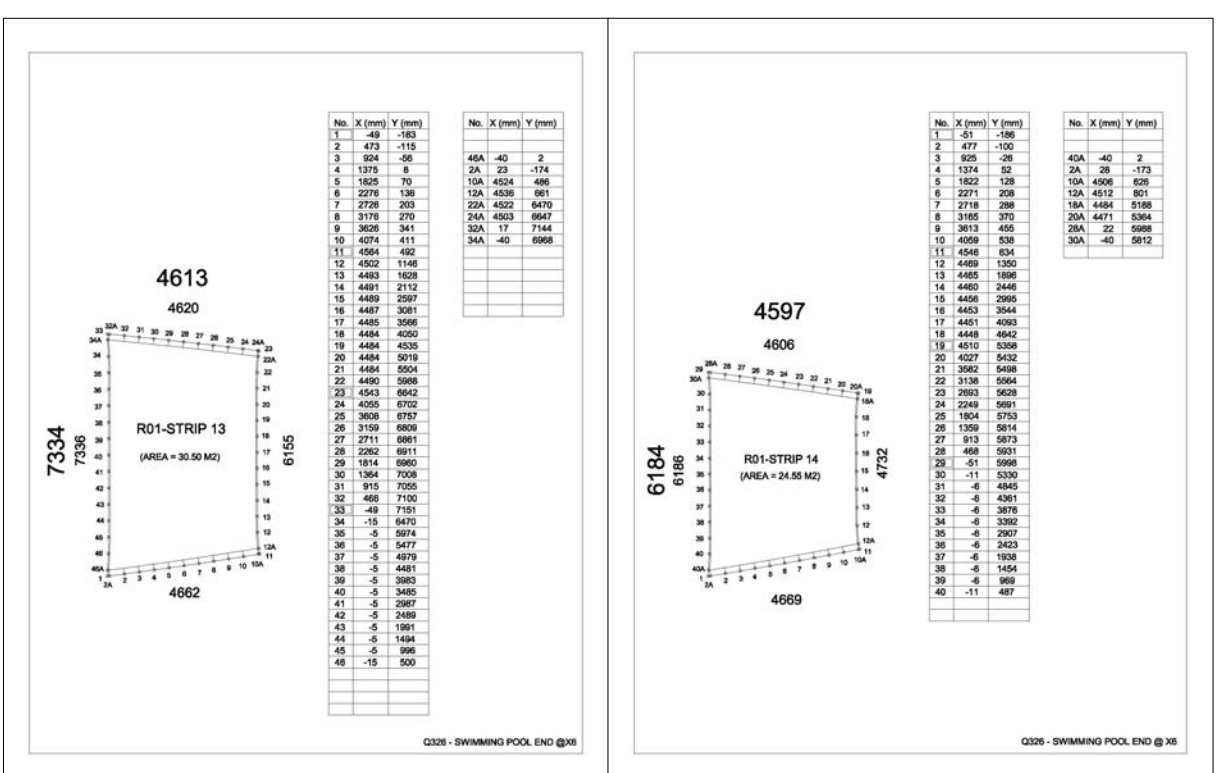
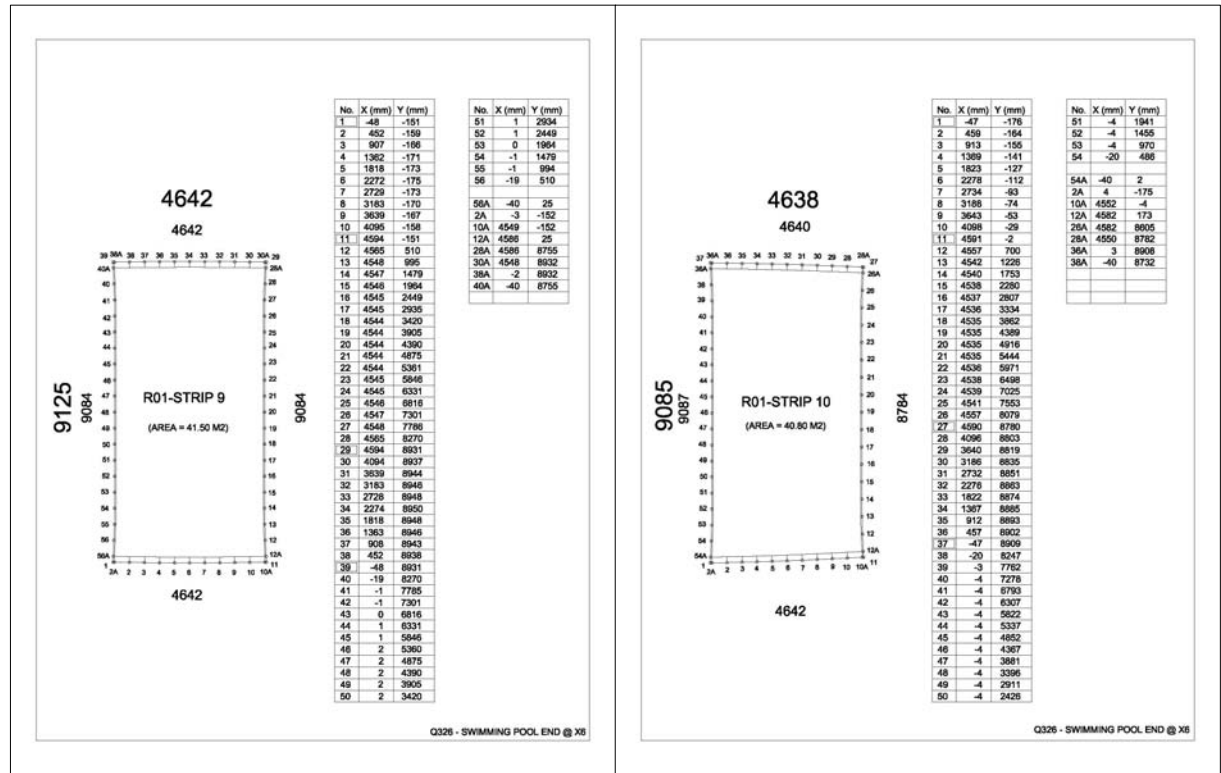
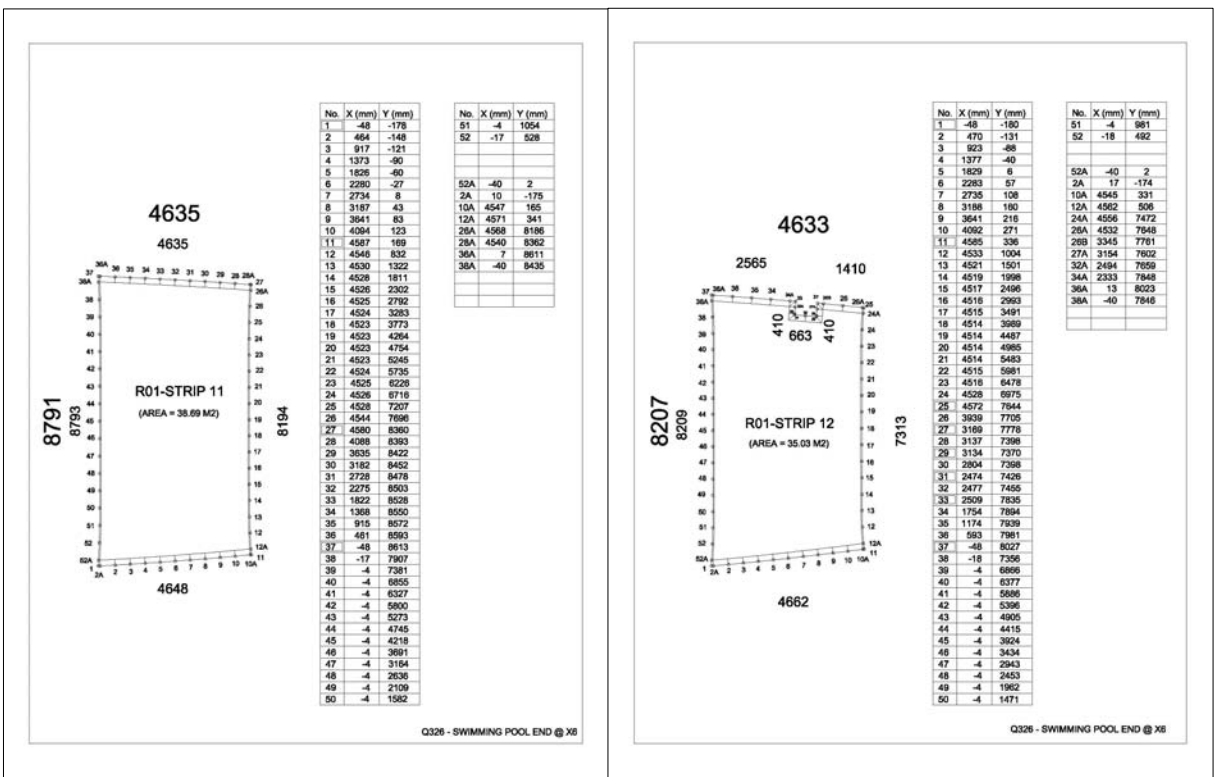
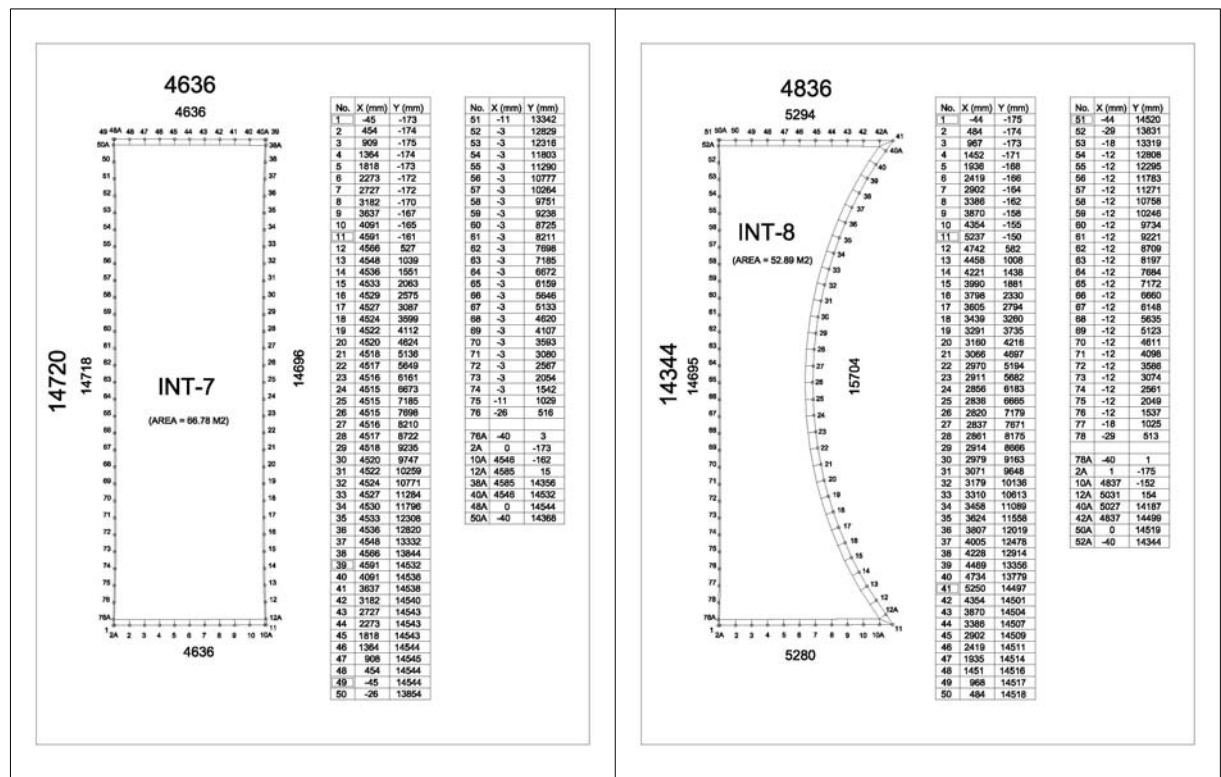
8.7.3 OFFSET CUTTING PATTERN

The cutting pattern based on fabric system are to be further process before actual cutting can be carried out. The tabulation of how much offset is shown in the sketch below. The offsetting process is then done in autocad.



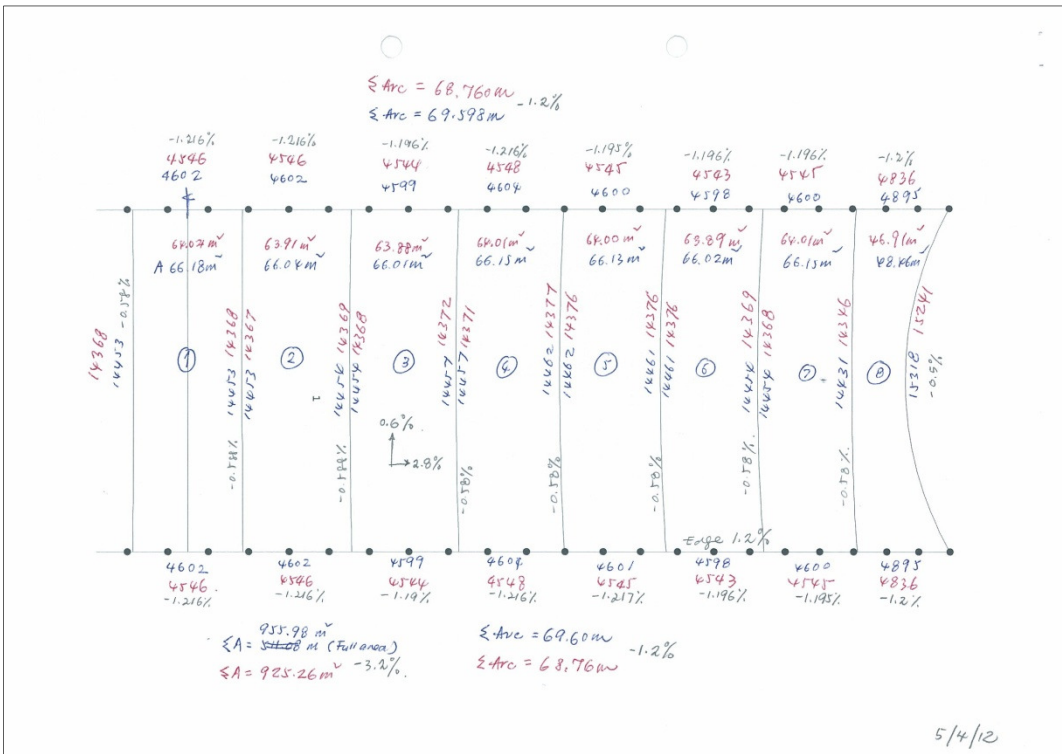
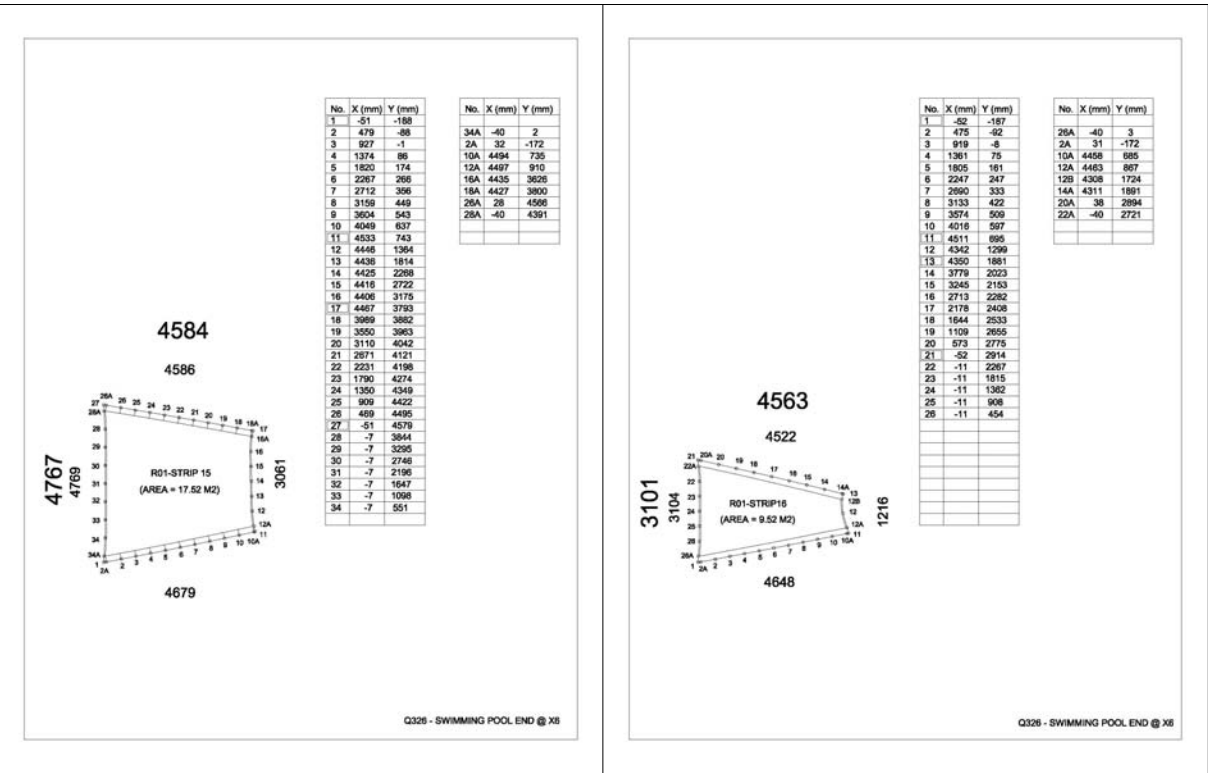
After that a different set of cutting pattern data is then passed to factory for actual fabrication.



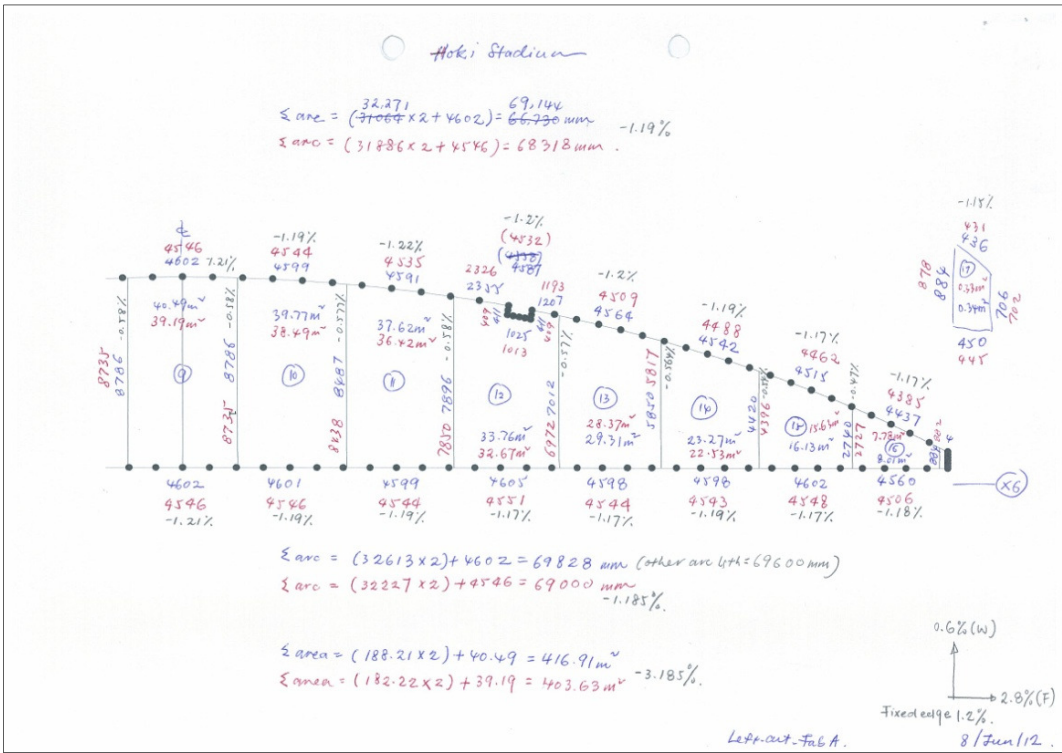
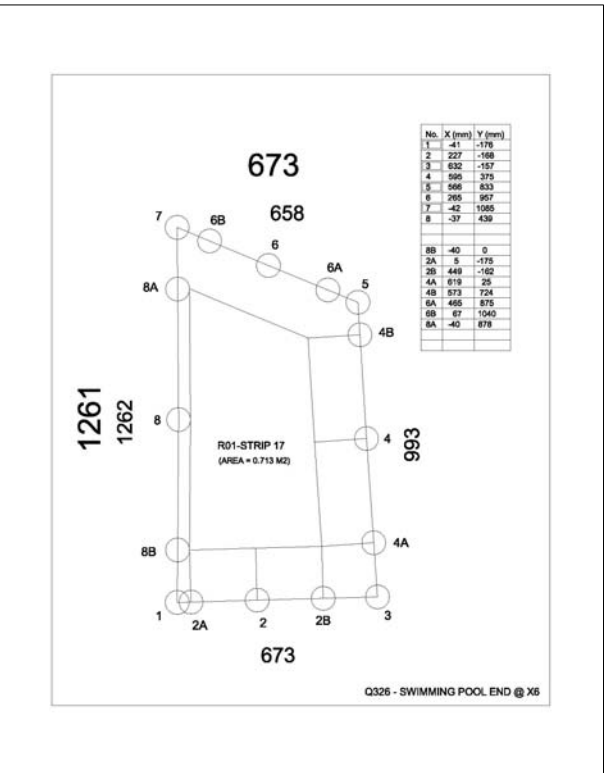


8.7.4 DIMENSION CHECK

As the cutting pattern is to be use 5 times for internal panel and 2 times for the end panel, extra measure is taken to make sure the compensated strips are done correctly, so dimension check of uncompensated length and area against the compensated length is done as shown.



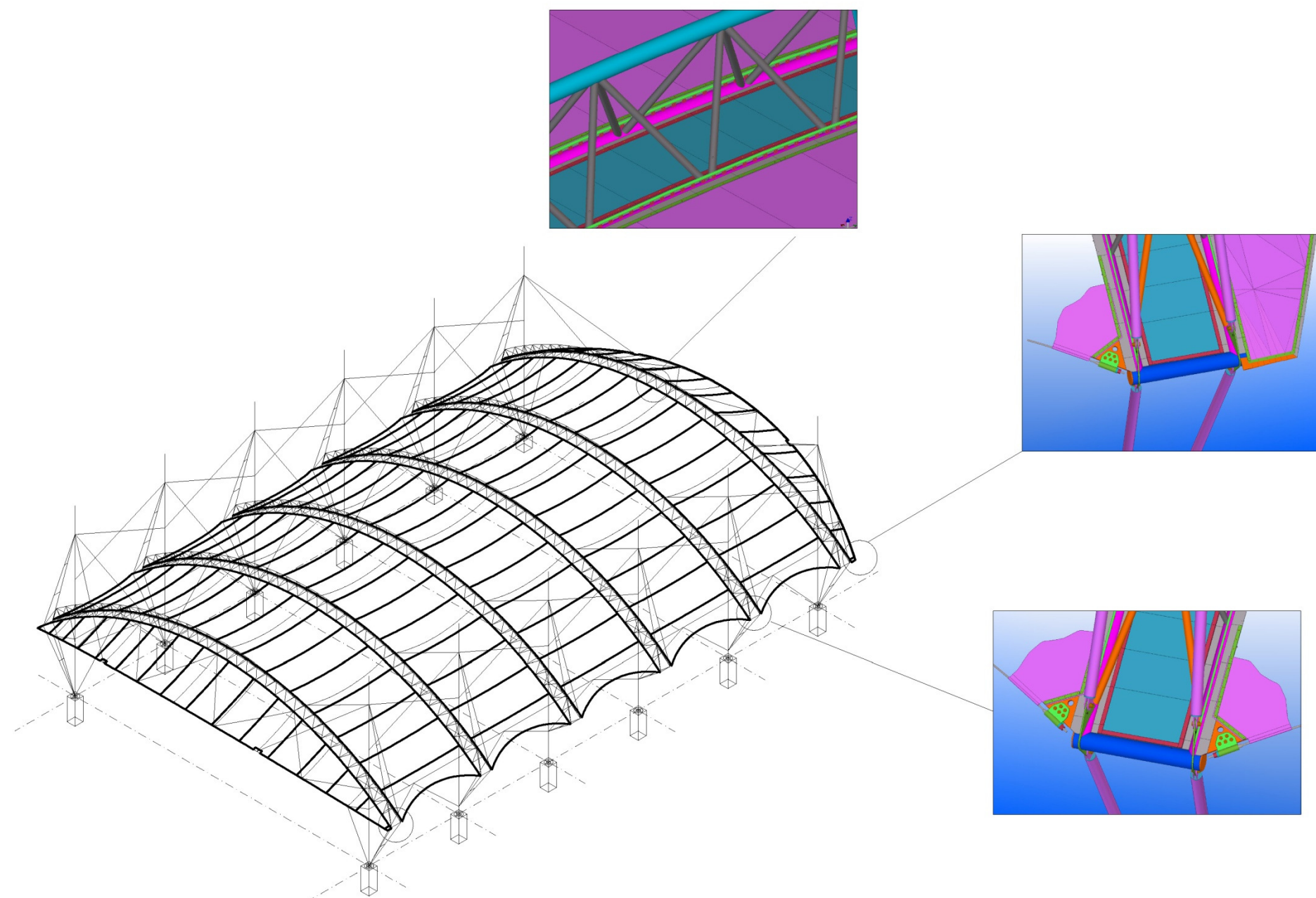
DIMENSION CHECK FOR INTERNAL STRIPS



DIMENSION CHECK FOR EDGE STRIPS



8.8 SUMMARY OF DETAILS



9. STEEL ERECTION

9.1 LIFTING CHECK

After site visit, noted that site access for crane only possible on the pavement beside the pool and also the access road leading to existing hostel beside the swimming pool. And the width of pool side pavement is 6.5m width of 250mm thick concrete slab, and so bigger tonnage crane are not possible to be used at site. And so not possible to erection the trusses in one single lift.



CRANE ACCESS BESIDE EXISTING HOSTEL BLOCK AT REAR OF SITE



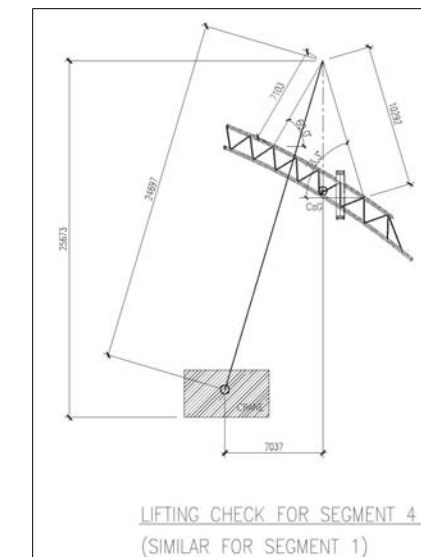
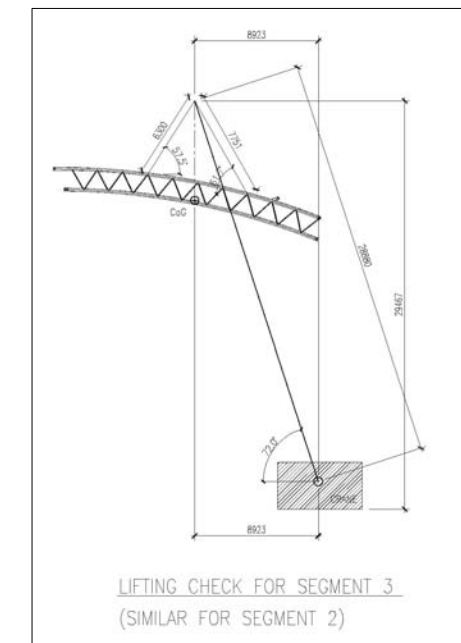
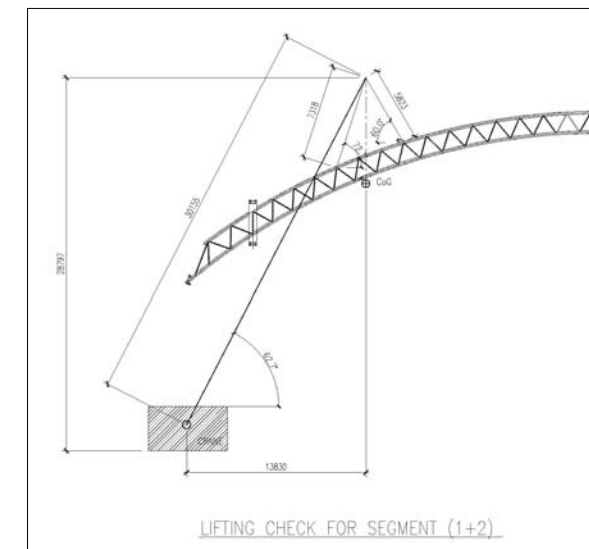
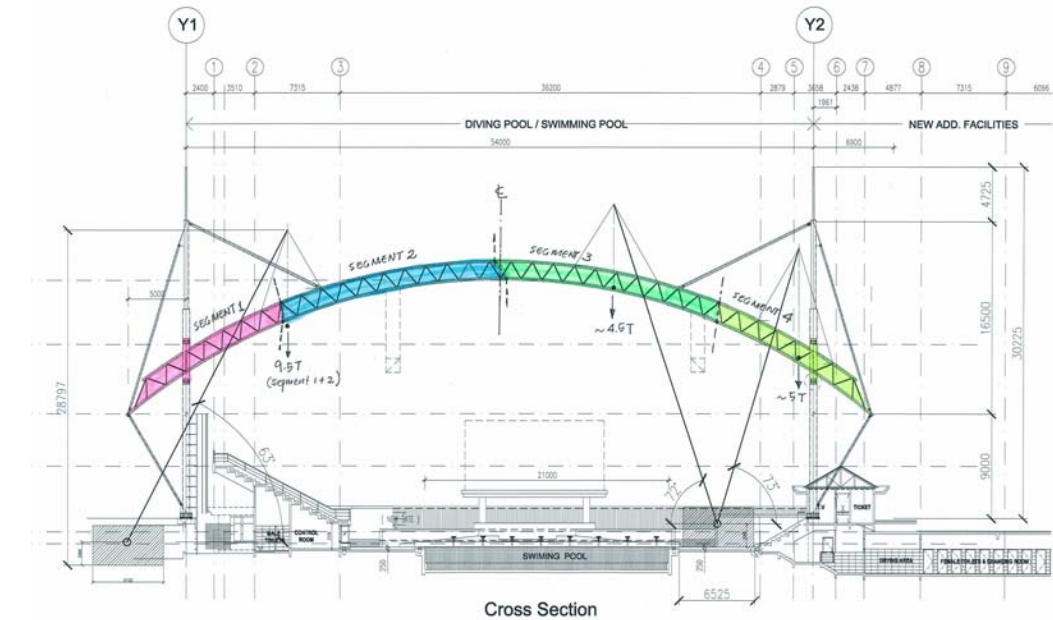
CRANE ACCESS BESIDE POOL

Due to these site access constrain, and preferably no welding work on site, proposed to use 35 ton hydraulic mobile crane. As such the 3D curved truss of approximately 68m span have to be fabricated in 4 segment to enable lifting by 35 tons crane and flange jointed to ensure the structural integrity and continuity of the trusses.

The truss is then subdivided further to 4t to 5t each so that they are possible to be lifted by the crane. And it is preferred that they are exactly oriented in final position when lifted and placed in position, so the center of gravity of these segment truss and correct length of lifting sling is important to the erector.

The Cog of these segmented truss is calculated with StaadPro software.

In the preliminary study of erection method, possibility of lifting truss segment 1 and segment 2 together from the rear access is also checked to minimize connection in the high air. But this option was not used at site later. It is attached for information.



9.2 ERECTION SEQUENCE

The steel frame erection sequence is briefly describe below, a detail illustration of the erection process is refers to attachment in the appendix.

The erection will starts from gridline X1 near to Score Board and progressively to gridline X6.

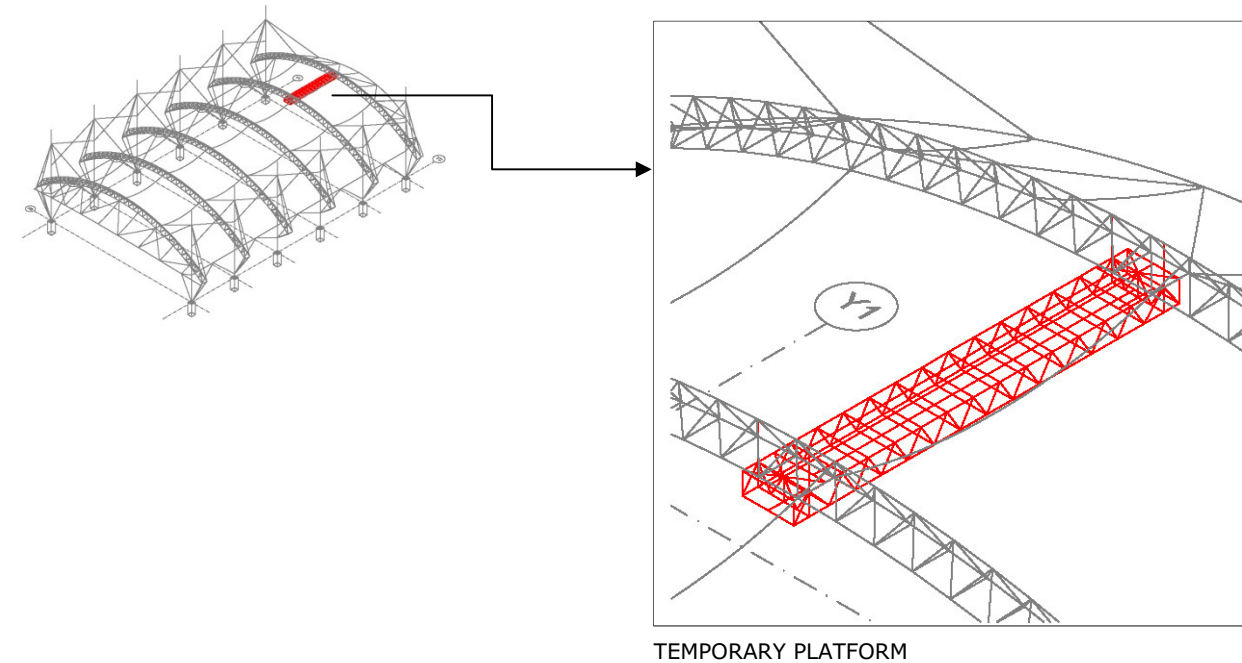
- 1) Firstly lift the lower column with base stump into correct position.
- 2) Then tie up at least 2 lower mast with the horizontal brace and cross bracing.
- 3) Then put in position Segment 1 truss on top and bolt up the flange joint.
- 4) With Segment 1 truss, the lower backstay can be fix up.
- 5) The step 1 to 4 can be repeated to the other side as well.
- 6) Then the upper mast with backstay and front hanger is connected placed on top
- 7) Then using 2 crane to lift the Segment 2 truss and also bolt the front hanger to stabilized the partly erected frame.
- 8) And a truss is completed when the opposite side Segment truss 3 is lifted and connected.
- 9) The same process will repeat for the second truss.
- 10) When the two truss are done, the 3 nos of curve tie beam can then be bolted on.
- 11) Same process repeat for the remaining truss until gridline X6.
- 12) Then the 2 end cap frame is erect with all its brace member until complete.
- 13) The 2 end front hanger is then bolted on.
- 14) Now the main structure is completed, the cross cable at the upper mast can then be install.
- 15) The catwalk hanging cage and walkway frame is then bolt on to the main roof structure.
- 16) So the roof is now ready to take on the fabric installation.

10. MEMBRANE INSTALLATION

10.1 MEMBRANE HANDLING

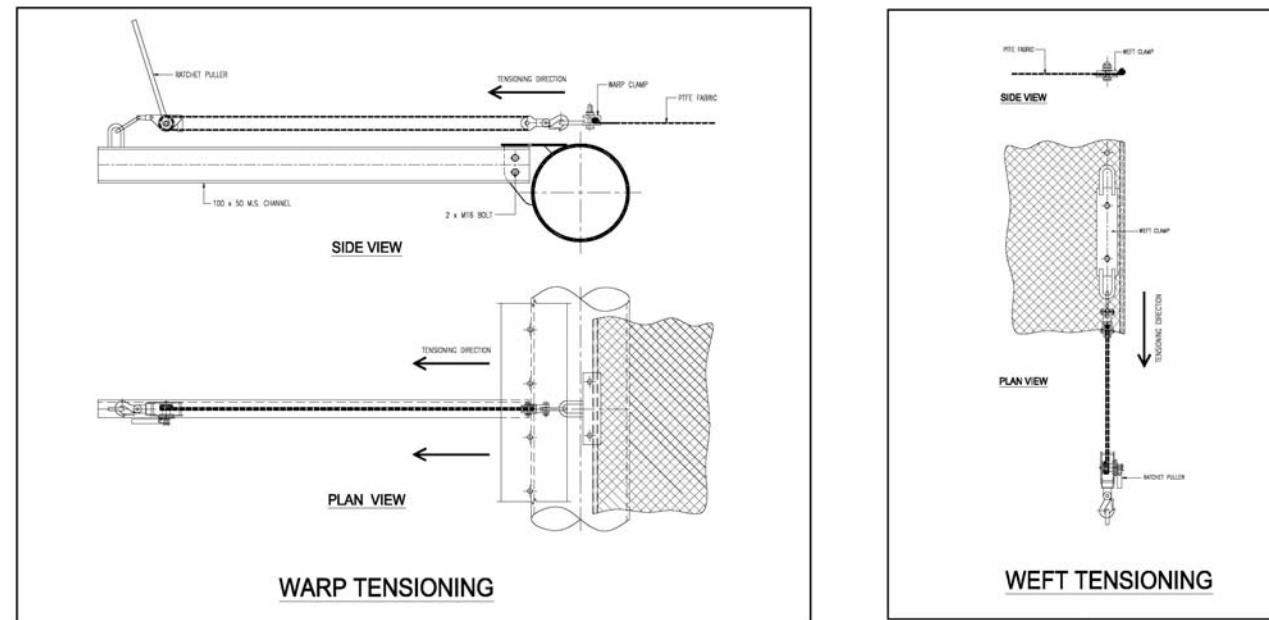
For lifting of fabric to the right level for installation, a temporary platform is proposed to be hung in-between 2 nos of 3D truss of 16.5m apart. This 3D platform is 18m in length, 2.4m width and 1.05m depth. It has to be lighted weight so not to impose too much load on to the steel structures. It is designed to be less than 2 tons and mainly welded from rectangular, square hollow section and angles.

4 nos of lifting padeye is provided at 4 corner, and 12mm thick plywood is fixed on top the platform. The platform will be placed slightly off center of the truss to avoid the center tie member , and it will be opened up at the center with the help of a crane with a spreader beam of as long as the width of the membrane 14m to one side and then to other side.



10.2 MEMBRANE TENSIONING

For installation of the membrane, some in-house tools are used. There are two type of tensioning tools used in this project; one for the warp and the other for the weft direction.

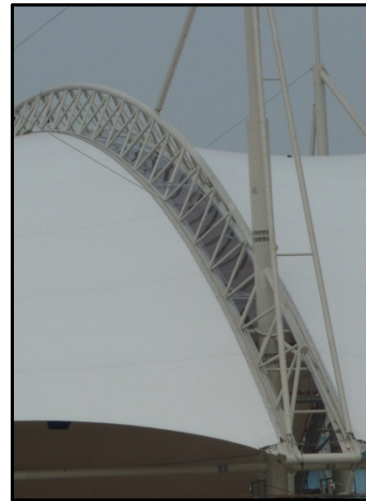


10.3 ERECTION SEQUENCE

The membrane installation is starting from grid X1 outward to grid X6. The sequence is briefly description as follow;

- 1) Firstly lift the temporary platform to just underneath the 3D truss and then secured at four corner to the bottom chord of truss.
- 2) Then lift the fabric with a spreader beam and place it on to top of the platform.
- 3) After that, fix the nylon ropes at a constant distance of about 1.5m across the truss. And do all necessary preparation for securing fabric.
- 4) Then secure 2 corners of the fabric to the spreader beam and lift up slowly by crane.
- 5) As the fabric is slowly lifted up and move outward, the edge of the fabric is temporary secure with the warp tensioning tools.
- 6) So this process will continue until the fabric reaches the end of truss.
- 7) After all necessary temporary securing is done, the crane can release the fabric.
- 8) The same process will repeat for the other side of the fabric.
- 9) The remaining work is then time consuming and it will progress slowly to tension the warp and weft of the fabric.
- 10) The same sequence is repeated for internal panel 2 and until panel 5.
- 11) After all internal fabric is installed, then proceed for preparation work for edge fabric.
- 12) The erection process of the edge panel is similar to the internal fabric.
- 13) After all the fabric are installed, the tensioning and fixing of clamping edge work is still in progress until they are all fully tension and clamped.
- 14) A fully illustration of the sequence can refer to photo images in the Appendix.





11. APPENDIX

11.1 WORK PROGRAMME

11.2 ENGINEERING DRAWINGS

11.3 ERECTION SEQUENCE

11.4 PHOTO IMAGES OF STEEL WORK

11.5 PHOTO IMAGES OF FABRIC WORK

11.6 PHOTO IMAGES OF COMPARISON BEFORE & AFTER ERECTION

11.7 AERIAL VIEW PHASE 1 COMPLETION

11.8 AERIAL VIEW PHASE 2 COMPLETION – IMPRESSION

11.9 NEWSPAPER ARTICLES BEFORE THE GAMES

11.10 PHOTO IMAGES DURING THE GAMES

11.11 BIAXIAL TEST REPORT

11.12 DESIGN CALCULATION

11.1 WORK PROGRAMME



11.2 ENGINEERING DRAWINGS



PROPOSED TENSILE FABRIC ROOF SYSTEM AT KOMPLEKS KOLAM RENANG, WISMA BELIA INDERA MAHKOTA, KUANTAN, PAHANG DARUL MAKMUR. MALAYSIA.

Kompleks Kolam Renang

NOTE : 55

03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

REF	DATE	DESCRIPTION
-----	------	-------------

OWNER :



MAJLIS PERBANDARAN KUANTAN

Jalan Tanah Putih, 25100 Kuantan,
Pahang Darul Makmur, Malaysia.
TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.

117-A, 1st. FLOOR, MUIP BUILDING,
JALAN MAHKOTA, 25000 KUANTAN ,
PAHANG DARUL MAKMUR
TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :



**dzj & ASSOCIATES ARCHITECTS
SENDIRIAN BERHAD (70890-P)**

B-26, Tingkat Satu, Jalan IM3/10
Bandar Indera Mahkota
25200 Kuantan, Pahang Darul Makmur.
Tel :09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:



TRI-ARCH sdn. bhd.

7-JALAN 2/115A, TAMAN PAGAR RUYONG
OFF. JALAN KUCHAI LAMA,
59200 KUALA LUMPUR.
TEL : 7961 2870 FAX : 7961 8210
E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
No. 11, Jalan USR, Segar 10 Bukit Mering, 61500 Seri Kembangan, Selangor,
14100 Kajang, Selangor.
Tel : 03-89257021 Fax: 03-89257022
E-mail : info@sedibena.com website : www.sedibena.com



TRANSERVE PTE LTD
(In Reg. No. 19772436)

39 PANDAN ROAD, JURONG, SINGAPORE 609281
Tel: (65) 6268 3069 Fax: (65) 6266 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:

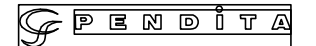


JURUNDING HYH SDN. BHD.

A-7732, Tingkat Satu, Kedai LKNP,
Jalan Dato' Bahaman, 25200 Kuantan,
Pahang Darul Makmur.

Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



NO.C-9-9, Level 11, Menara Ujang Emas,
85 Jalan Loke Yew, 55200 Kuala Lumpur.
Tel : 03-92008268 Fax : 03-92008276 (391855-V)
email: info@pendita.com.my website: pendita.com.my

PROJECT :

**CADANGAN MENAIK TARAF
KOLAM RENANG SERTA KERJA-KERJA
BERKAITAN DI WISMA BELIA,
INDERA MAHKOTA, KUANTAN. MALAYSIA.**

TITLE :

3D - VIEW

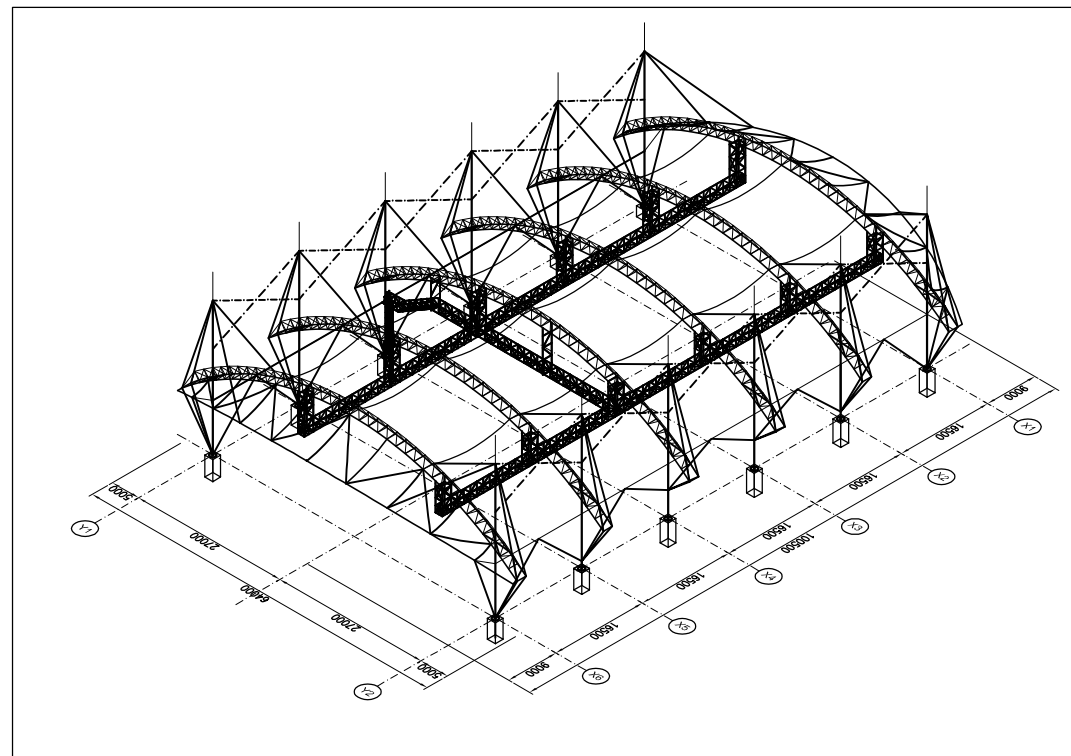
DATE : 29.12.2011 DRAWN :

SCALE : NTS CHECKED :

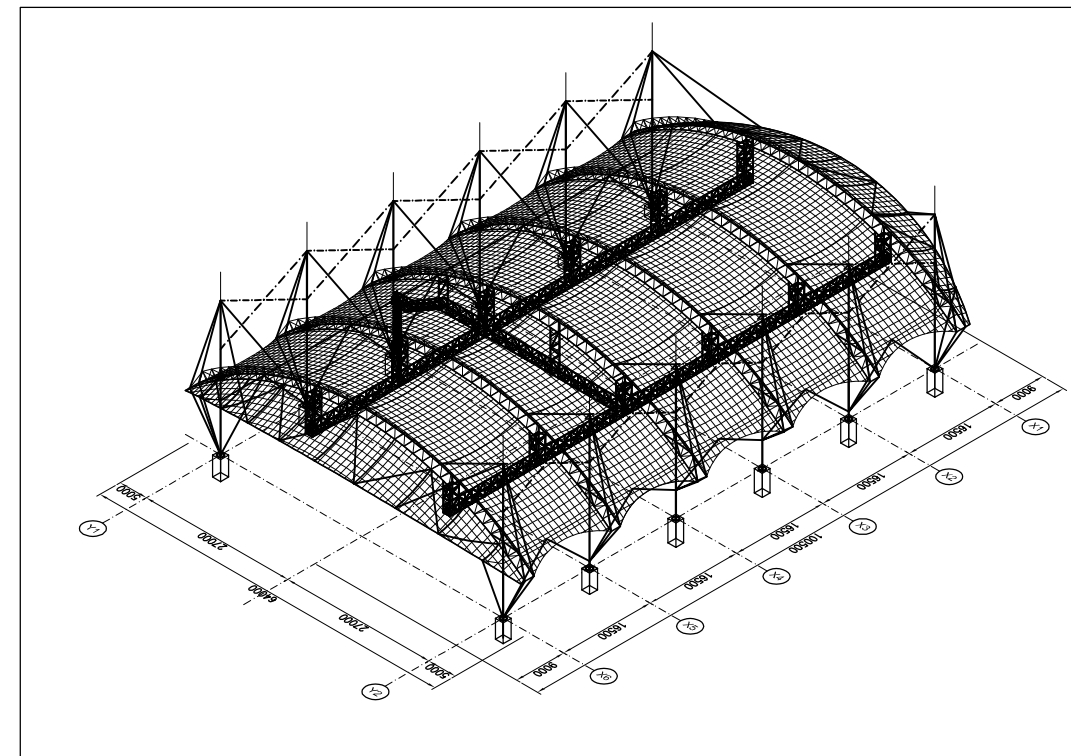
DRAWING NO. : REVISION

TA-Q326-01

03

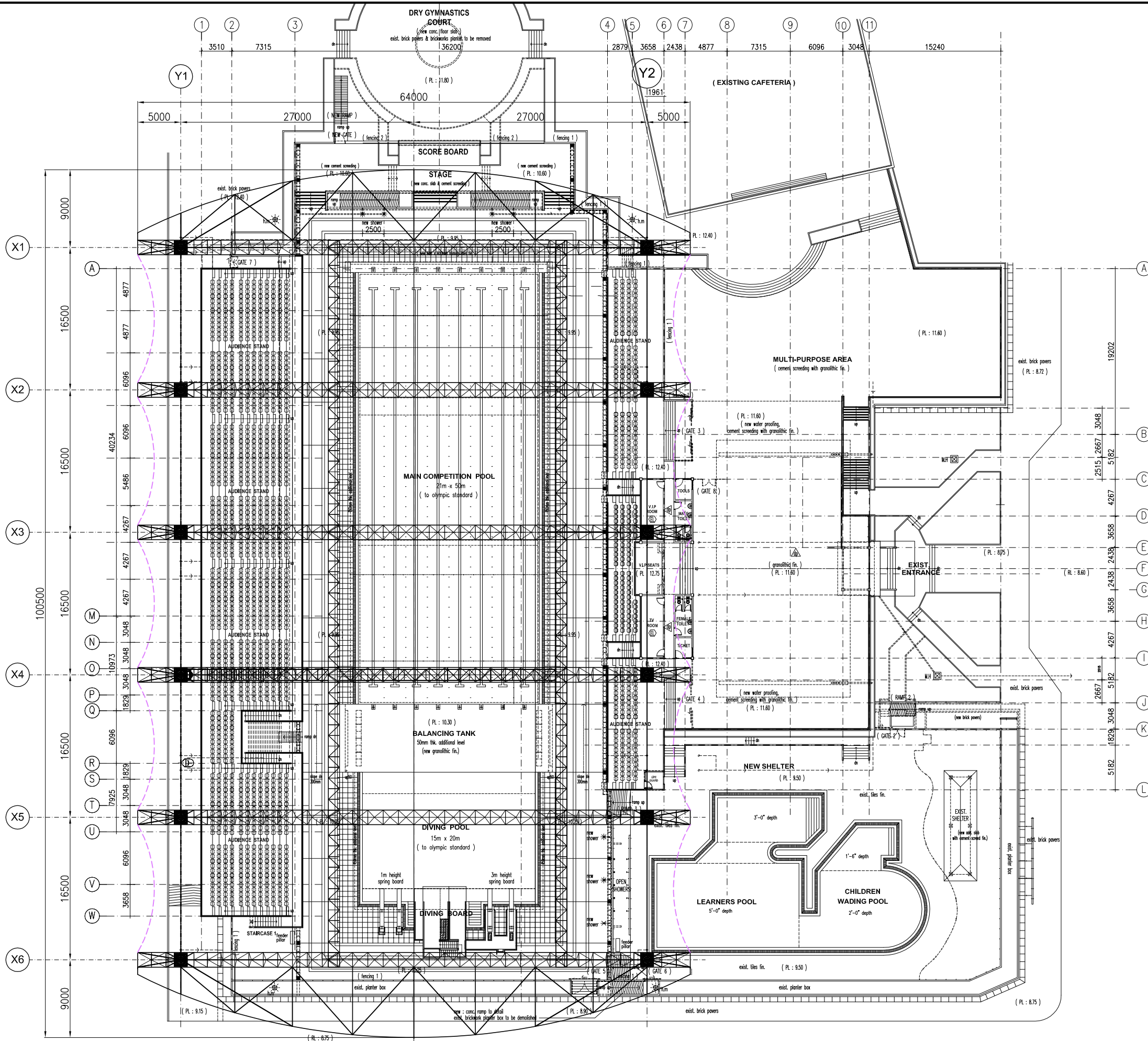


3D-VIEW OF STRUCTURE FRAMING










3D-VIEW OF STRUCTURE FRAMING + FABRIC





SUPPORT COLUMN LAYOUT PLAN

Kompleks Kolam Renang		NOTE :	56
03	31.07.2012	AS-BUILT	
02	20.04.2012	GENERAL	
01	12.01.2012	GENERAL	
REF	DATE	DESCRIPTION	
OWNER :			
 MAJLIS PERBANDARAN KUANTAN Jalan Tanah Putih, 25100 Kuantan, Pahang Darul Makmur, Malaysia. TEL : 09-5121555/666 FAXS : 5130644			
MAIN CONTRACTOR :			
SUARA HATI SDN. BHD. 117-A, 1st. FLOOR, MUIP BUILDING, JALAN MAHKOTA, 25000 KUANTAN, PAHANG DARUL MAKMUR TEL : 609-515 2473, FAX : 603-516 2619			
ARCHITECTS :			
 dzj & ASSOCIATES ARCHITECTS SENDIRIAN BERHAD (708280-P) 8-26, Tingkat Satu, Jalan IM3/10 Bandar Indera Mahkota 25200 Kuantan, Pahang Darul Makmur. Tel: 09-5736430 / 5736372 Fax: 09-5736443			
SPECIALIST ROOF & CLADDING CONTRACTOR:			
 TRI-ARCH sdn. bhd. 7-1, JALAN 2/115A, TAMAN PAGAR RUYONG OFF JALAN KUCHAI LAMA, 58200 KUALA LUMPUR. TEL : 7981 2870 FAX : 7981 8210 Email: triarch9@yahoo.com.my			
IN CONJUNCTION WITH:			
 SEDIABENA sdn. bhd. No. 11, Jalan Kencana, Dewan, K. B. B. Jalan, 47500 Seremban, Selangor Darul Ehsan, Malaysia. Tel: 06-89561233 Fax: 06-89561222 Email: sdn@sedibena.com Website: www.sedibena.com			
 TRANSERVE PTE LTD 39 PANDAN ROAD, JURONG, SINGAPORE 609281 Tel: (65) 6268 3099 Fax: (65) 6266 2324 Email: sales@transerve.com.sg			
ENGINEER'S CAS and M&E:			
 JURUNING HYH SDN. BHD. A-7732, Tingkat Satu, Kedai LKNP, Jalan Dato' Bahaman, 25200 Kuantan, Pahang Darul Makmur. Tel : 09-566 3031 Faks : 09-560 1182			
QUANTITY SURVEYOR :			
 PENDITA NO.9-9-9, Level 11, Menara Ujang Emas, 85, Jalan Loke Yew, 55200 Kuala Lumpur Tel : 03-92008268 Fax : 03-92008276 (391855-V) email: info@pendita.com.my website: pendita.com.my			
PROJECT :			
CADANGAN MENAIK TARAF KOLAM RENANG SERTA KERJA-KERJA BERKAITAN DI WISMA BELIA, INDERA MAHKOTA, KUANTAN, MALAYSIA.			
TITLE :			
SUPPORT COLUMN LAYOUT PLAN			
DATE : 29.12.2011	DRAWN :		
SCALE : 1 : 500	CHECKED :		
DRAWING NO. :			REVISION
TA-Q326-02			03



REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :



MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN,
 PAHANG DARUL MAKMUR
 TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :




dzj & ASSOCIATES ARCHITECTS
BENDIRIAN BERHAD (708290-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:




TRI-ARCH sdn. bhd.
 7-1, JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 55200 KUALA LUMPUR.
 TEL : 7961 2870 FAX : 7961 8210
 E-mail: triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
 11, Jalan Awan 1/18, Sungai Udang, 41500 Seremban, Negeri Sembilan, Malaysia.
 Tel: 06-7651221 Fax: 06-7651222
 (Company No: 987574) web: www.sediabena.com

&



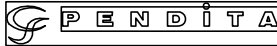
TRANSERVE PTE LTD
 (In Reg. No: 197721430)
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3069 Fax: (65) 6268 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:



JURUNING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



PENDITA
 NO.C-9-9, Level 11, Menara Ungang Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

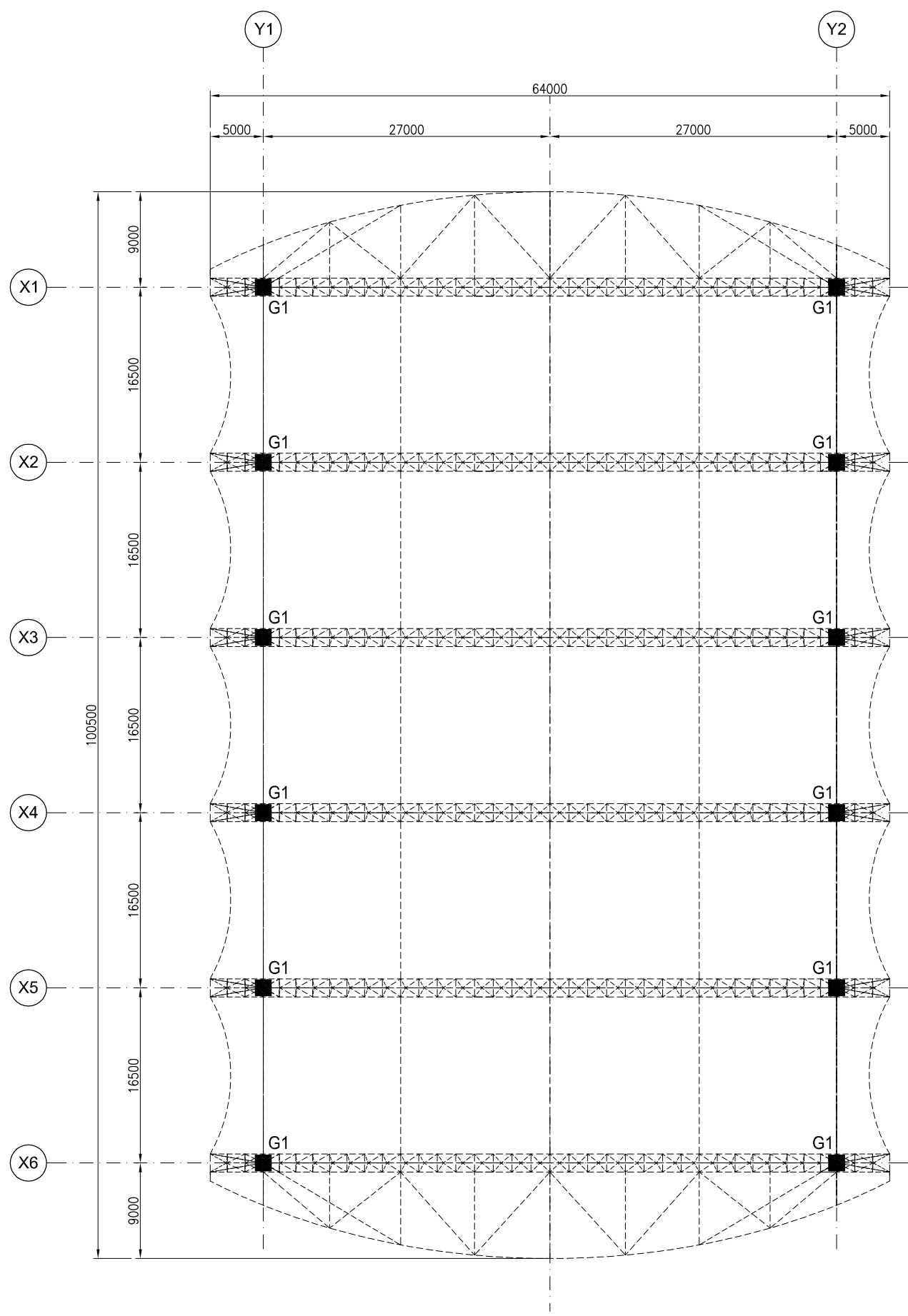
PROJECT :

**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN. MALAYSIA.**

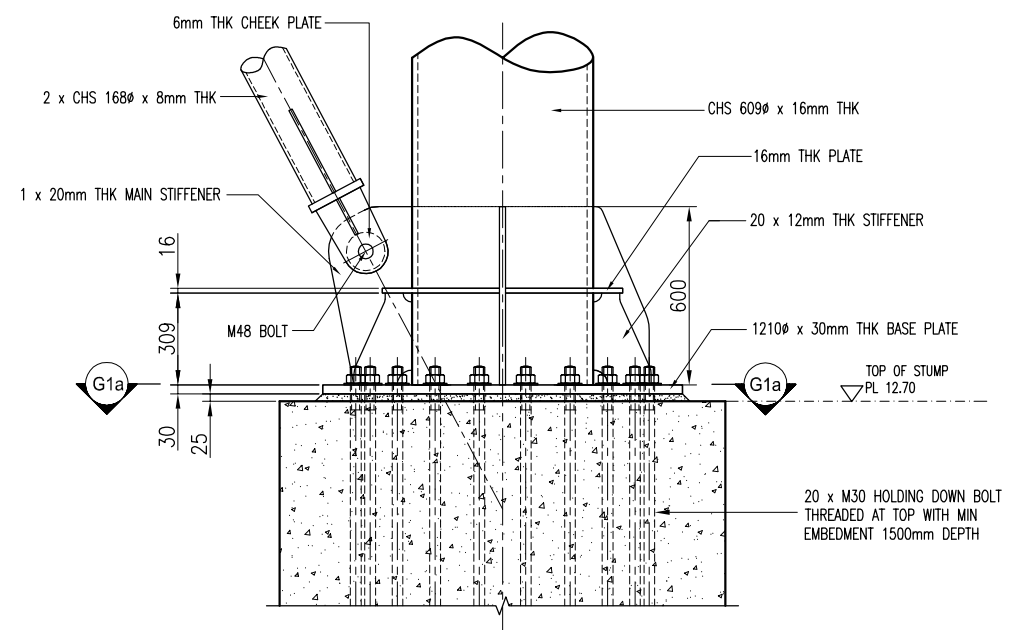
TITLE :

**HOLDING DOWN BOLT LAYOUT PLAN
 & DETAILS**

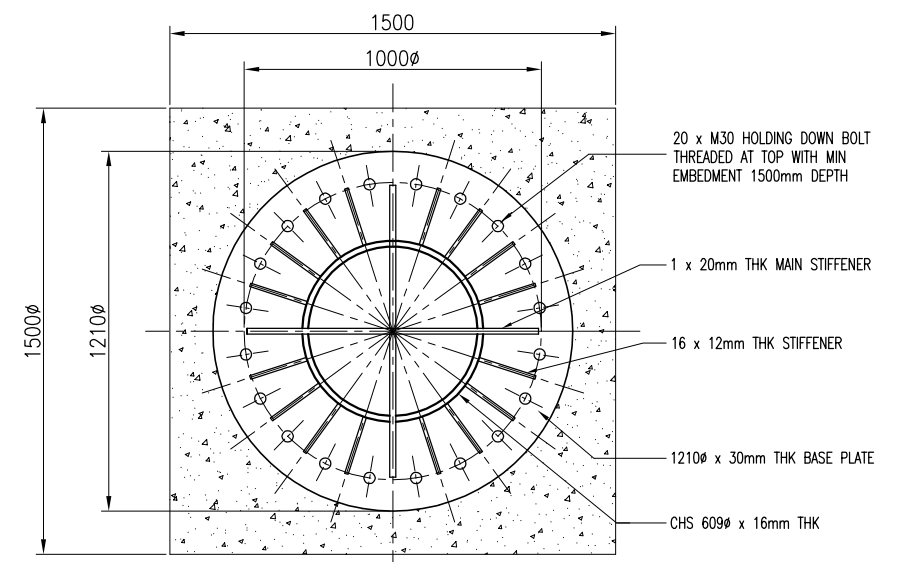
DATE : 29.12.2011	DRAWN :
SCALE : 1 : 500 / 1 : 20	CHECKED :
DRAWING NO. : TA-Q326-03	REVISION : 03



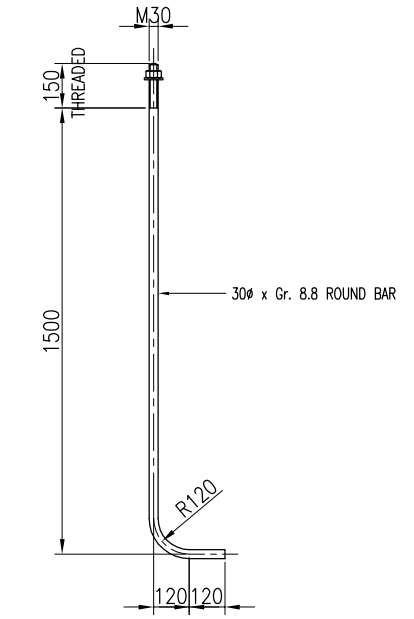
HOLDING DOWN BOLT LAYOUT PLAN
 (NOTE: TOP OF STUMP LEVEL SUBJECT TO SITE ADJUSTMENT)



TYPICAL BASE PLATE DETAIL - TYPE G1

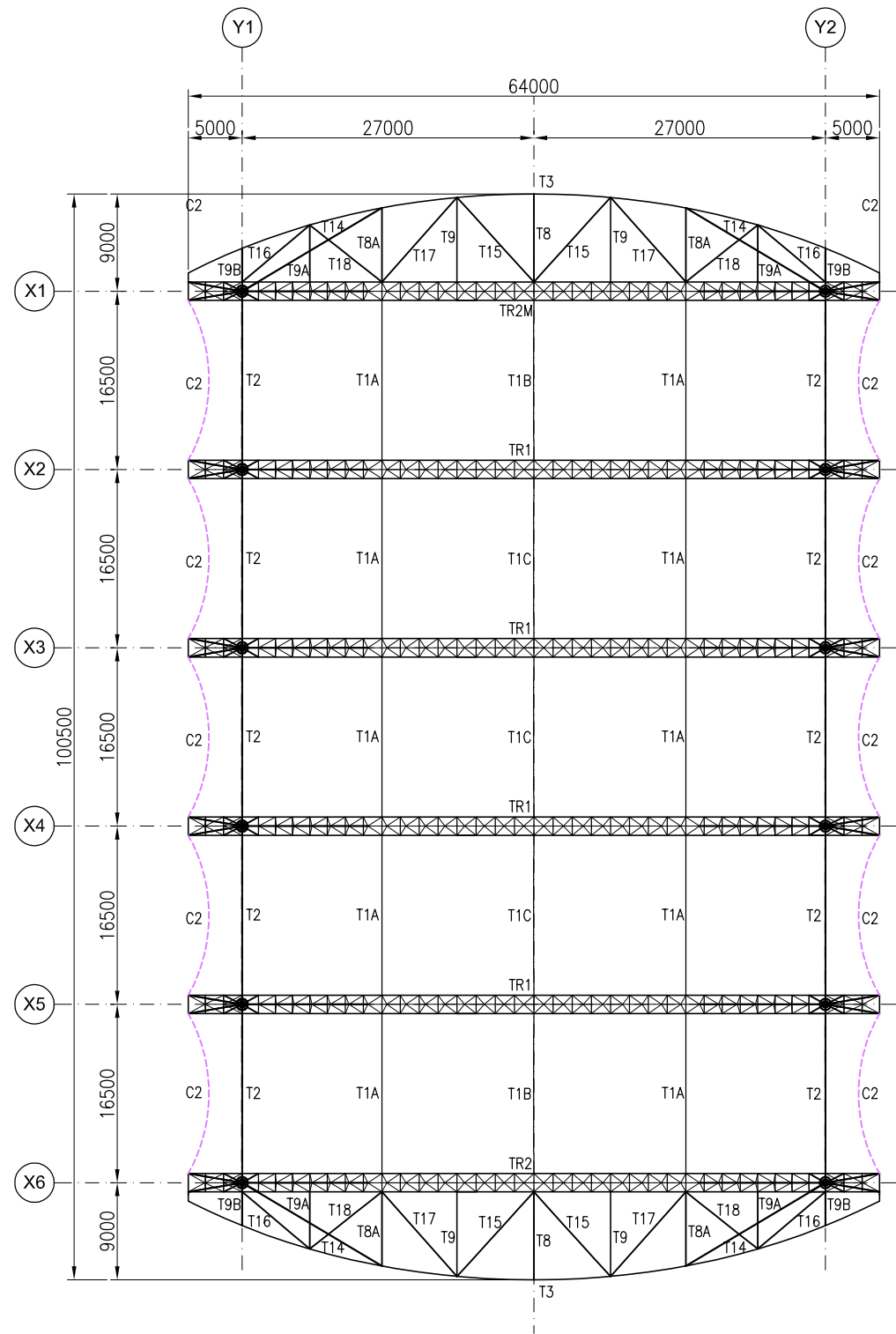


SECTION G1a - G1a

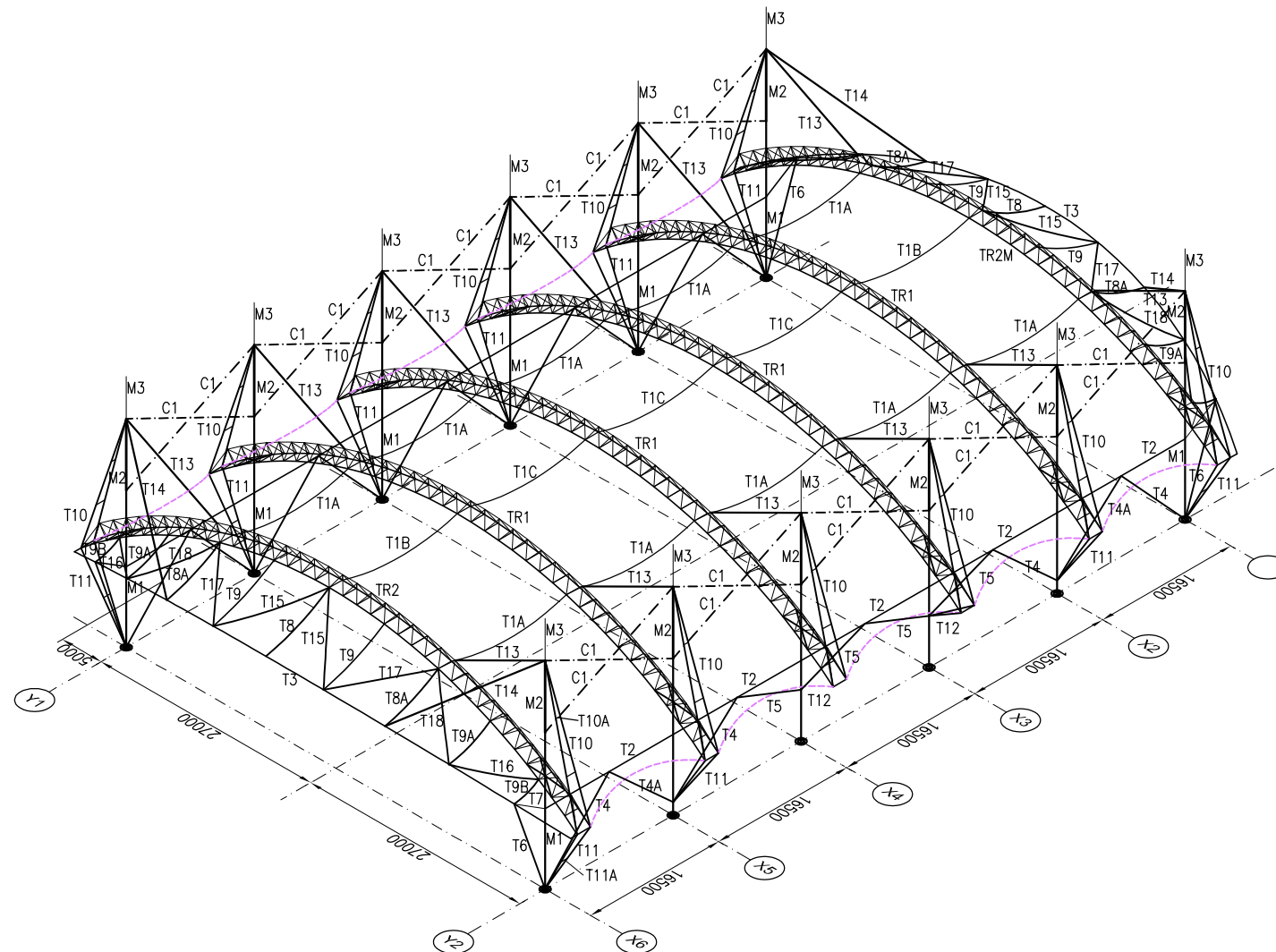


TYPICAL HOLDING DOWN BOLT DETAIL





STEEL STRUCTURE FRAMING PLAN



3D-VIEW STEEL STRUCTURE FRAMING

MEMBER SIZING

MARKING	DESCRIPTION	GENERAL SIZE
M1	BOTTOM MAST	CHS 609ø x 16mm THK
M2	INTERMEDIATE MAST	CHS 406ø x 12.5mm THK
M3	TOP MAST	CHS 168ø x 6mm THK
TR1	TOP CHORD	CHS 219ø x 6mm THK
	BOTTOM CHORD	CHS 219ø x 6mm THK
	DIAGONAL & HORIZONTAL	CHS 89ø x 4mm THK
T1A	TIE BETWEEN TRUSS TR1/TR2	CHS 273ø x 9mm THK
T1B	TIE BETWEEN TRUSS TR1/TR2	CHS 273ø x 9mm THK
T1C	TIE BETWEEN TRUSS TR1	CHS 273ø x 8mm THK
T2	TIE BETWEEN COLUMN	CHS 273ø x 9mm THK
T3	CURVED EDGE BEAM	CHS 273ø x 9mm THK
T4	NORMAL BRACING FOR T2	CHS 219ø x 6mm THK
T4A	NORMAL BRACING FOR T2	CHS 219ø x 9mm THK
T5	SHORT BRACING FOR T2	CHS 219ø x 6mm THK
T6	LOWER PROP TO T3	CHS 219ø x 6mm THK
T7	UPPER PROP TO T3	CHS 219ø x 9mm THK
T8	TIE FOR T3	CHS 168ø x 7mm THK
T8A	TIE FOR T3	CHS 168ø x 7mm THK
T9	TIE FOR T3	CHS 168ø x 6mm THK
T9A	TIE FOR T3	CHS 168ø x 6mm THK
T9B	TIE FOR T3	CHS 168ø x 6mm THK
T10	MAST UPPER BACKSTAY	2 X CHS 168ø x 7mm THK
T10A	TIE BETWEEN T10	2 X CHS 73ø x 5.16mm THK

MEMBER SIZING

MARKING	DESCRIPTION	GENERAL SIZE
T11	MAST LOWER BACKSTAY	2 X CHS 168ø x 7mm THK
T11A	TIE BETWEEN T11	CHS 73ø x 5.16mm THK
T12	SHORTENED MAST LOWER BACKSTAY	CHS 168ø x 7mm THK
T13	MAST FRONTSTAY TO TR1	CHS 219ø x 9mm THK
T14	MAST FRONTSTAY TO T3	CHS 219ø x 9mm THK
T15	DIAGONAL BRACING FOR T3	CHS 168ø x 11mm THK
T16	DIAGONAL BRACING FOR T3	CHS 168ø x 11mm THK
T17	DIAGONAL BRACING FOR T3	CHS 177ø x 8mm THK
T18	DIAGONAL BRACING FOR T3	CHS 177ø x 8mm THK
C1	MAST STABILIZING CABLE	16ø GALVANIZED WIRE ROPE
C2	FABRIC BORDER CABLE	28ø GALVANIZED WIRE ROPE WITH PE COVER

Kompleks Kolam Renang

NOTE : 58

REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :

MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAKS : 5130644

MAIN CONTRACTOR :
SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN,
 PAHANG DARUL MAKMUR
 TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :

dzj & ASSOCIATES ARCHITECTS
SENDIRIAN BERHAD (708290-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:

TRI-ARCH sdn. bhd.
 7-JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 59200 KUALA LUMPUR.
 TEL : 79612070 FAX : 79618210
 E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:

SEDIABENA sdn. bhd.
 No. 11, Jalan Jaya 9/11, Sungai Ud Bakti, 41300 Seremban, Selangor Darul Ehsan, Malaysia.
 Tel: 06-79612070 Fax: 06-79612022
 (Company No: 957547) web: www.sediabena.com

TRANSERVE TRANSERVE PTE LTD
 (In Reg. No: 1977243M)
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3069 Fax: (65) 6268 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:

JURUNING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :

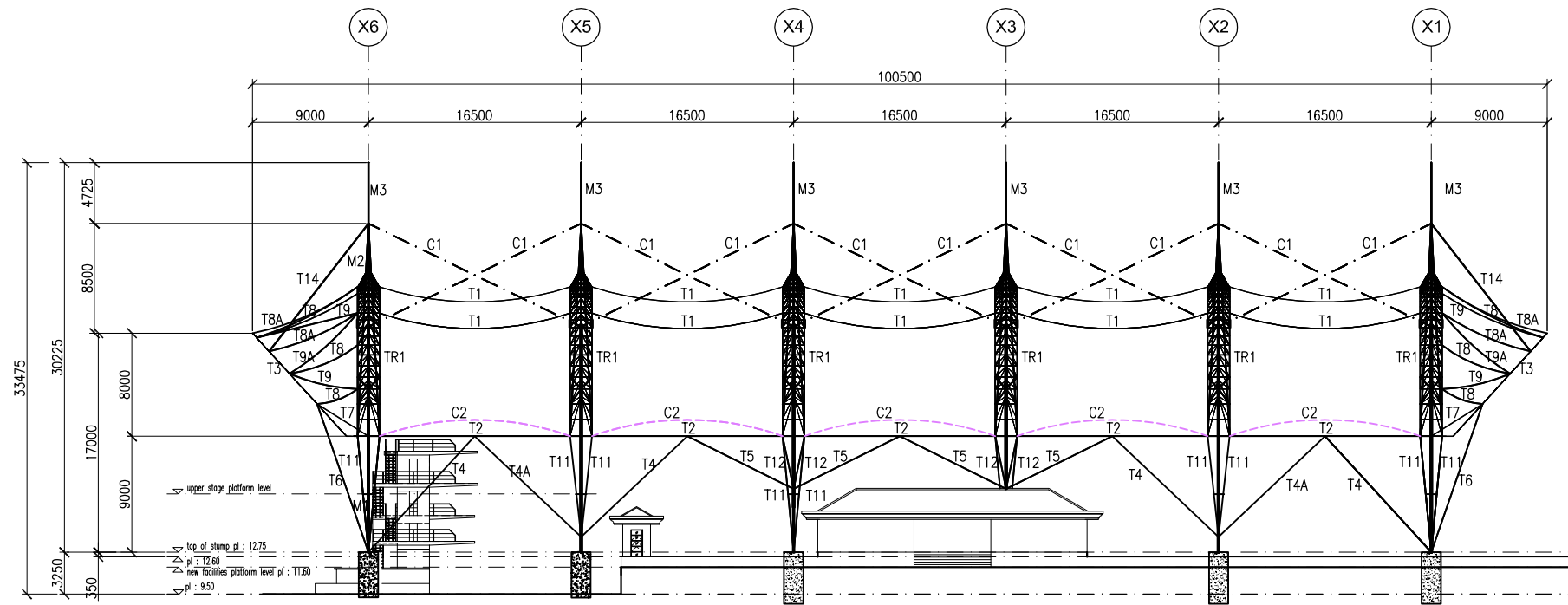
PENDITA
 NO.C-9-9, Level 11, Menara Ujang Emas,
 85 Jalan Lake*Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :
**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN. MALAYSIA.**

TITLE :
STEEL STRUCTURE FRAMING PLAN

DATE : 29.12.2011	DRAWN :
SCALE : 1 : 600	CHECKED :
DRAWING NO. : TA-Q326-04	REVISION 03

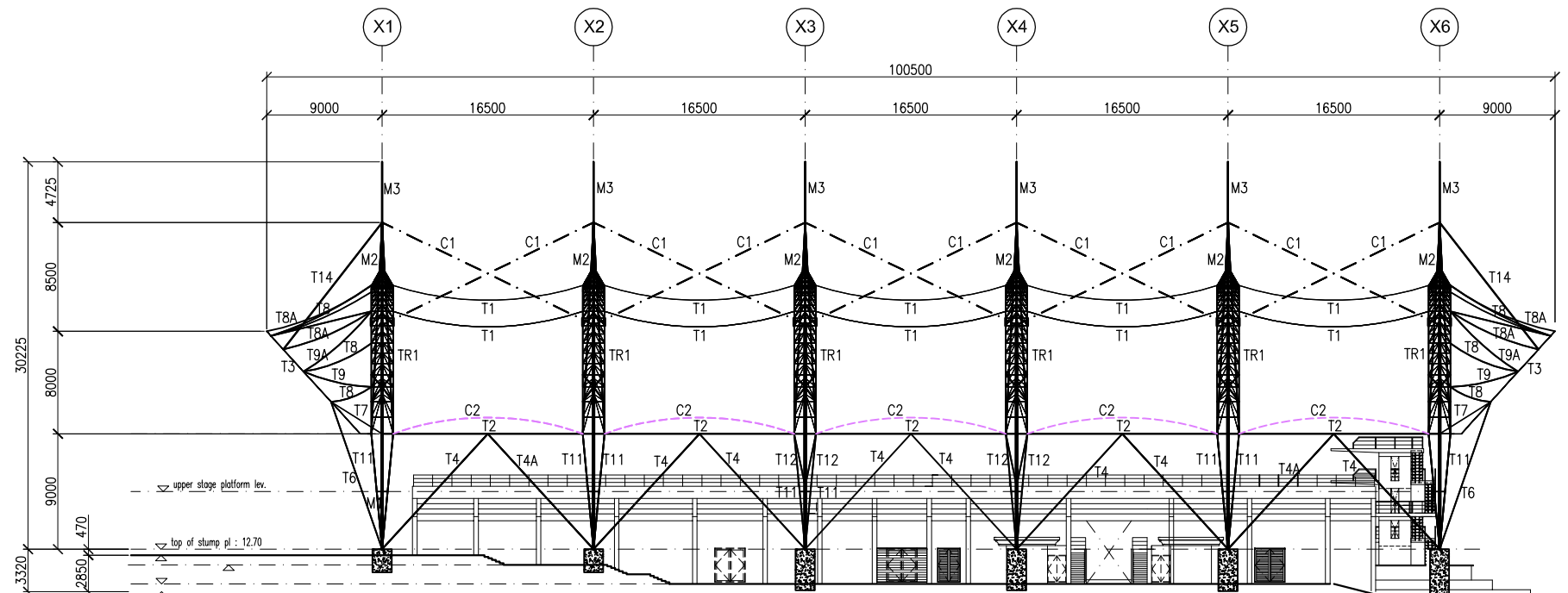




FRONT ELEVATION OF STRUCTURE FRAMING

MEMBER SIZING

MARKING	DESCRIPTION	GENERAL SIZE
M1	BOTTOM MAST	CHS 609ø x 16mm THK
M2	INTERMEDIATE MAST	CHS 406ø x 12.5mm THK
M3	TOP MAST	CHS 168ø x 6mm THK
TR1	TOP CHORD	CHS 219ø x 6mm THK
	BOTTOM CHORD	CHS 219ø x 6mm THK
	DIAGONAL & HORIZONTAL	CHS 89ø x 4mm THK
T1A	TIE BETWEEN TRUSS TR1/TR2	CHS 273ø x 9mm THK
T1B	TIE BETWEEN TRUSS TR1/TR2	CHS 273ø x 9mm THK
T1C	TIE BETWEEN TRUSS TR1	CHS 273ø x 8mm THK
T2	TIE BETWEEN COLUMN	CHS 273ø x 9mm THK
T3	CURVED EDGE BEAM	CHS 273ø x 9mm THK
T4	NORMAL BRACING FOR T2	CHS 219ø x 6mm THK
T4A	NORMAL BRACING FOR T2	CHS 219ø x 9mm THK
T5	SHORT BRACING FOR T2	CHS 219ø x 6mm THK
T6	LOWER PROP TO T3	CHS 219ø x 6mm THK
T7	UPPER PROP TO T3	CHS 219ø x 9mm THK
T8	TIE FOR T3	CHS 168ø x 7mm THK
T8A	TIE FOR T3	CHS 168ø x 7mm THK
T9	TIE FOR T3	CHS 168ø x 6mm THK
T9A	TIE FOR T3	CHS 168ø x 6mm THK
T9B	TIE FOR T3	CHS 168ø x 6mm THK
T10	MAST UPPER BACKSTAY	2 X CHS 168ø x 7mm THK
T10A	TIE BETWEEN T10	2 X CHS 73ø x 5.16mm THK
T11	MAST LOWER BACKSTAY	2 X CHS 168ø x 7mm THK
T11A	TIE BETWEEN T11	CHS 73ø x 5.16mm THK
T12	SHORTENED MAST LOWER BACKSTAY	CHS 168ø x 8mm THK
T13	MAST FRONTSTAY TO TR1	CHS 219ø x 9mm THK
T14	MAST FRONTSTAY TO T3	CHS 219ø x 9mm THK
T15	DIAGONAL BRACING FOR T3	CHS 168ø x 11mm THK
T16	DIAGONAL BRACING FOR T3	CHS 168ø x 11mm THK
T17	DIAGONAL BRACING FOR T3	CHS 177ø x 8mm THK
T18	DIAGONAL BRACING FOR T3	CHS 177ø x 8mm THK
C1	MAST STABILIZING CABLE	16ø GALVANIZED WIRE ROPE
C2	FABRIC BORDER CABLE	28ø GALVANIZED WIRE ROPE WITH PE COVER



REAR ELEVATION OF STRUCTURE FRAMING

Kompleks Kolam Renang

NOTE : 59

REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :



MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN,
 PAHANG DARUL MAKMUR
 TEL : 609-515 2473, FAX : 603-516 2619

ARCHITECT'S :




dzj & ASSOCIATES ARCHITECTS
BENDIRIAN BERHAD (70880-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:




TRI-ARCH sdn. bhd.
 7-JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 59200 KUALA LUMPUR,
 TEL : 7981 2870 FAX : 7981 8210
 E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
 No. 11, Jalan Uluu, Seberang Perai, 13400 Butterworth,
 Pulau Pinang.
 Tel: 04-5251221 Fax: 04-5251222
 Email: info@sedibena.com

&



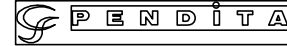
TRANSERVE PTE LTD
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3069 Fax: (65) 6268 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:



JURUNDING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



PENDITA
 NO. C-9-9, Level 11, Menara Ujang Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :

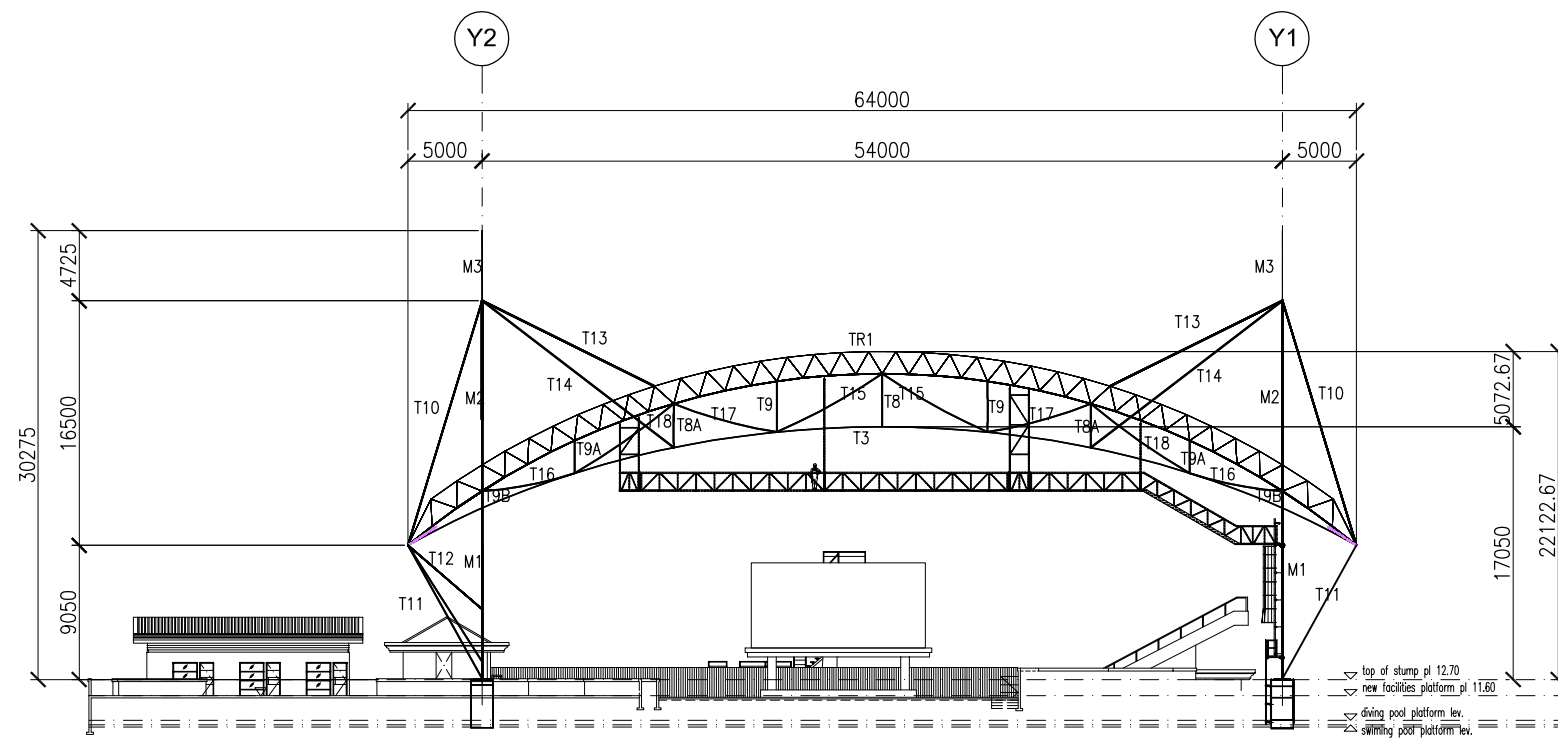
**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN, MALAYSIA.**

TITLE :

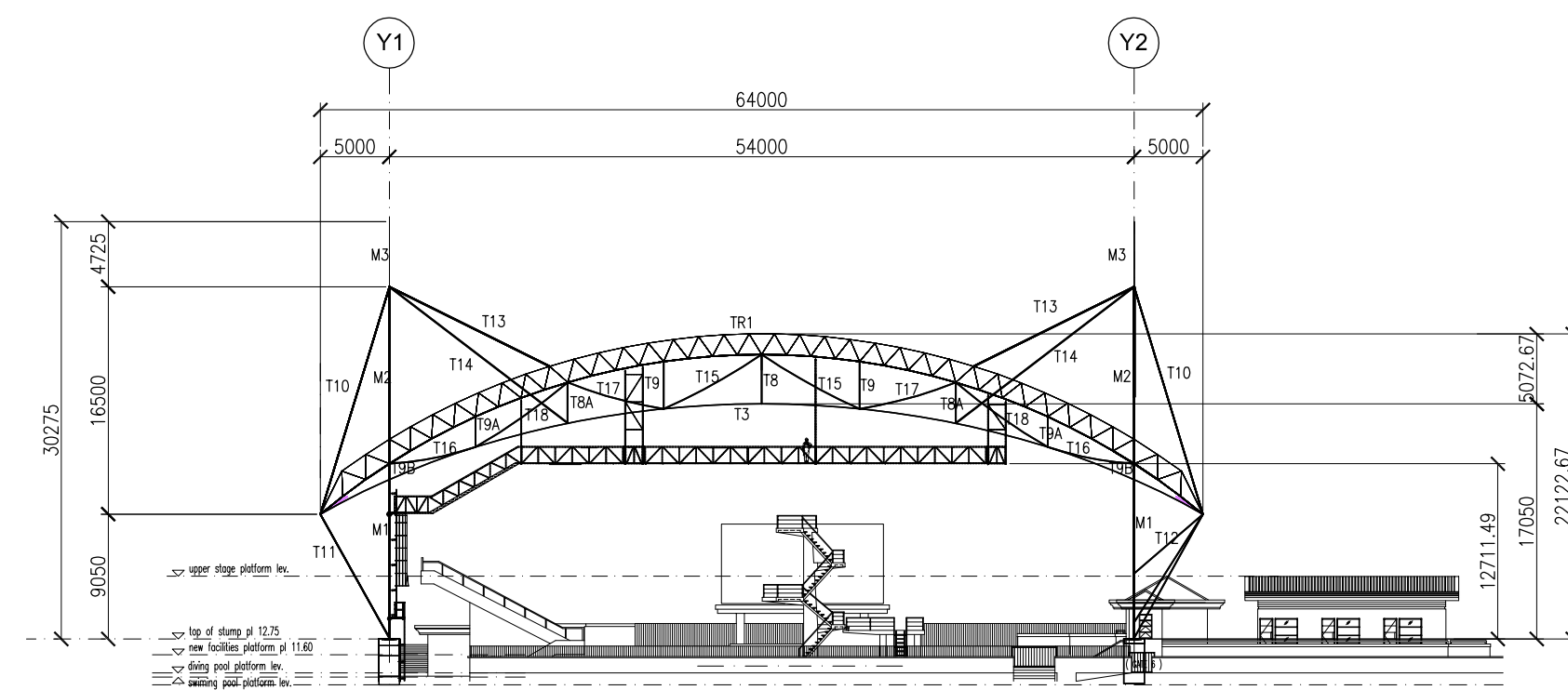
FRONT ELEVATION
 REAR ELEVATION

DATE : 14.12.2011	DRAWN :
SCALE : 1 : 500	CHECKED :
DRAWING NO. : TA-Q326-05	REVISION 03





RIGHT ELEVATION



LEFT ELEVATION

MEMBER SIZING

MARKING	DESCRIPTION	GENERAL SIZE
M1	BOTTOM MAST	CHS 609ø x 16mm THK
M2	INTERMEDIATE MAST	CHS 406ø x 12.5mm THK
M3	TOP MAST	CHS 168ø x 6mm THK
TR1	TOP CHORD	CHS 219ø x 6mm THK
	BOTTOM CHORD	CHS 219ø x 6mm THK
	DIAGONAL & HORIZONTAL	CHS 89ø x 4mm THK
T1A	TIE BETWEEN TRUSS TR1/TR2	CHS 273ø x 9mm THK
T1B	TIE BETWEEN TRUSS TR1/TR2	CHS 273ø x 9mm THK
T1C	TIE BETWEEN TRUSS TR1	CHS 273ø x 8mm THK
T2	TIE BETWEEN COLUMN	CHS 273ø x 9mm THK
T3	CURVED EDGE BEAM	CHS 273ø x 9mm THK
T4	NORMAL BRACING FOR T2	CHS 219ø x 6mm THK
T4A	NORMAL BRACING FOR T2	CHS 219ø x 9mm THK
T5	SHORT BRACING FOR T2	CHS 219ø x 6mm THK
T6	LOWER PROP TO T3	CHS 219ø x 6mm THK
T7	UPPER PROP TO T3	CHS 219ø x 9mm THK
T8	TIE FOR T3	CHS 168ø x 7mm THK
T8A	TIE FOR T3	CHS 168ø x 7mm THK
T9	TIE FOR T3	CHS 168ø x 6mm THK
T9A	TIE FOR T3	CHS 168ø x 6mm THK
T9B	TIE FOR T3	CHS 168ø x 6mm THK
T10	MAST UPPER BACKSTAY	2 X CHS 168ø x 7mm THK
T10A	TIE BETWEEN T10	2 X CHS 73ø x 5.16mm THK
T11	MAST LOWER BACKSTAY	2 X CHS 168ø x 7mm THK
T11A	TIE BETWEEN T11	CHS 73ø x 5.16mm THK
T12	SHORTENED MAST LOWER BACKSTAY	CHS 168ø x 8mm THK
T13	MAST FRONTSTAY TO TR1	CHS 219ø x 9mm THK
T14	MAST FRONTSTAY TO T3	CHS 219ø x 9mm THK
T15	DIAGONAL BRACING FOR T3	CHS 168ø x 11mm THK
T16	DIAGONAL BRACING FOR T3	CHS 168ø x 11mm THK
T17	DIAGONAL BRACING FOR T3	CHS 177ø x 8mm THK
T18	DIAGONAL BRACING FOR T3	CHS 177ø x 8mm THK
C1	MAST STABILIZING CABLE	16ø GALVANIZED WIRE ROPE
C2	FABRIC BORDER CABLE	28ø GALVANIZED WIRE ROPE WITH PE COVER

Kompleks Kolam Renang

NOTE : 60

NO	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :

MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644



MAIN CONTRACTOR :
SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUJIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN,
 PAHANG DARUL MAKMUR,
 TEL : 609-515 2473, FAX : 603-516 2619

ARCHITECTS :

dzj & ASSOCIATES ARCHITECTS
SENDIRIAN BERHAD (78888-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan Pahang Darul Makmur.
 Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:

TRI-ARCH sdn. bhd.
 7-1, JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF JALAN KUCHA LAMA,
 55000 KUALA LUMPUR
 TEL : 79812870 FAX : 79818210
 E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:

SEDIABENA SDN. BHD.
 No. 11, Jalan Industri, Sektor 13, 38100 Klang, 40150 Shah Alam, Selangor Darul Ehsan, Malaysia.
 Tel: 03-75071033 Fax: 03-75071022
 (Company No: 885594)
 &

TRANSERVE PTE LTD
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3069 Fax: (65) 6266 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:

JURUNING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKMP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :

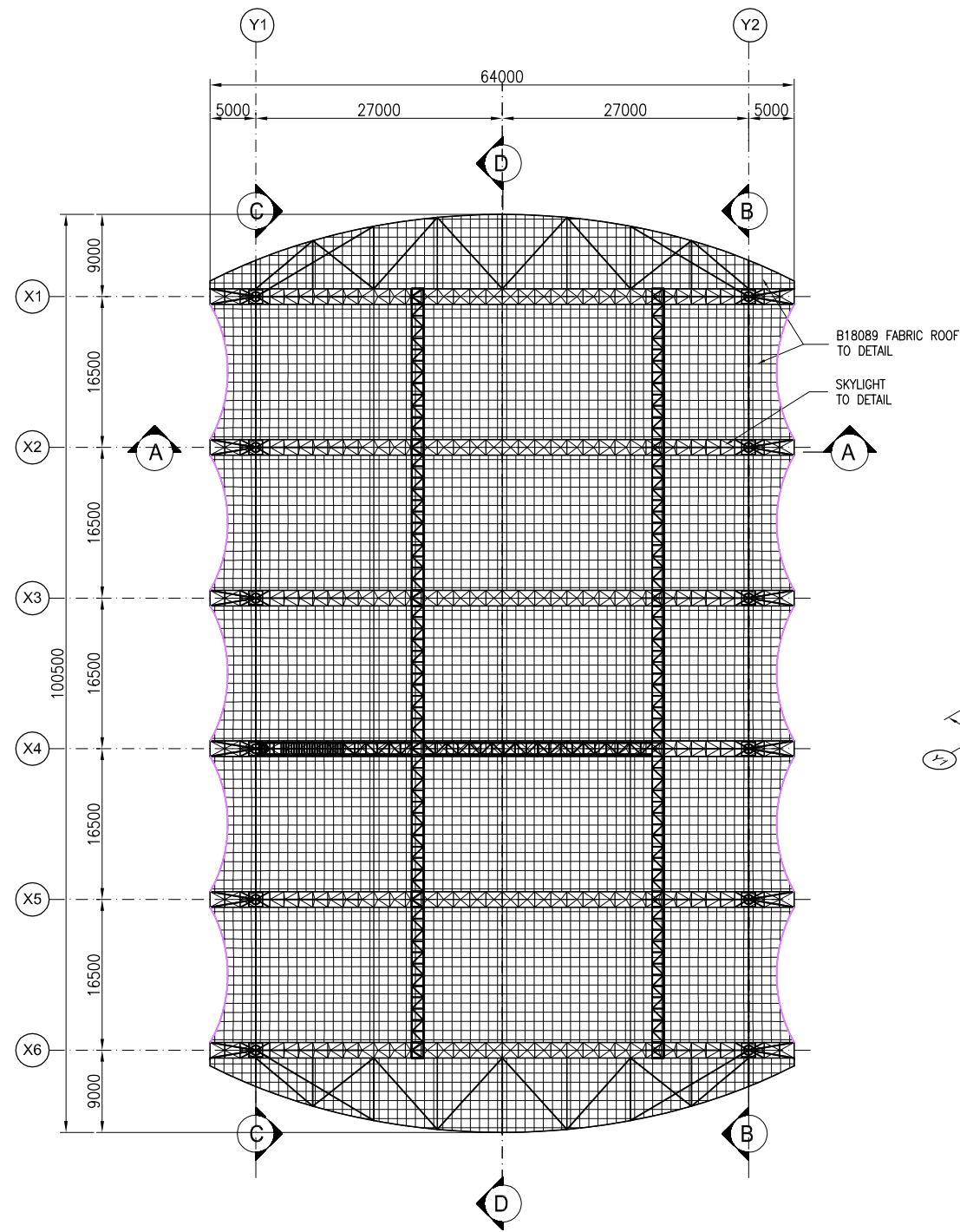
PENDITA
 NO.C-9-9, Level 11, Menara Uncoang Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :
**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN, MALAYSIA.**

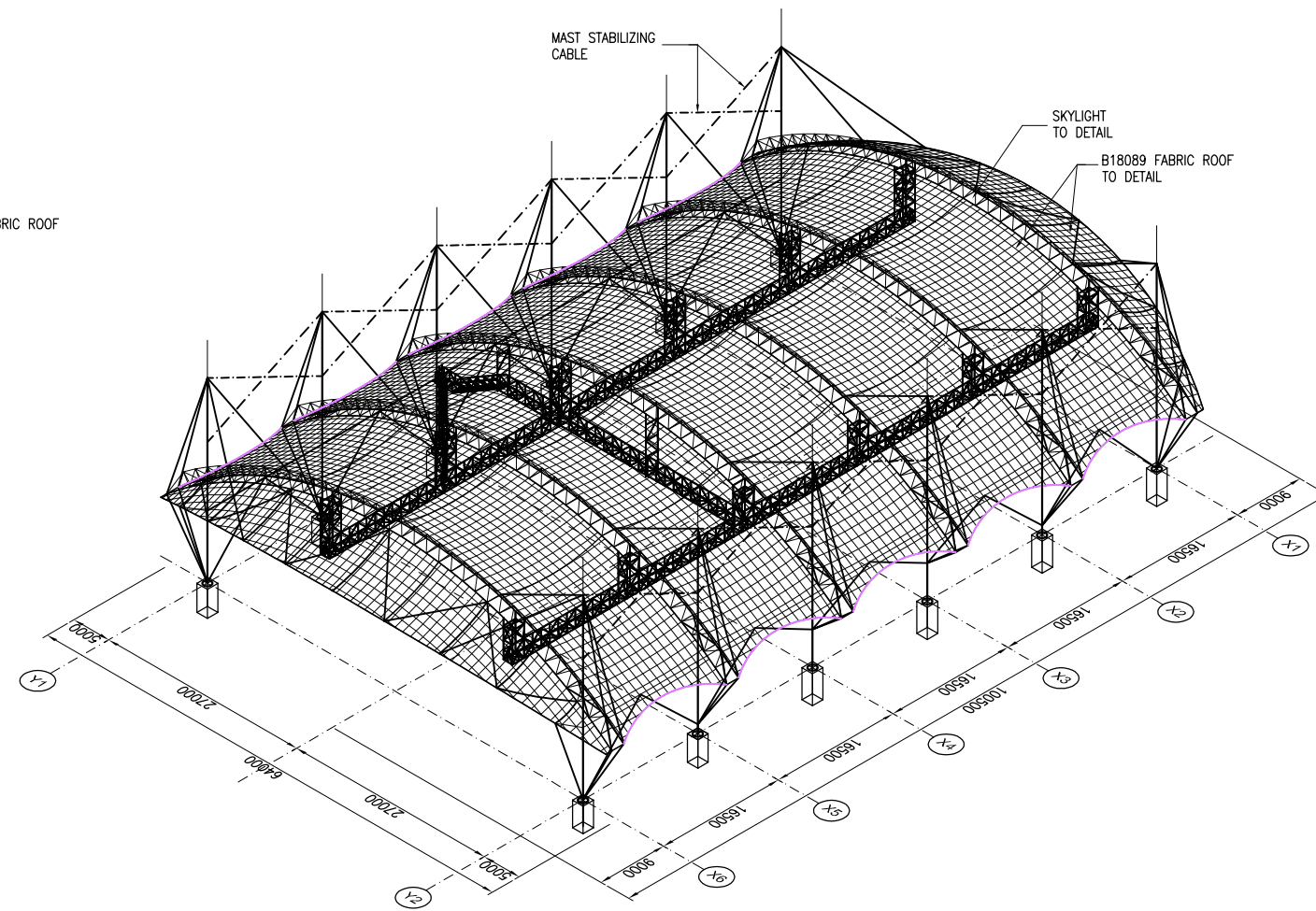
TITLE :
**RIGHT ELEVATION
 LEFT ELEVATION**

DATE : 29.12.2011	DRAWN :
SCALE : 1 : 500	CHECKED :
DRAWING NO. : TA-Q326-06	REVISION 03





FABRIC ROOF LAYOUT PLAN



3D-VIEW OF FABRIC ROOF LAYOUT

Kompleks Kolam Renang

NOTE : 61

REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :



MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.

117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN ,
 PAHANG DARUL MAKMUR
 TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :



dzj & ASSOCIATES ARCHITECTS
SENDIRIAN BERHAD (70890-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:



TRI-ARCH sdn. bhd.
 7-1, JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 59200 KUALA LUMPUR.
 TEL : 79612870 FAX : 79618210
 E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
 No. 11, Jalan Ulu Rengas, Seksyen 08, Bukit Mering, 41550 Bukit Mertajam, Pulau Pinang.
 Tel: 04-5812012 Fax: 04-5812022
 E-mail: info@sedibena.com.my



TRANSERVE PTE LTD
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3069 Fax: (65) 6266 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:



JURUNDING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



NO. C-9-9, Level 11, Menara Ujang Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :

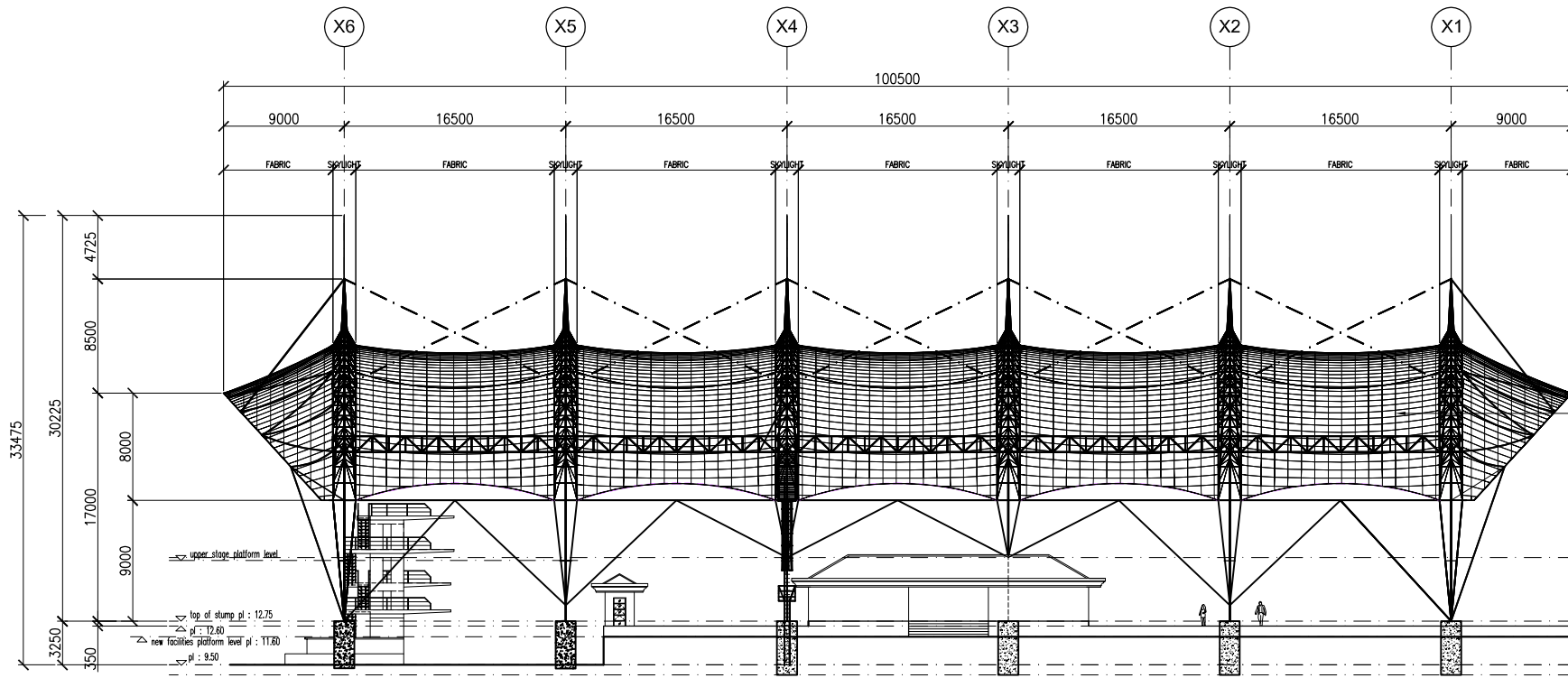
**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN, MALAYSIA.**

TITLE :

FABRIC ROOF LAYOUT PLAN
 3D-VIEW OF FABRIC ROOF LAYOUT

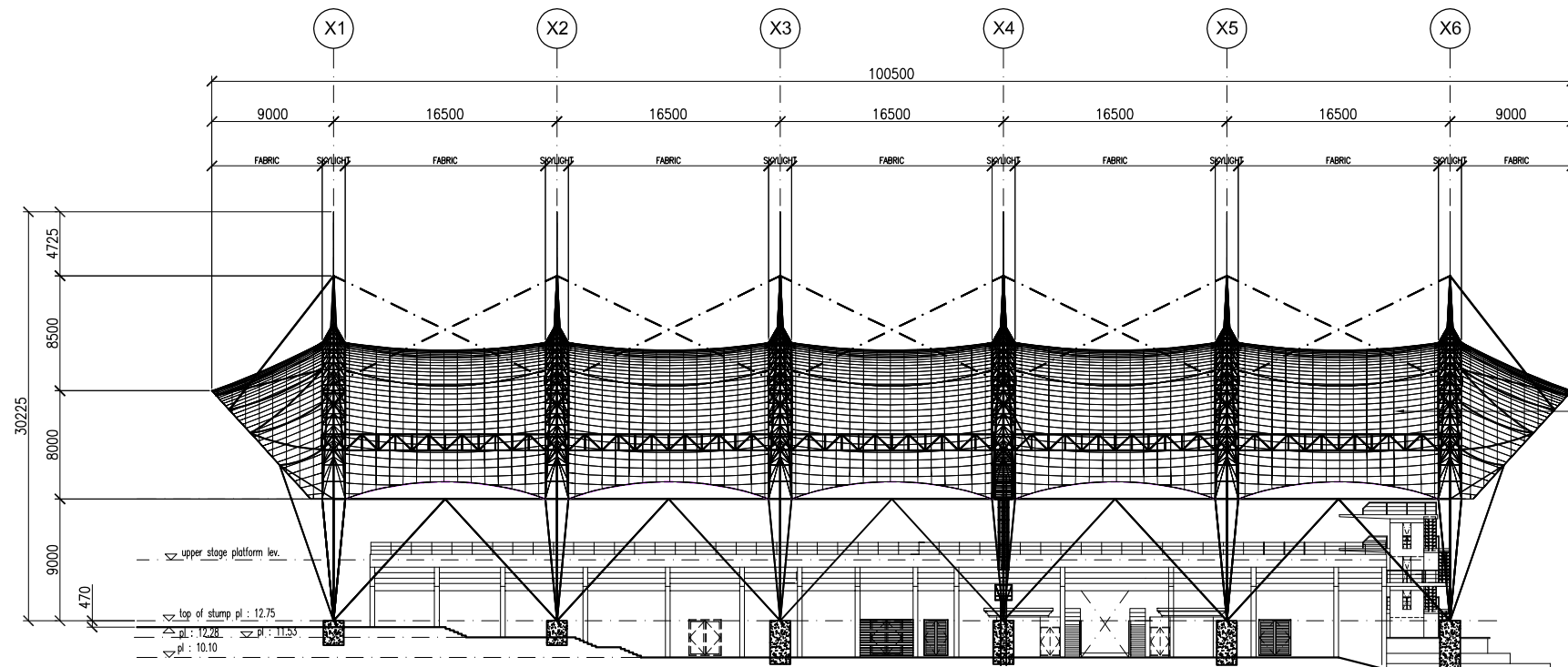
DATE : 28.12.2011	DRAWN :
SCALE : 1 : 700	CHECKED :
DRAWING NO. : TA-Q326-07	REVISION 03





FRONT ELEVATION OF
STRUCTURE FRAMING + FABRIC

B18089 FABRIC ROOF
TO DETAIL



REAR ELEVATION OF
STRUCTURE FRAMING + FABRIC

B18089 PTFE
COATED FABRIC ROOF

Kompleks Kolam Renang

NOTE : 62

REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :



MAJLIS PERBANDARAN KUANTAN
Jalan Tanah Putih, 25100 Kuantan,
Pahang Darul Makmur, Malaysia.
TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.

117-A, 1st. FLOOR, MUIP BUILDING,
JALAN MAHKOTA, 25000 KUANTAN ,
PAHANG DARUL MAKMUR
TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :



dzj & ASSOCIATES ARCHITECTS
BENDIRIAN BERHAD (70890-P)
B-26, Tingkat Satu, Jalan IM3/10
Bandar Indera Mahkota
25200 Kuantan, Pahang Darul Makmur.
Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:



TRI-ARCH sdn. bhd.
7-JALAN 2/115A, TAMAN PAGAR RUYONG
OFF. JALAN KUCHAI LAMA,
59200 KUALA LUMPUR.
TEL : 7981 2870 FAX : 7981 8210
E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
No. 11, Jalan Ulu Ulu, Segar, 41500 Segar, Selangor Darul Ehsan, Kuala Lumpur.
Tel: 03-92082281 Fax: 03-92082282
Gomen: 03-92082281
E-mail: info@sedibena.com.my
www.sedibena.com



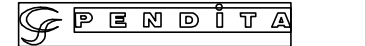
TRANSERVE PTE LTD
39 PANDAN ROAD, JURONG, SINGAPORE 609281
Tel: (65) 6268 3069 Fax: (65) 6266 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:



JURUNDING HYH SDN. BHD.
A-7732, Tingkat Satu, Kedai LKNP,
Jalan Dato' Bahaman, 25200 Kuantan,
Pahang Darul Makmur.
Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



NO. C-9-9, Level 11, Menara Ujang Emas,
85 Jalan Loke Yew, 55200 Kuala Lumpur
Tel : 03-92008268 Fax : 03-92008276 (391855-V)
email: info@pendita.com.my website: pendita.com.my

PROJECT :

**CADANGAN MENAIK TARAF
KOLAM RENANG SERTA KERJA-KERJA
BERKAITAN DI WISMA BELIA,
INDERA MAHKOTA, KUANTAN, MALAYSIA.**

TITLE :

FRONT ELEVATION OF STRUCTURE FRAMING + FABRIC
REAR ELEVATION OF STRUCTURE FRAMING + FABRIC

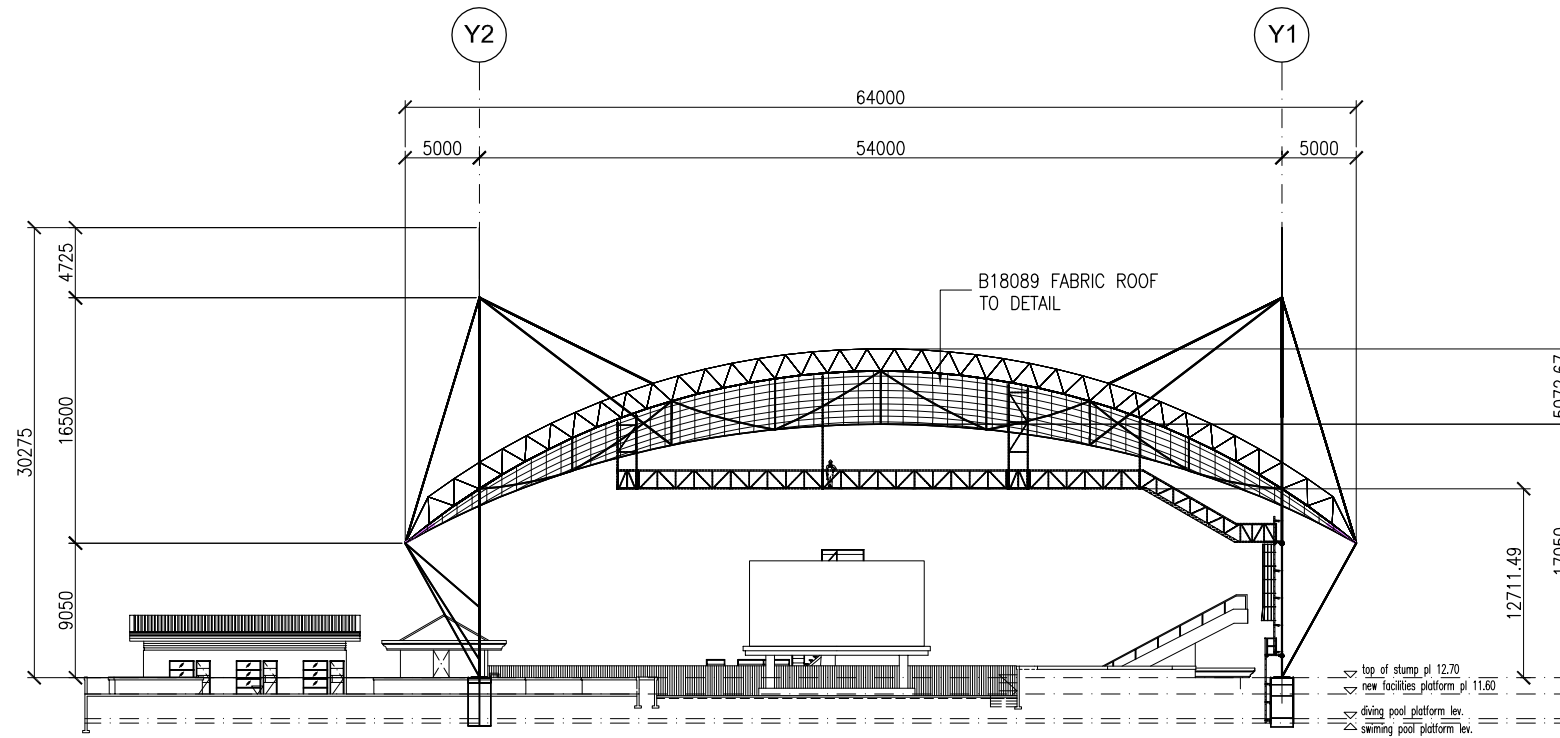
DATE : 29.12.2011 DRAWN :

SCALE : 1 : 500 CHECKED :

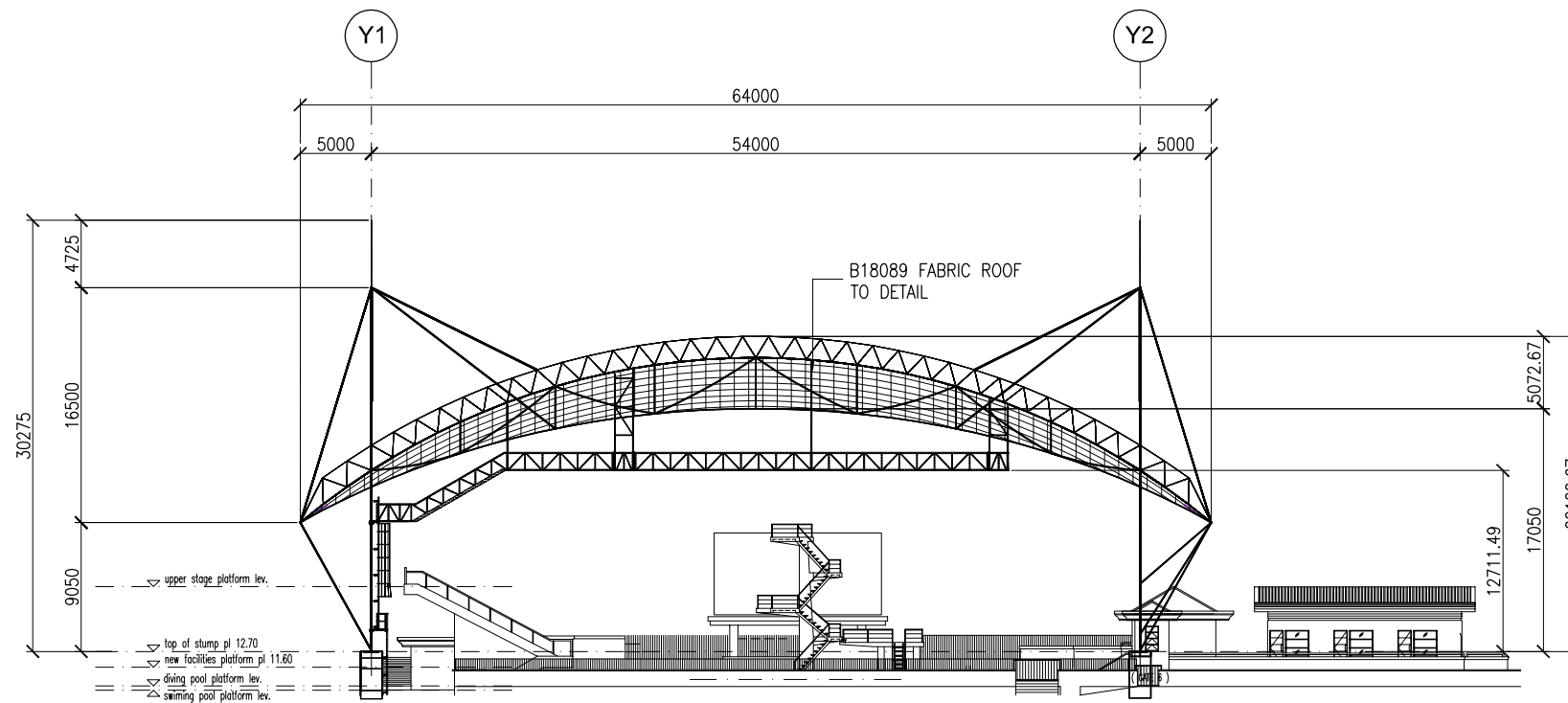
DRAWING NO. : REVISION

TA-Q326-08 03





RIGHT ELEVATION OF
STRUCTURE FRAMING + FABRIC



LEFT ELEVATION OF
STRUCTURE FRAMING + FABRIC

Kompleks Kolam Renang

NOTE : 63

REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :



MAJLIS PERBANDARAN KUANTAN
Jalan Tanah Putih, 25100 Kuantan,
Pahang Darul Makmur, Malaysia.
TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.

117-A, 1st. FLOOR, MUIP BUILDING,
JALAN MAHKOTA, 25000 KUANTAN ,
PAHANG DARUL MAKMUR
TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :



& ASSOCIATES ARCHITECTS
BENDIRIAN BERHAD (70890-P)
B-26, Tingkat Satu, Jalan IM3/10
Bandar Indera Mahkota
25200 Kuantan, Pahang Darul Makmur.
Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:



TRI-ARCH sdn. bhd.
7-JALAN 2/115A, TAMAN PAGAR RUYONG
OFF. JALAN KUCHAI LAMA,
59200 KUALA LUMPUR,
TEL : 7961 2870 FAX : 7961 8210
E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
No. 11, Jalan Ulu Ulu, Segar, 08, Bukit Mertajam, 14130 Simpang Ampat, Pulau
Pinang, Malaysia. Tel: 04-5730722 Fax: 04-5730722
E-mail: info@sedibena.com
www.sedibena.com



TRANSERVE PTE LTD
(In Reg. No. 19772436)
39 PANDAN ROAD, JURONG, SINGAPORE 609281
Tel: (65) 6268 3099 Fax: (65) 6266 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:



JURUNDING HYH SDN. BHD.
A-7732, Tingkat Satu, Kedai LKNP,
Jalan Dato' Bahaman, 25200 Kuantan,
Pahang Darul Makmur.
Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



NO. C-9-9, Level 11, Menara Ujang Emas,
85 Jalan Loke Yew, 55200 Kuala Lumpur
Tel : 03-92008268 Fax : 03-92008276 (391855-V)
email: info@pendita.com.my website: pendita.com.my

PROJECT :

**CADANGAN MENAIK TARAF
KOLAM RENANG SERTA KERJA-KERJA
BERKAITAN DI WISMA BELIA,
INDERA MAHKOTA, KUANTAN, MALAYSIA.**

TITLE :

RIGHT ELEVATION OF STRUCTURE FRAMING + FABRIC
LEFT ELEVATION OF STRUCTURE FRAMING + FABRIC

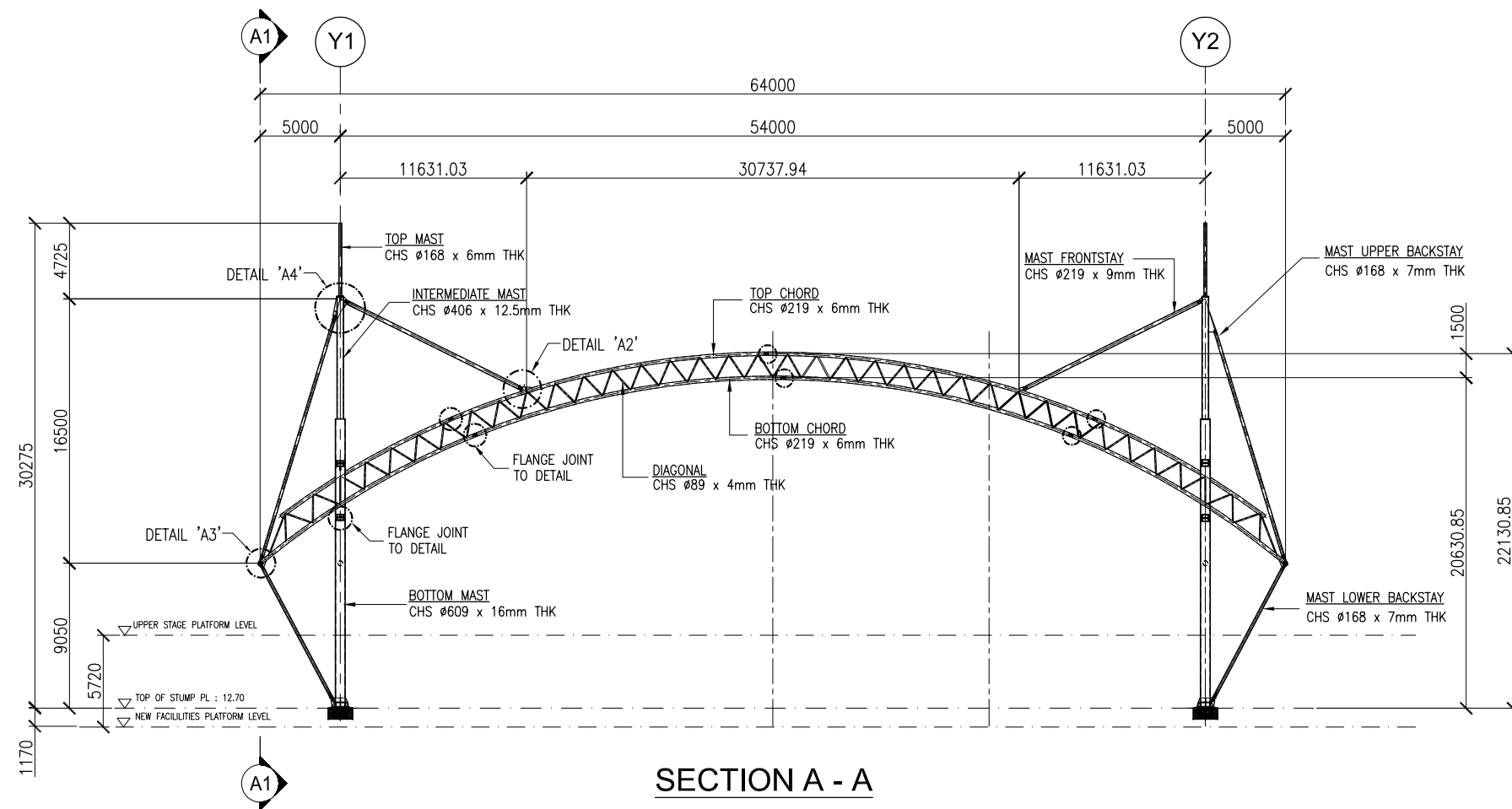
DATE : 29.12.2011 DRAWN :

SCALE : 1 : 500 CHECKED :

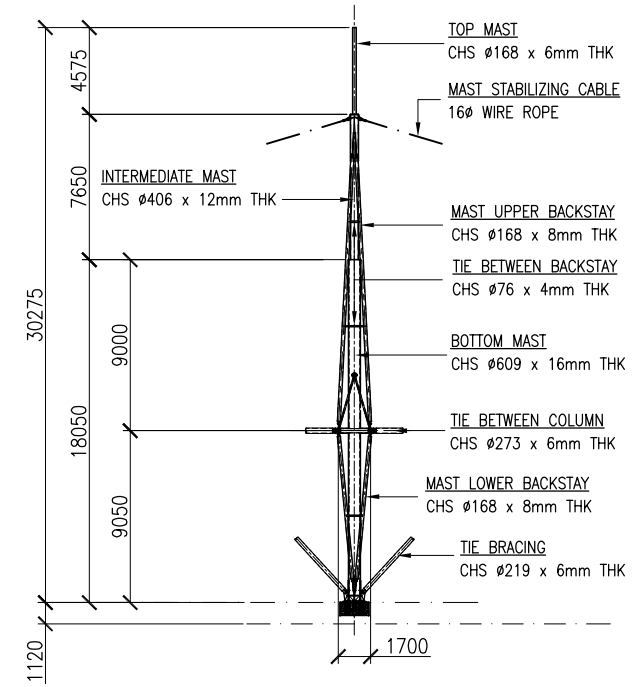
DRAWING NO. : REVISION

TA-Q326-09 03

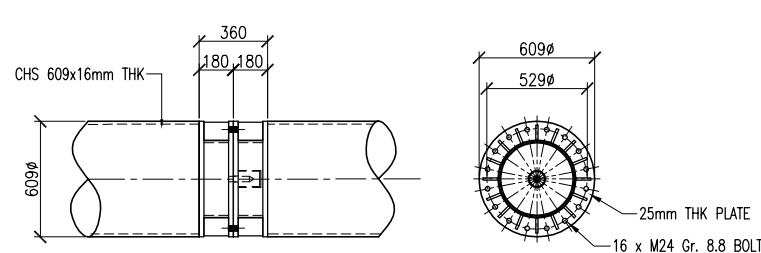




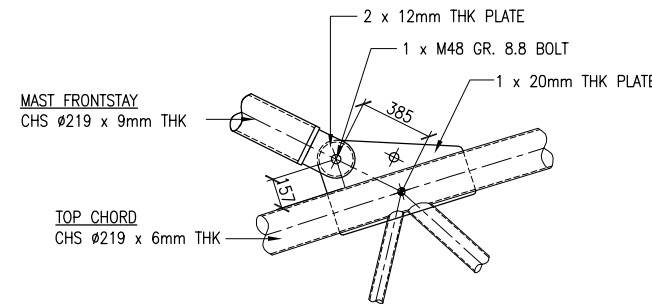
SECTION A - A



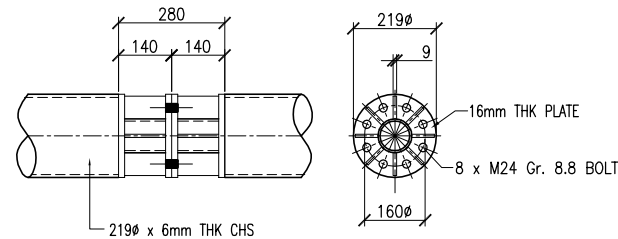
SECTION A1 - A1



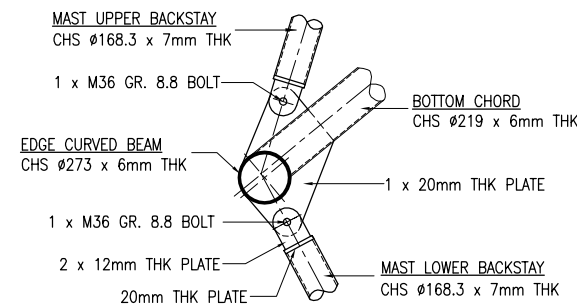
TYPICAL FLANGE JOINT FOR CHS 609Ø x 20mm THK



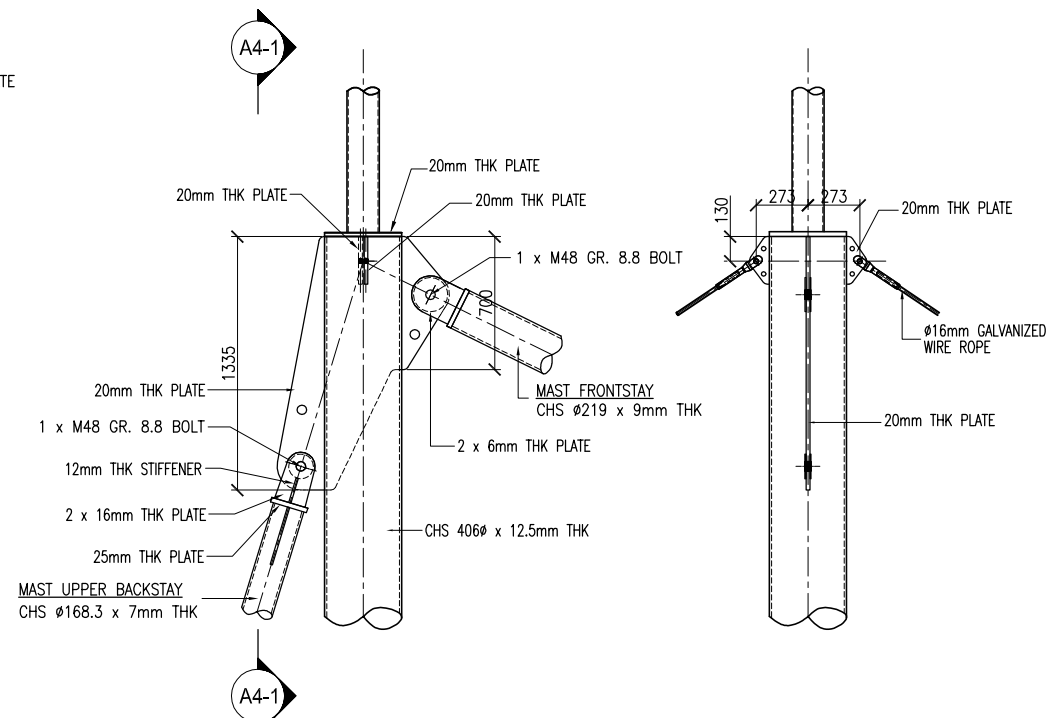
DETAIL 'A2'



TYPICAL FLANGE JOINT FOR CHS 219Ø x 6mm THK



DETAIL 'A3'



DETAIL 'A4'

VIEW A4-1 - A4-1

Kompleks Kolam Renang

NOTE : 64

REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :

MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644



MAIN CONTRACTOR :
SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN,
 PAHANG DARUL MAKMUR
 TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :

dzj & ASSOCIATES ARCHITECTS
BENDIRIAN BERHAD (70890-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel: 09-5736430 / 5736372 Fax: 09-5736443


SPECIALIST ROOF & CLADDING CONTRACTOR:

TRI-ARCH sdn. bhd.
 7-JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 59200 KUALA LUMPUR.
 TEL : 7961 2870 FAX : 7961 8210
 Email : triarch90@yahoo.com.my

IN CONJUNCTION WITH:

SEDIABENA sdn. bhd.
 No. 11, Jalan Ulu Ulu, Segar Hill Building, 4115 Star Hill, Selangor Darul Ehsan, Kuala Lumpur.
 Tel: 03-7691 2870 Fax: 03-7691 2222
 (Company No: 955754)
 &

TRANSERVE PTE LTD
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3099 Fax: (65) 6266 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:

JURUNING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

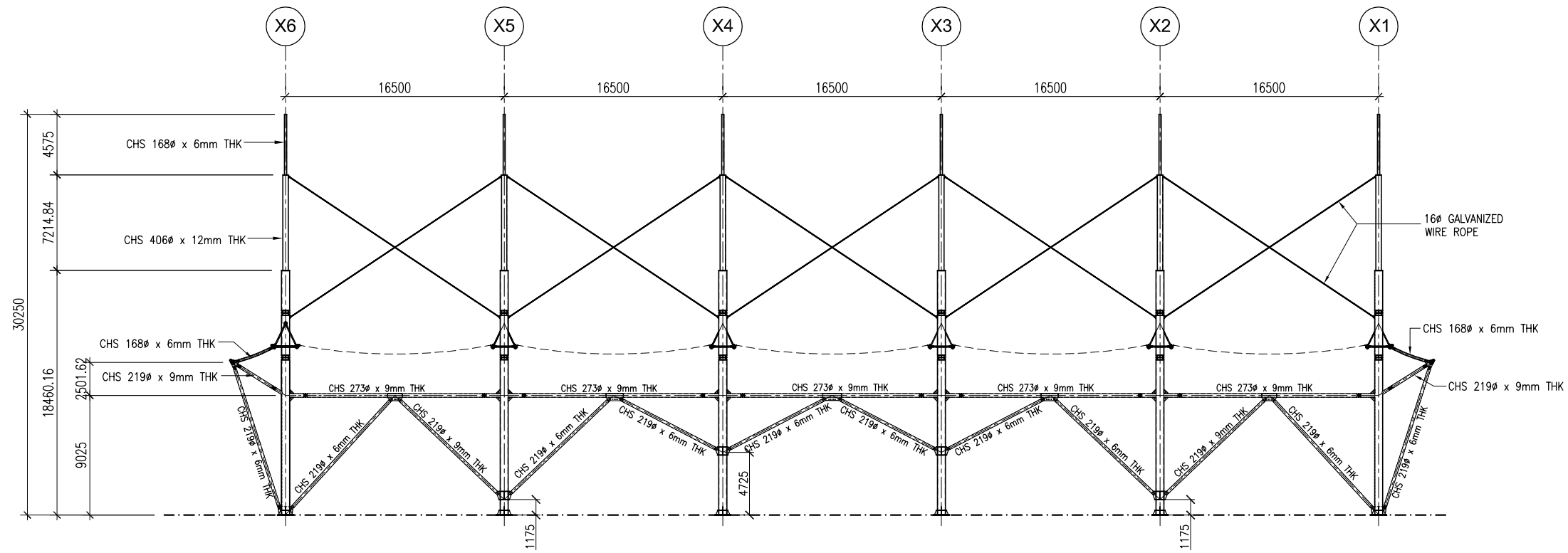
QUANTITY SURVEYOR :

PENDITA
 NO. C-9-9, Level 11, Menara Ujang Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :
**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN. MALAYSIA**

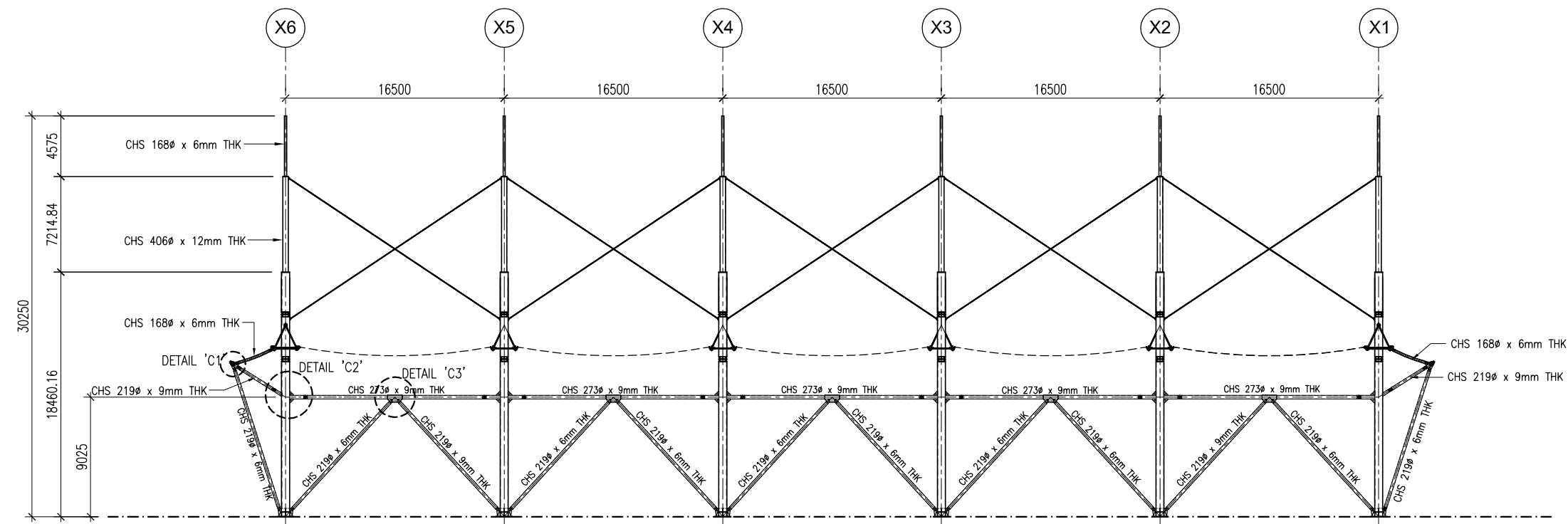
TITLE :
SECTION A-A & DETAILS

DATE : 29.12.2011	DRAWN :
SCALE : 1 : 600 1 : 10	CHECKED :
DRAWING NO. : TA-Q326-10	REVISION 03





SECTION B - B



SECTION C - C

Kompleks Kolam Renang

NOTE : 65

REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :



MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.

117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN,
 PAHANG DARUL MAKMUR
 TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :



B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:



7-JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 59200 KUALA LUMPUR.
 TEL : 79612870 FAX : 79618210
 E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



11, Jalan Ulu Ulu, Segar Hill Dam, 41300 Segar Hill, Selangor Darul Ehsan, Kuala Lumpur.
 Tel: 03-79612870 Fax: 03-79612871
 E-mail: info@sedibena.com website: www.sedibena.com

TRANSSERVE PTE LTD

39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6266 3069 Fax: (65) 6266 2324 Email: sales@transserve.com.sg

ENGINEER'S O&S and M&E:



A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



NO. C-9-9, Level 11, Menara Ujang Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :

**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN, MALAYSIA.**

TITLE :

SECTION B-B
 SECTION C-C

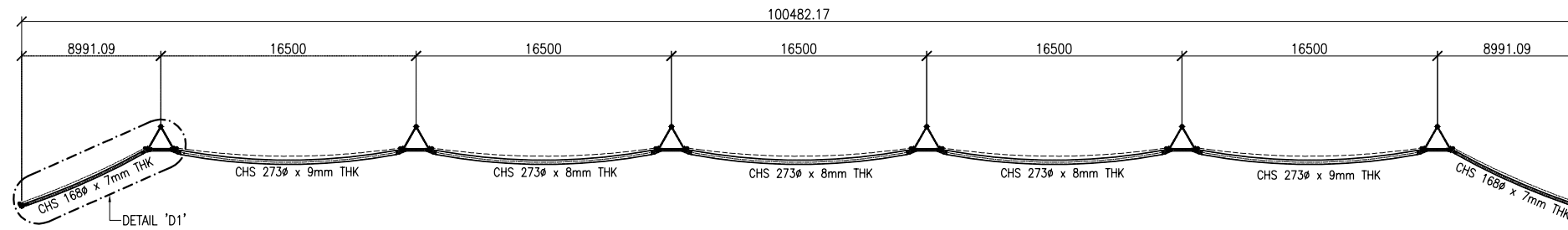
DATE : 29.12.2011 DRAWN :

SCALE : 1 : 400 CHECKED :

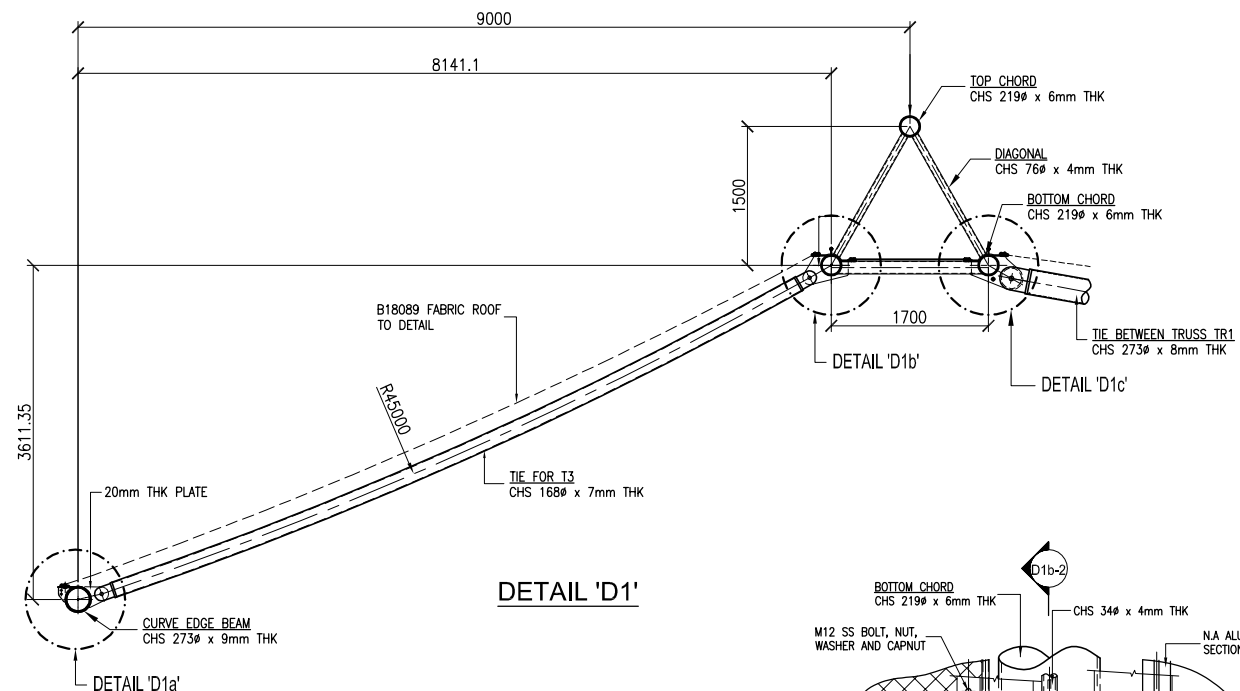
DRAWING NO. : REVISION

TA-Q326-11 03

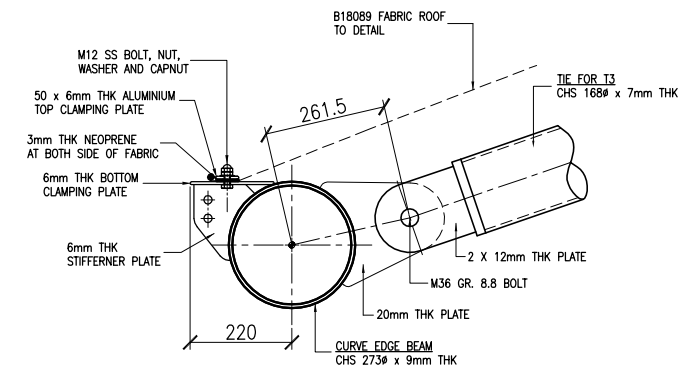




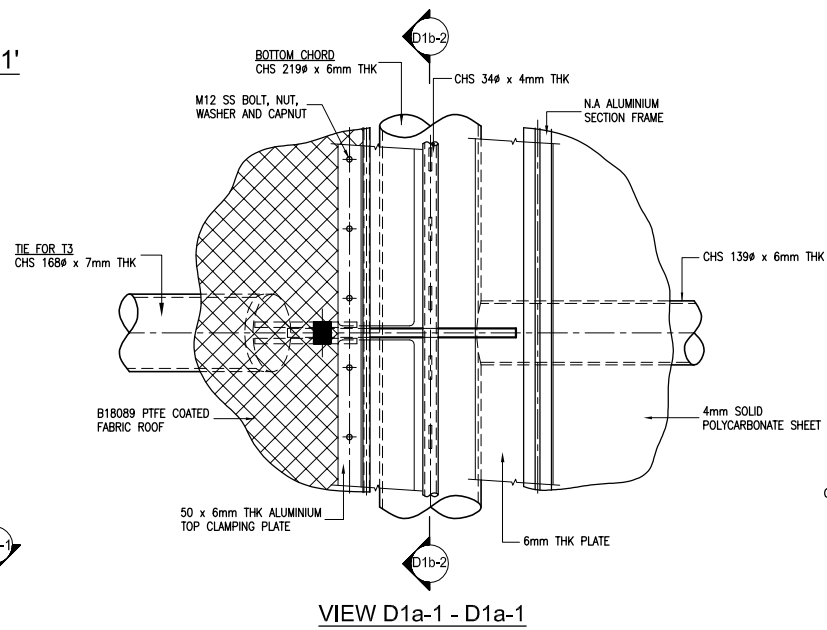
SECTION D - D



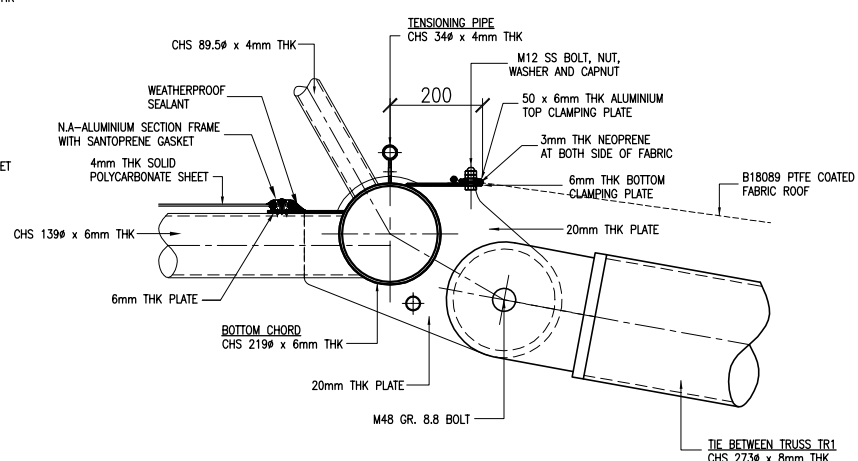
DETAIL 'D1'



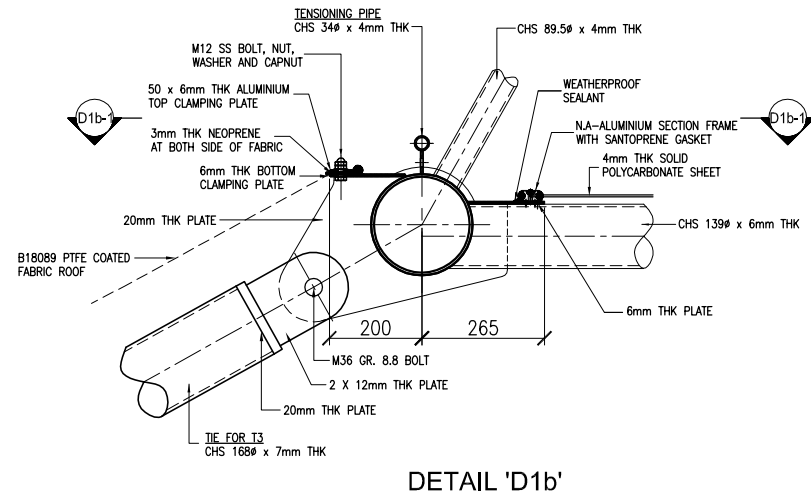
DETAIL 'D1a'



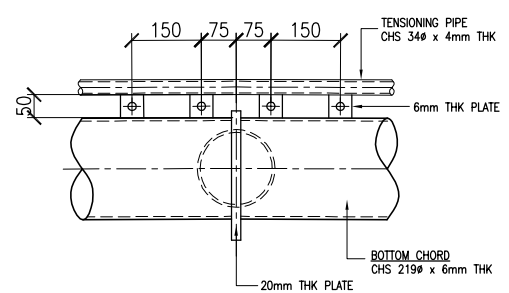
VIEW D1a-1 - D1a-1







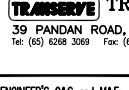


DETAIL 'D1c'



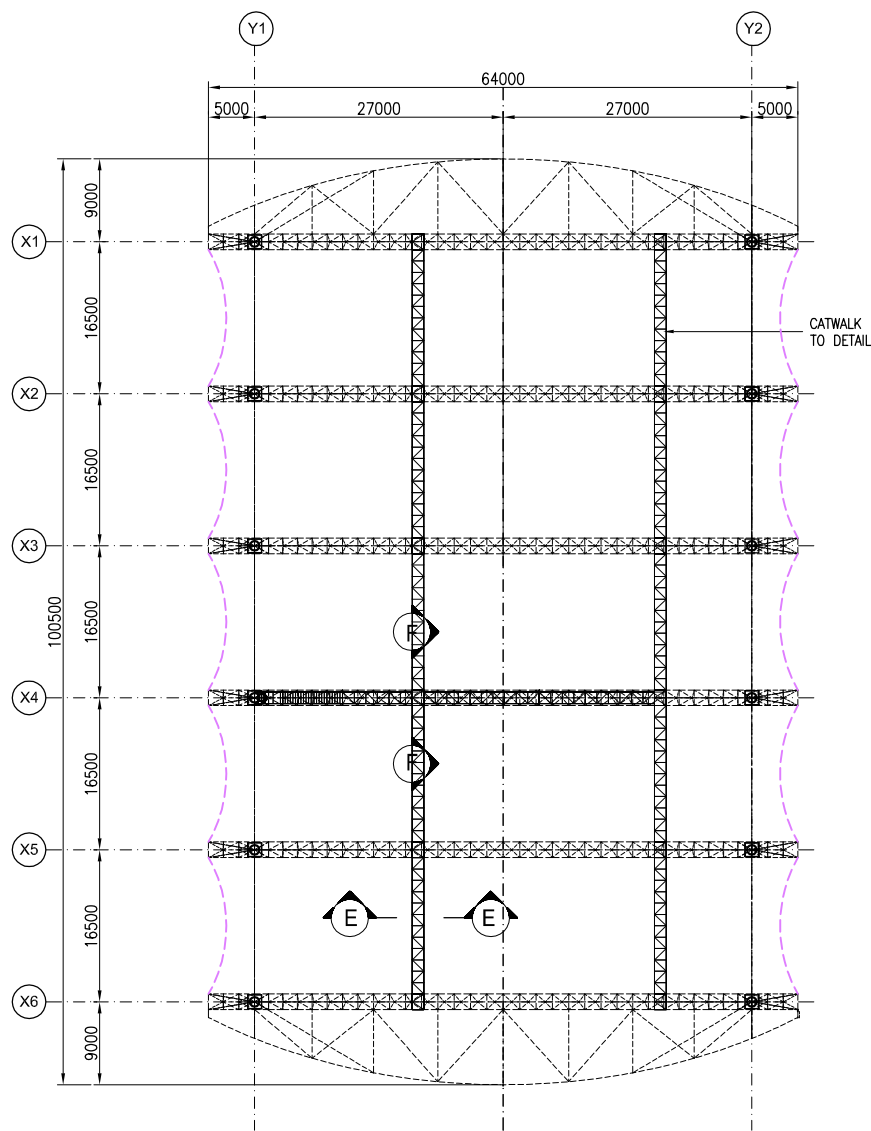
DETAIL 'D1b'



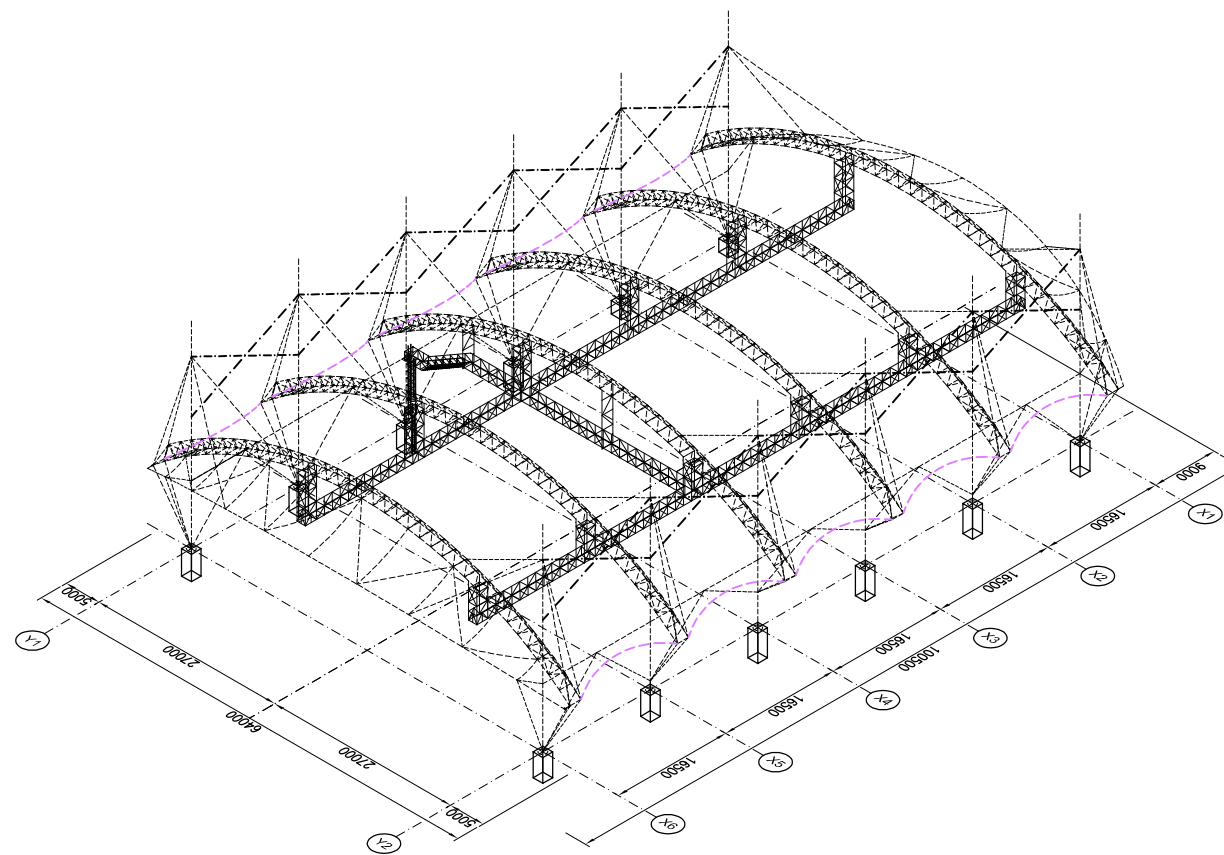
VIEW D1b-2 - D1b-2

Kompleks Kolam Renang		
NOTE :		66
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL
REF	DATE	DESCRIPTION
OWNER :		
 MAJLIS PERBANDARAN KUANTAN Jalan Tanah Putih, 25100 Kuantan, Pahang Darul Makmur, Malaysia. TEL : 09-5121555/666 FAXS : 5130644		
MAIN CONTRACTOR :		
SUARA HATI SDN. BHD. 117-A, 1st. FLOOR, MUIP BUILDING, JALAN MAHKOTA, 25000 KUANTAN , PAHANG DARUL MAKMUR TEL :609-515 2473, FAX : 603-516 2619		
ARCHITECT'S :		
 dzj & ASSOCIATES ARCHITECTS BENDIRIAN BERAHAD (709290-P) B-26, Tingkat Satu, Jalan IM3/10 Bandar Indera Mahkota 25200 Kuantan, Pahang Darul Makmur. Tel 09-5736430 / 5736372 Fax: 09-5736443		
SPECIALIST ROOF & CLADDING CONTRACTOR:		
 TRI-ARCH sdn. bhd. 7-JALAN 2/115A, TAMAN PAGAR RUYONG OFF. JALAN KUCHAI LAMA, 59200 KUALA LUMPUR, TEL : 79612070 FAX : 79618210 Email : triarch90@yahoo.com.my		
IN CONJUNCTION WITH:		
 SEDIABENA sdn. bhd. No. 11, Jalan Kerasi, Seberang Perak, 06000 Alor Setar, Kedah Darul Aman, Malaysia. Tel: 043661001 Fax: 043661002 Corp No: 302754 web: www.sediabena.com		
 TRANSERVE PTE LTD 39 PANDAN ROAD, JURONG, SINGAPORE 609281 Tel: (65) 6268 3069 Fax: (65) 6266 2324 Email: sales@transerve.com.sg		
ENGINEER'S C&S and M&E:		
 JURUNING HYH SDN. BHD. A-7732, Tingkat Satu, Kedai LKNP, Jalan Dato' Bahaman, 25200 Kuantan, Pahang Darul Makmur. Tel : 09-566 3031 Faks : 09-560 1182		
QUANTITY SURVEYOR :		
 PENDITA NO. C-9-9, Level 11, Menara Ujang Emas, 85 Jalan Lake Yew, 55200 Kuala Lumpur Tel : 03-92008268 Fax : 03-92008276 (391855-V) email: info@pendita.com.my website: pendita.com.my		
PROJECT :		
CADANGAN MENAIK TARAF KOLAM RENANG SERTA KERJA-KERJA BERKAITAN DI WISMA BELIA, INDERA MAHKOTA, KUANTAN. MALAYSIA.		
TITLE :		
SECTION D-D & DETAILS		
DATE : 29.12.2011	DRAWN :	
SCALE : 1 : 400 / 1 : 40	CHECKED :	
DRAWING NO. :		REVISION
TA-Q326-12		03

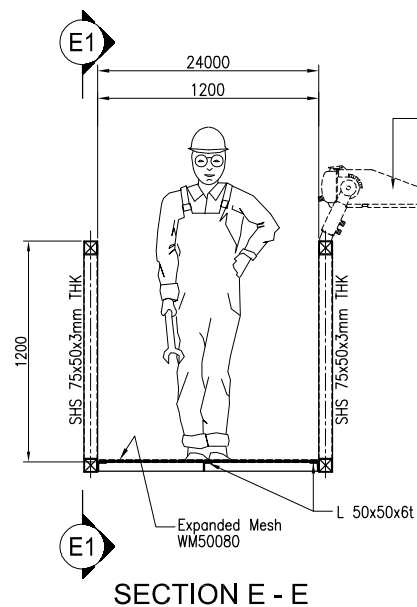




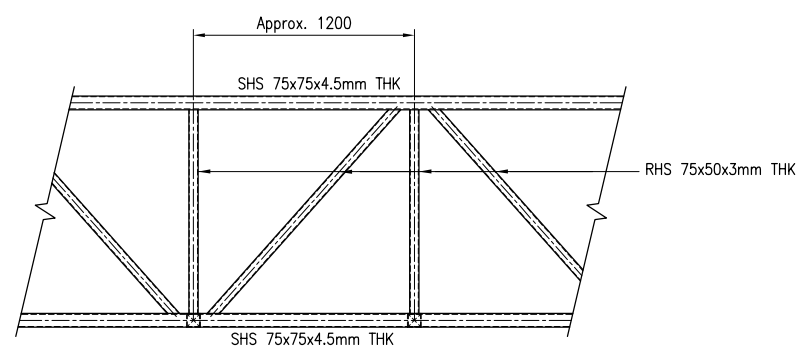
CATWALK LAYOUT PLAN



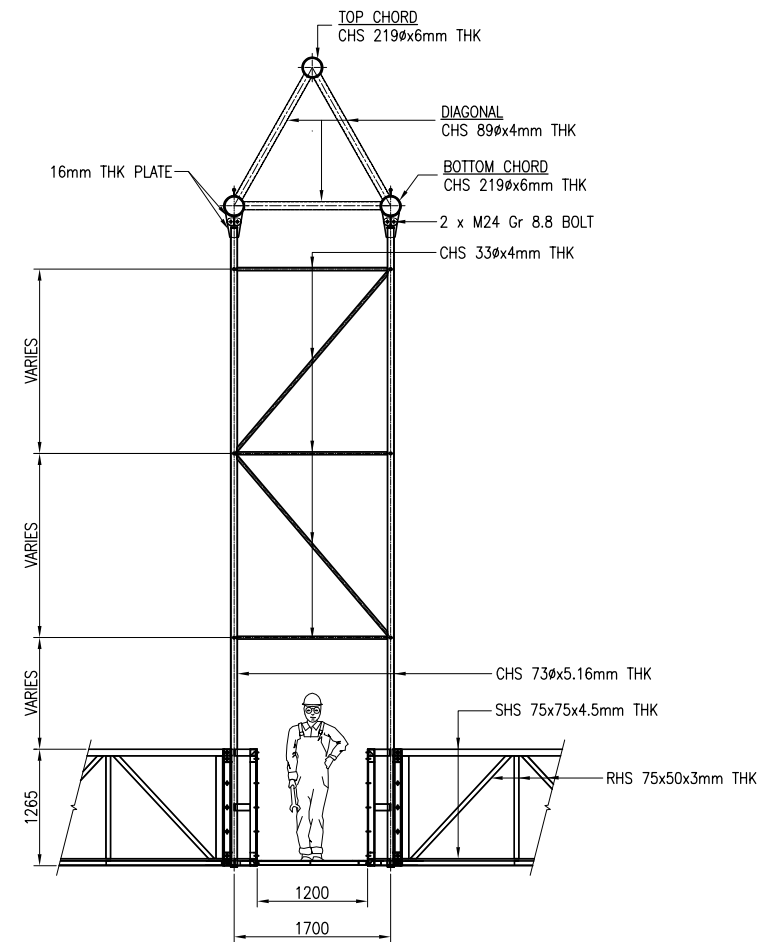
3D-VIEW OF CATWALK LAYOUT



SECTION E - E



SECTION E1 - E1



SECTION F - F

TYPICAL CATWALK DETAILS

REF	DATE	DESCRIPTION
03	31.07.2012	AS-BUILT
02	20.04.2012	GENERAL
01	12.01.2012	GENERAL

OWNER :



MAJLIS PERBANDARAN KUANTAN
Jalan Tanah Putih, 25100 Kuantan,
Pahang Darul Makmur, Malaysia.
TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.

117-A, 1st. FLOOR, MUIP BUILDING,
JALAN MAHKOTA, 25000 KUANTAN,
PAHANG DARUL MAKMUR
TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :



dzj & ASSOCIATES ARCHITECTS & ASSOCIATES ARCHITECTS SENDIRIAN BERHAD (708990-P)
B-26, Tingkat Satu, Jalan IM3/10
Bandar Indera Mahkota
25200 Kuantan, Pahang Darul Makmur.
Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:



TRI-ARCH sdn. bhd.
7-1, JALAN 2/115A, TAMAN PAGAR RUYONG
OFF. JALAN KUCHAI LAMA,
58200 KUALA LUMPUR.
TEL : 7961 2870 FAX : 7961 8210
E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
No. 11, Jalan Kuda Ular, Seksyen 08, Bukit Mering, 41550 Bukit Mertajam, Pulau Pinang.
Tel: 04-628 2321 Fax: 04-628 2322
E-mail: sdn@sedibena.com.my
Website: www.sedibena.com



TRANSERVE TRANSSERVE PTE LTD
39 PANDAN ROAD, JURONG, SINGAPORE 609281
Tel: (65) 6268 3099 Fax: (65) 6268 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:



JURUNDING HYH SDN. BHD.
A-7732, Tingkat Satu, Kedai LKNP,
Jalan Dato' Bahaman, 25200 Kuantan,
Pahang Darul Makmur.
Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



PENDITA
NO. C-9-9, Level 11, Menara Ungang Emas,
85 Jalan Loke Yew, 55200 Kuala Lumpur
Tel : 03-92008268 Fax : 03-92008276 (391855-V)
email: info@pendita.com.my website: pendita.com.my

PROJECT :

**CADANGAN MENAIK TARAF
KOLAM RENANG SERTA KERJA-KERJA
BERKAITAN DI WISMA BELIA,
INDERA MAHKOTA, KUANTAN, MALAYSIA.**

TITLE :

CATWALK LAYOUT & SECTION

DATE : 29.12.2011

DRAWN :

SCALE : 1 : 700 / 1 : 35

CHECKED :

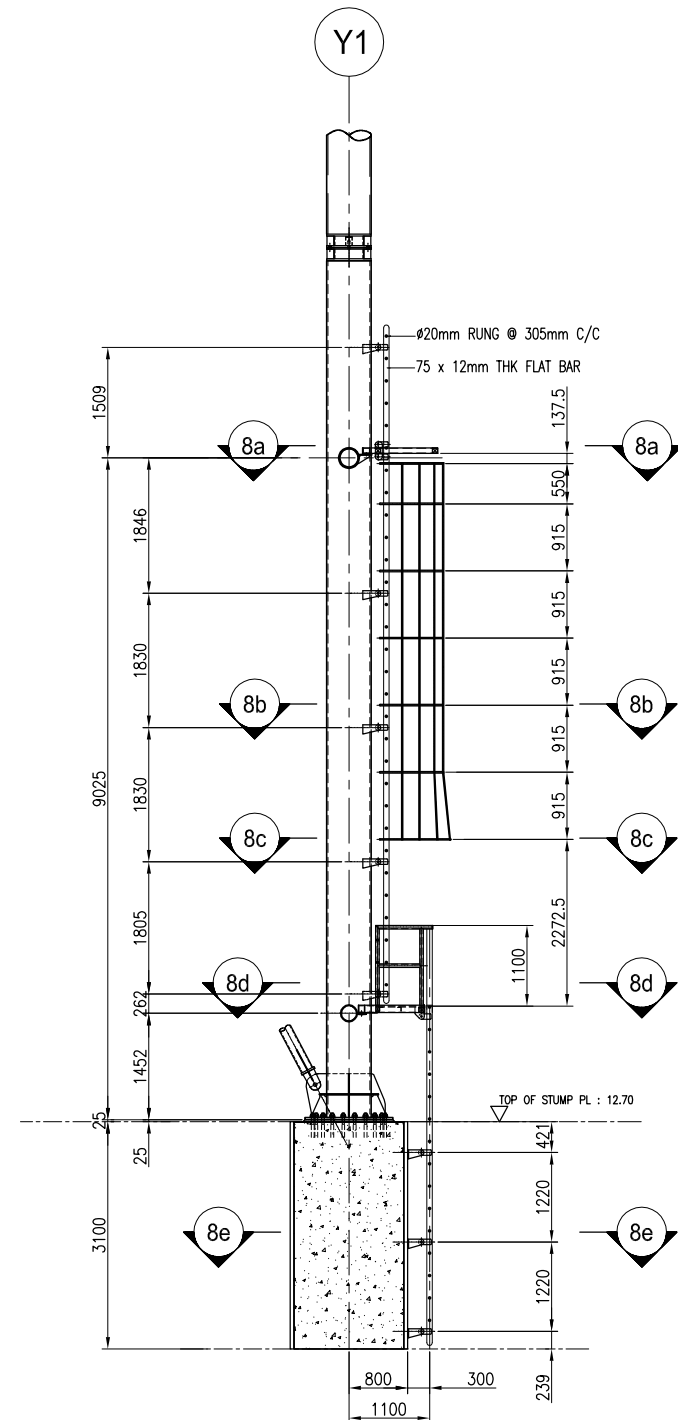
DRAWING NO. :

REVISION

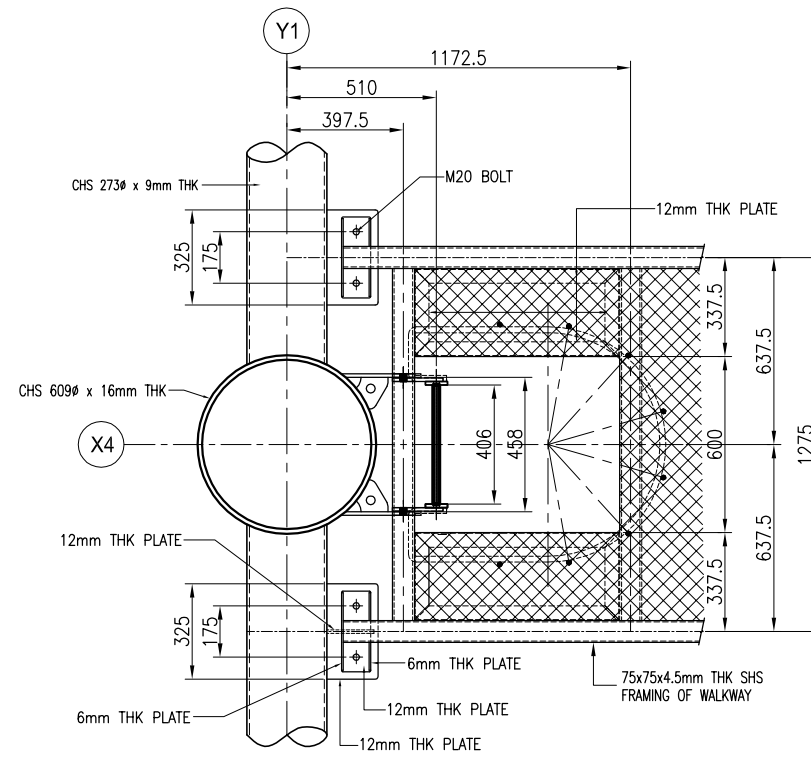
TA-Q326-13

03

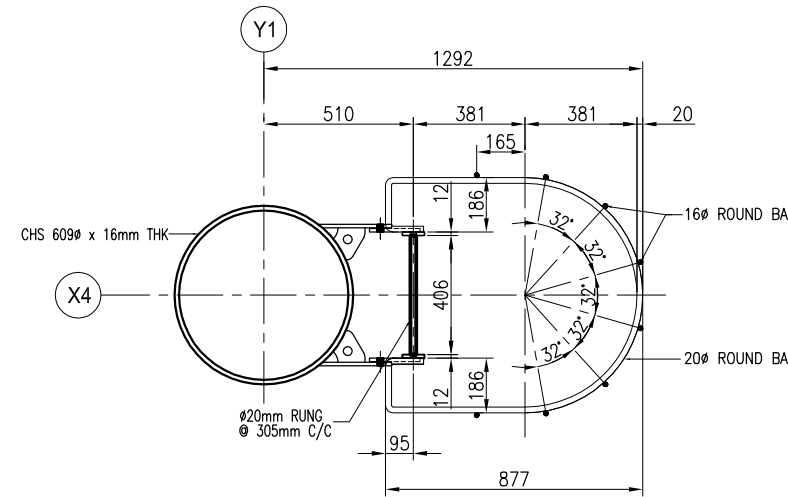




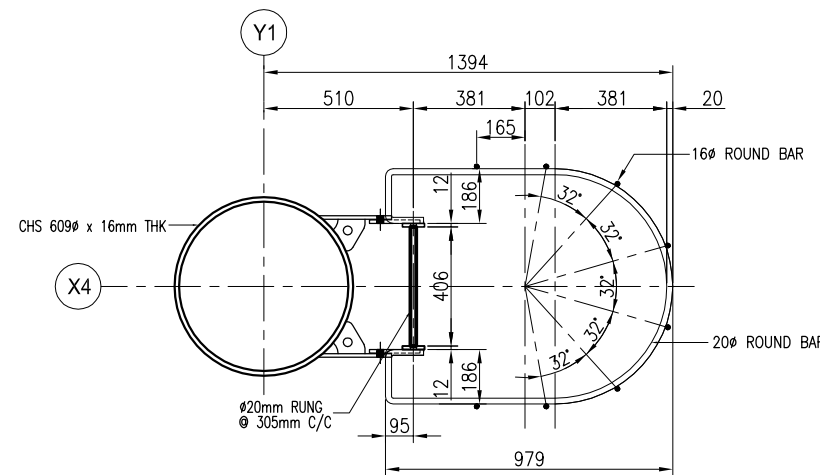
CATLADDER SETTING
ALONG GRIDLINE Y1/X4



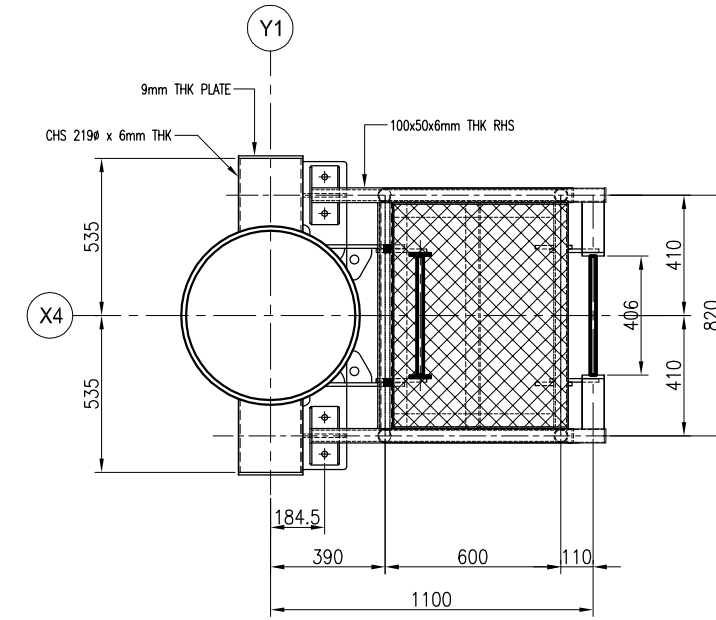
SECTION 8a - 8a



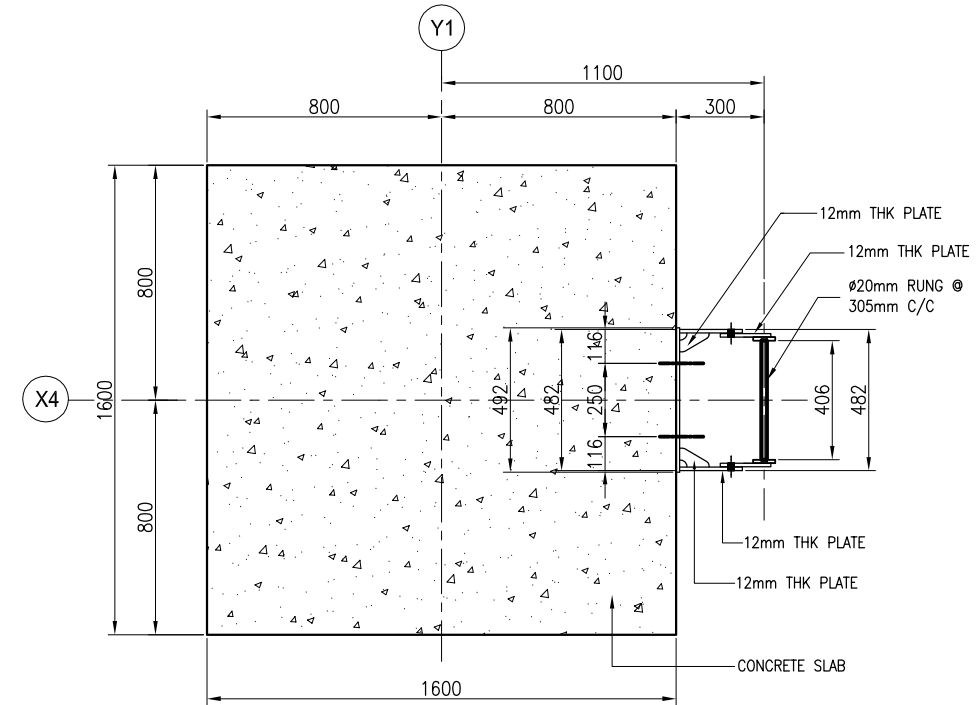
SECTION 8b - 8b



SECTION 8c - 8c



SECTION 8d - 8d



SECTION 8e - 8e

Kompleks Kolam Renang

NOTE : 68

REF	DATE	DESCRIPTION
00	31.07.12	AS-BUILT

OWNER :

MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :
SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN,
 PAHANG DARUL MAKMUR
 TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :

dzj & ASSOCIATES ARCHITECTS
BENDIRIAN BERHAD (708290-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:

TRI-ARCH sdn. bhd.
 7-1 JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 59200 KUALA LUMPUR.
 TEL : 7981 2870 FAX : 7981 8210
 E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:

SEDIABENA sdn. bhd.
 No. 11, Jalan Kerasi, 81000 Segamat, Johor Darul Makmur, 81700 Segamat, Johor Darul Makmur.
 Tel: 076-866 3369 Fax: 076-866 3324 Email: sales@sedibena.com.my
 Corp No: 382754 website: www.sedibena.com


TRANSERVE PTE LTD
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3069 Fax: (65) 6268 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:

JURUNING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :

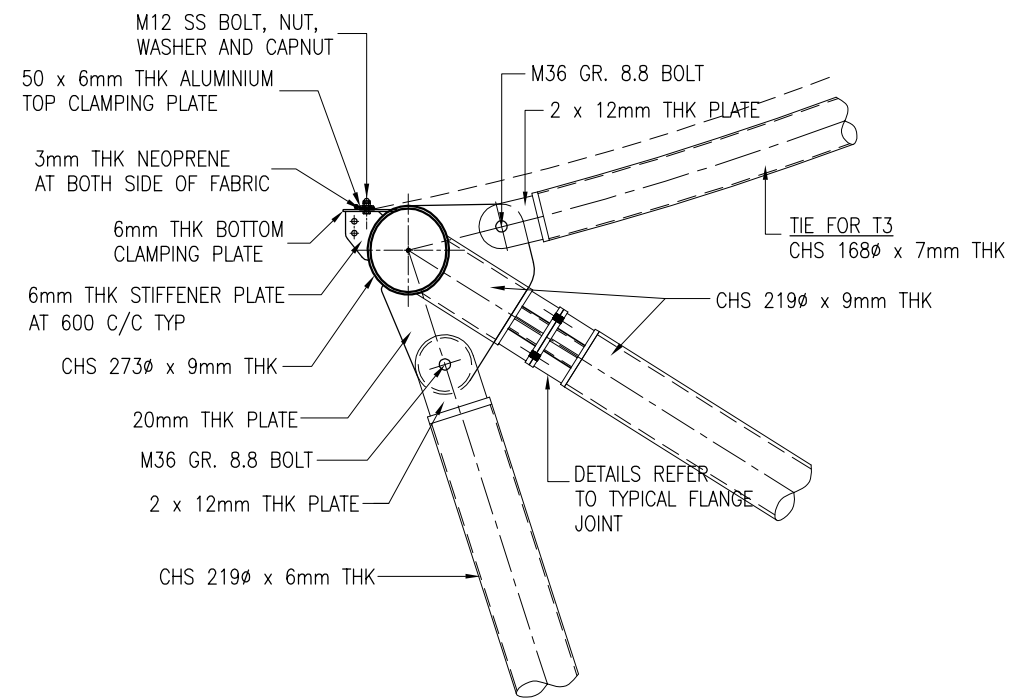
PENDITA
 NO. C-9-9, Level 11, Menara Ujang Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :
**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN, MALAYSIA.**

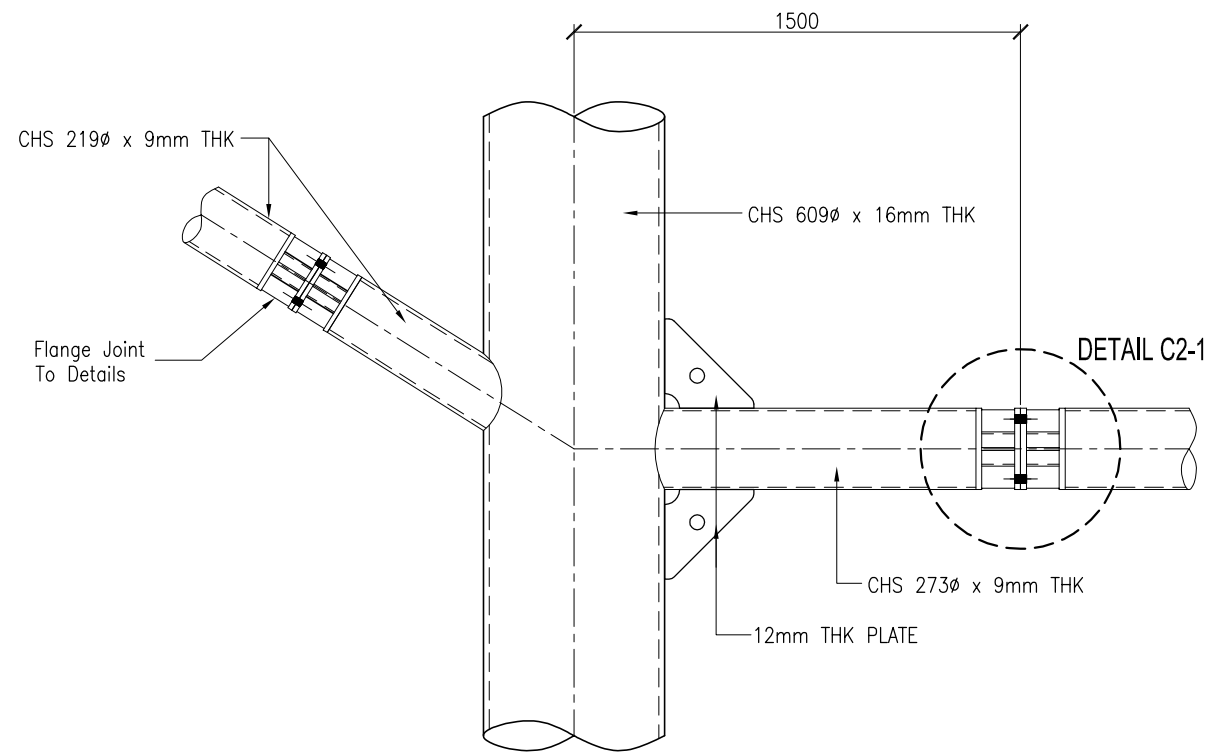
TITLE :
CATLADDER DETAILS

DATE : 31.07.2012	DRAWN :
SCALE : 1 : 100 / 1 : 25	CHECKED :
DRAWING NO. : TA-Q326-14	REVISION 00

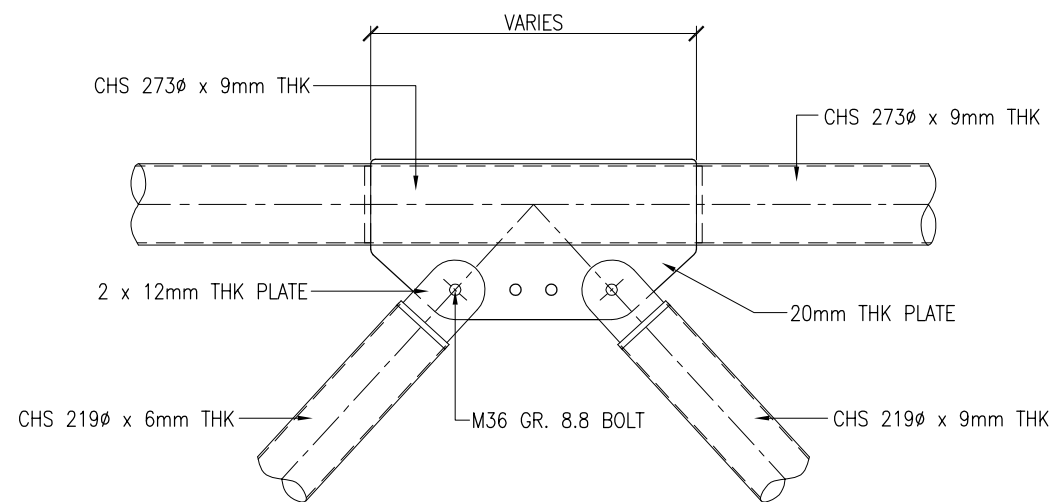




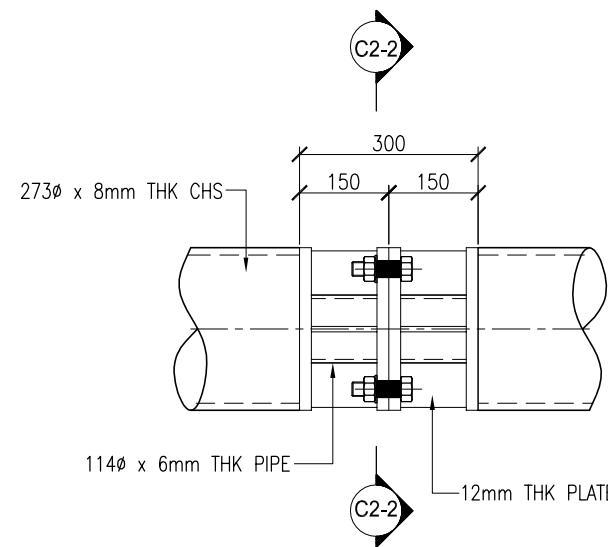
DETAIL C1



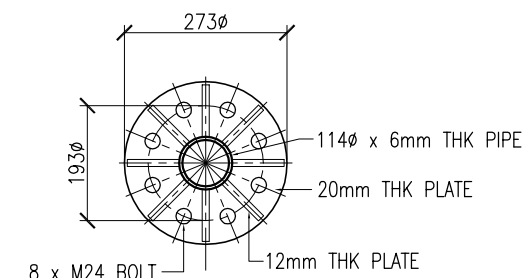
DETAIL C2



DETAIL C3



DETAIL C2-1



SECTION C2-2 - C2-2

Kompleks Kolam Renang

NOTE : 69

REF	DATE	DESCRIPTION
00	31.07.2012	AS-BUILT

OWNER :



MAJLIS PERBANDARAN KUANTAN
Jalan Tanah Putih, 25100 Kuantan,
Pahang Darul Makmur, Malaysia.
TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.

117-A, 1st. FLOOR, MUIP BUILDING,
JALAN MAHKOTA, 25000 KUANTAN ,
PAHANG DARUL MAKMUR
TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :



**dzj & ASSOCIATES ARCHITECTS
SENDIRIAN BERHAD (702200-P)**
B-26, Tingkat Satu, Jalan IM3/10
Bandar Indera Mahkota
25200 Kuantan, Pahang Darul Makmur.
Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:



TRI-ARCH sdn. bhd.
7-1 JALAN 2/115A, TAMAN PAGAR RUYONG
OFF. JALAN KUCHAI LAMA,
59200 KUALA LUMPUR.
TEL : 7961 2870 FAX : 7961 8210
E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
No. 11, Jalan Jaya 1/81, Senang Ulu Bukit, 47500 Sepang, Selangor Darul Ehsan, Malaysia.
Tel: 03-8921 2211 Fax: 03-8921 2222
Corporate: 03-8921 2211
Website: www.sediabena.com

TRANSERVE TRANSERVE PTE LTD

39 PANDAN ROAD, JURONG, SINGAPORE 609281
Tel: (65) 6268 3099 Fax: (65) 6268 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:

JURUNING HYH SDN. BHD.

A-7732, Tingkat Satu, Kedai LKNP,
Jalan Dato' Bahaman, 25200 Kuantan,
Pahang Darul Makmur.
Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



NO. C-9-9, Level 11, Menara Ujung Emas,
85 Jalan Lake Yew, 55200 Kuala Lumpur.
Tel : 03-92008268 Fax : 03-92008276 (391855-V)
email: info@pendita.com.my website: pendita.com.my

PROJECT :

**CADANGAN MENAIK TARAF
KOLAM RENANG SERTA KERJA-KERJA
BERKAITAN DI WISMA BELIA,
INDERA MAHKOTA, KUANTAN. MALAYSIA.**

TITLE :

DETAILS

DATE : 31.07.2012

DRAWN :

SCALE : 1 : 25

CHECKED :

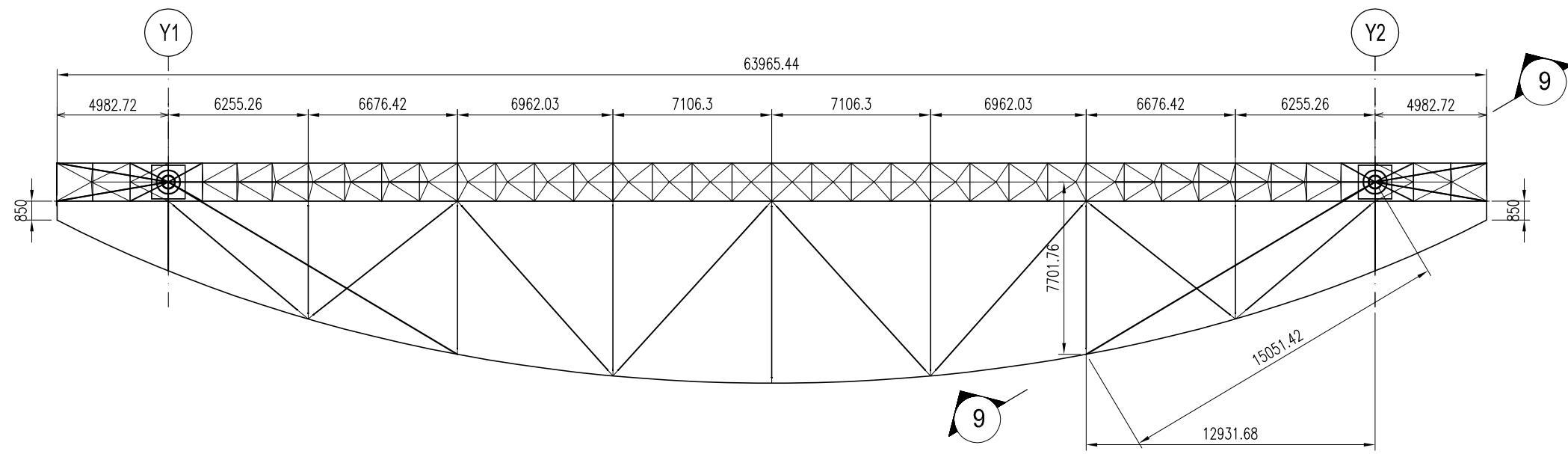
DRAWING NO. :

REVISION

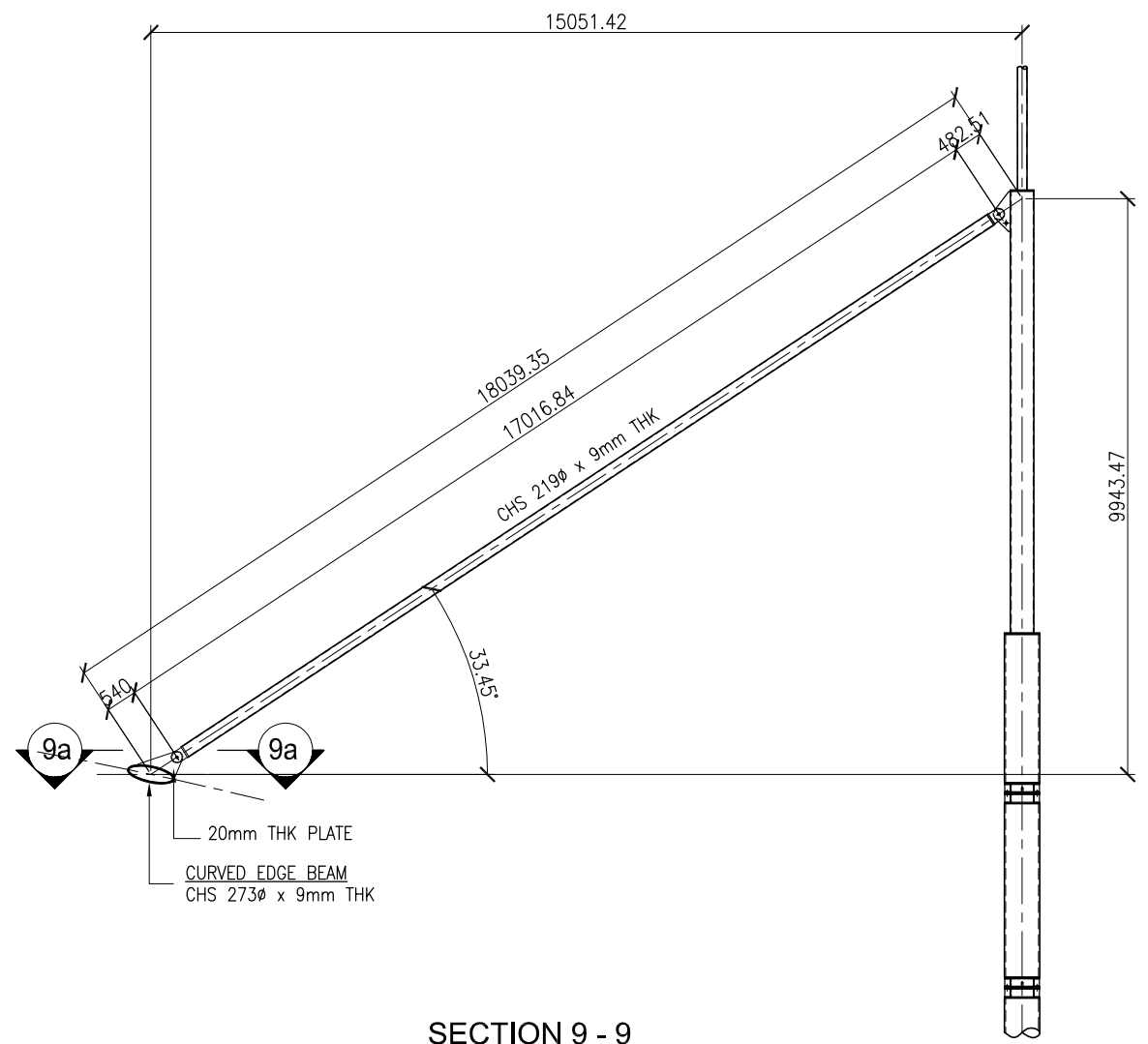
TA-Q326-15

00

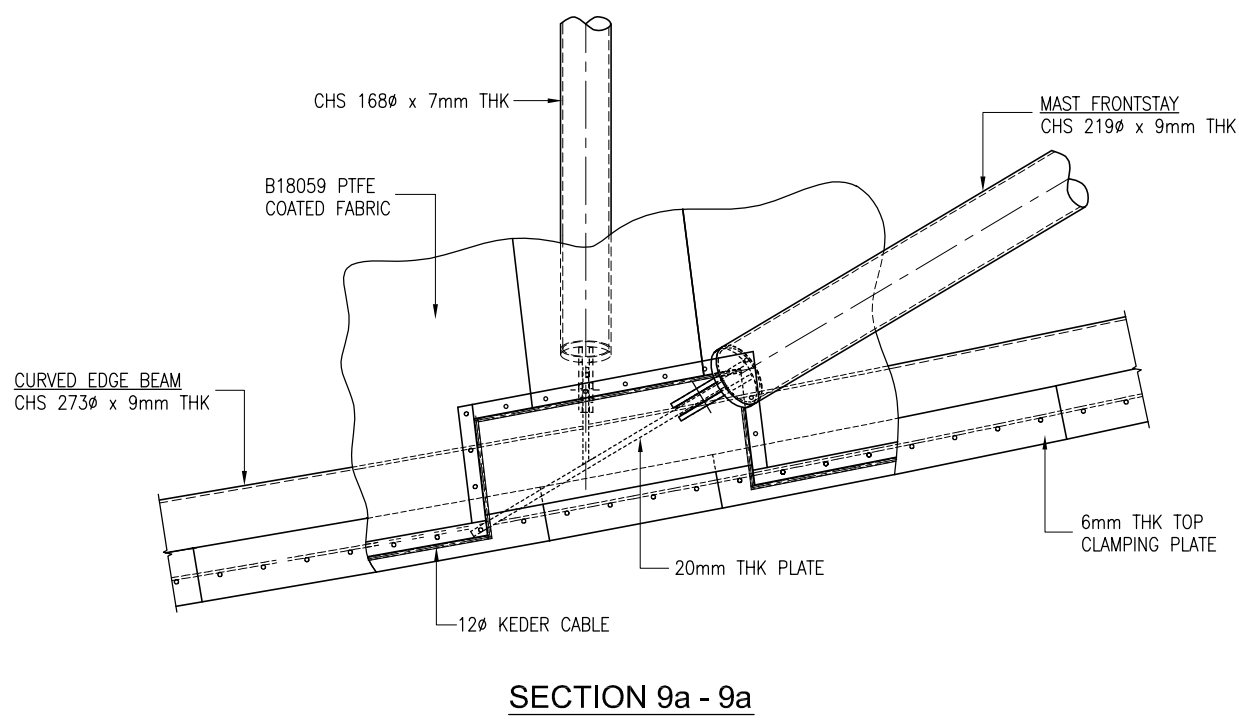




EDGE CANOPY FRAME SETTING - PLAN VIEW



SECTION 9 - 9



SECTION 9a - 9a

Kompleks Kolam Renang

NOTE : 70

REF	DATE	DESCRIPTION
00	31.07.2012	AS-BUILT

OWNER :



MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN ,
 PAHANG DARUL MAKMUR
 TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :



& ASSOCIATES ARCHITECTS
SENDIRIAN BERAHAD (709890-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan Pahang Darul Makmur.
 Tel 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:



TRI-ARCH sdn. bhd.
 7-JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 59200 KUALA LUMPUR,
 TEL : 7981 2870 FAX : 7981 8210
 E-mail : tjarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
 No. 11, Jalan Kerasi, Seberang Perak Tengah, 06000 Alor Setar, Kedah.
 Tel: 04-3601221 Fax: 04-3601222
 E-mail: info@sediabena.com
 Website: www.sediabena.com

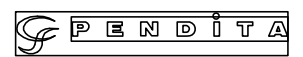
TRANSERVE TRANSERVE PTE LTD
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3069 Fax: (65) 6268 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:



JURUNDING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



NO.C-9-9, Level 11, Menara Ujang Emas,
 85 Jalan Lake Yew, 55200 Kuala Lumpur.
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :

**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN. MALAYSIA.**

TITLE :

**EDGE CANOPY FRAME SETTING
 & DETAILS**

DATE : 31.07.2012	DRAWN :
SCALE : 1 : 250	CHECKED :
DRAWING NO. : TA-Q326-16	REVISION 00



REF	DATE	DESCRIPTION
00	12.01.2012	AS-BUILT

OWNER :

MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644



MAIN CONTRACTOR :
SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN,
 PAHANG DARUL MAKMUR
 TEL : 609-515 2473, FAX : 603-516 2619

ARCHITECT'S :

dzj & ASSOCIATES ARCHITECTS
BENDIRIAN BERHAD (70890-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:

TRI-ARCH sdn. bhd.
 7-JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 55200 KUALA LUMPUR.
 TEL : 7961 2870 FAX : 7961 8210
 E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:

SEDIABENA sdn. bhd.
 No. 11, Jalan Uluu, Sektor 08, Bukit Mering, 41550 Bukit Mertajam, Pulau Pinang.
 Tel: 04-581 2211 Fax: 04-581 2222
 (Corp No: 952754) web: www.sediabena.com
 &

TRANSERVE PTE LTD
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6288 3069 Fax: (65) 6286 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:

JURUNING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

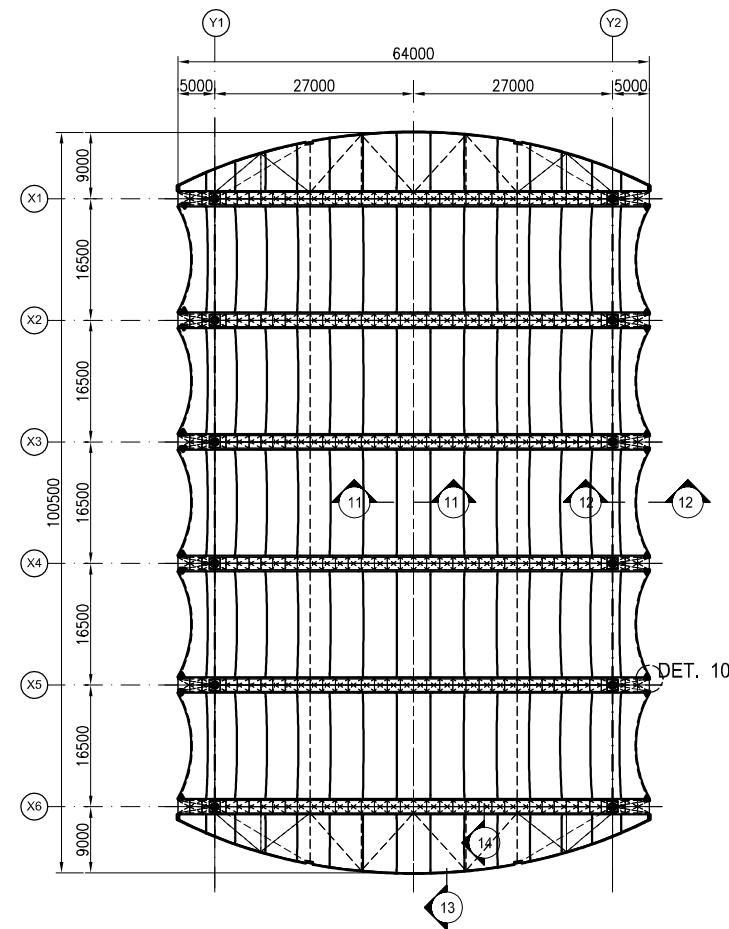
QUANTITY SURVEYOR :

PENDITA
 NO. C-9-9, Level 11, Menara Ujung Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

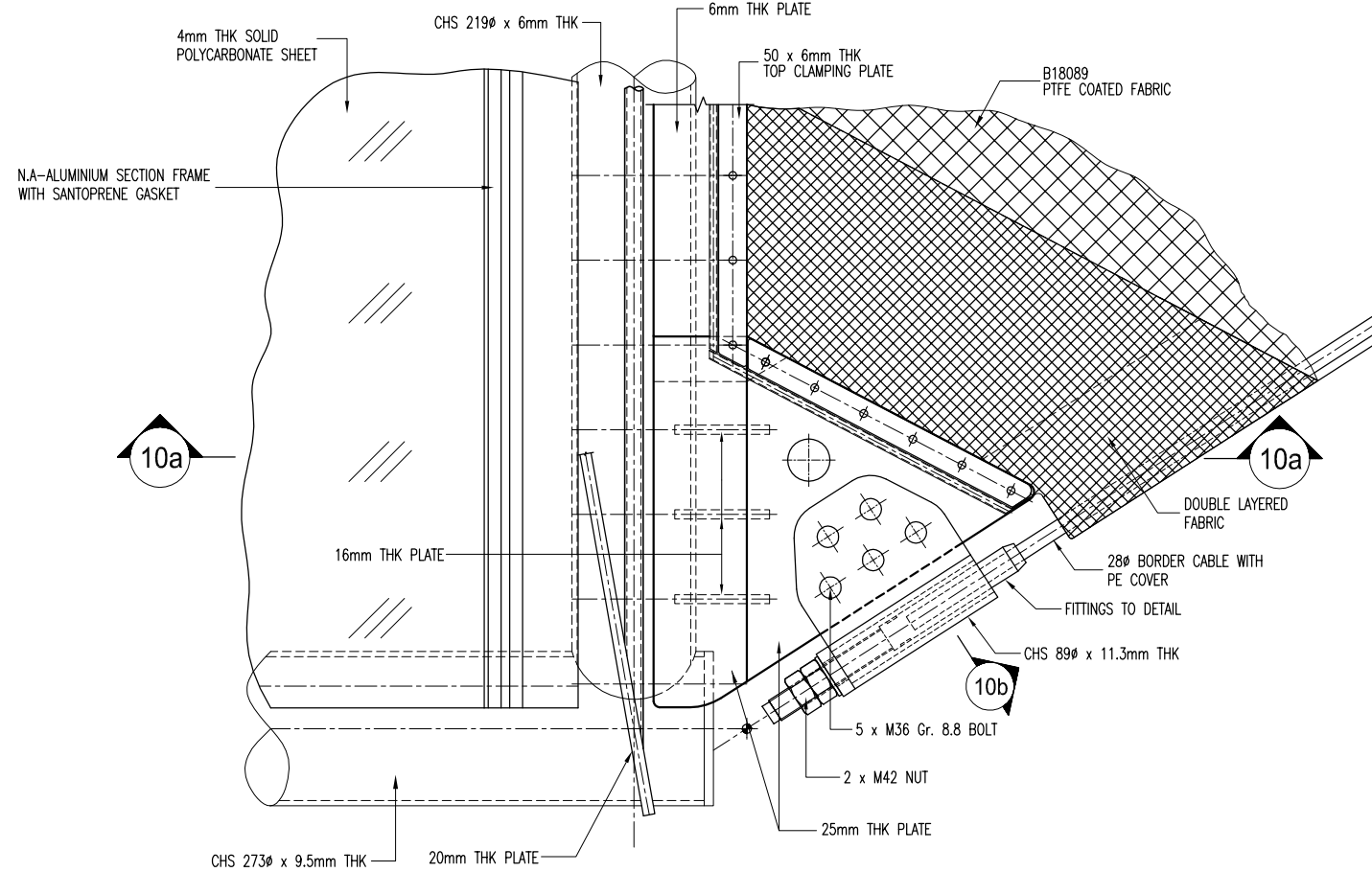
PROJECT :
**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN, MALAYSIA.**

TITLE :
CUTTING PATTERN LAYOUT & DETAILS

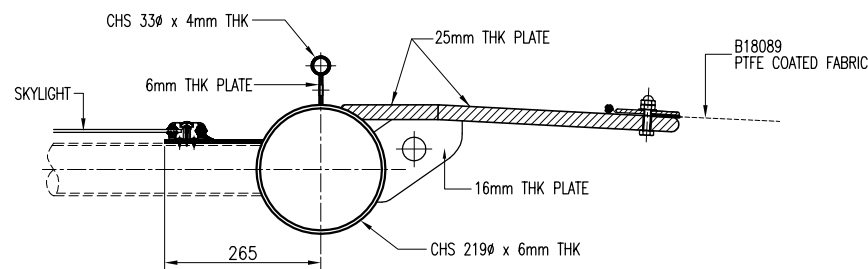
DATE : 31.07.2012	DRAWN :
SCALE : 1 : 500	CHECKED :
DRAWING NO. : TA-Q326-17	REVISION 00



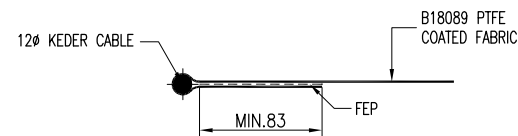
CUTTING PATTERN LAYOUT PLAN



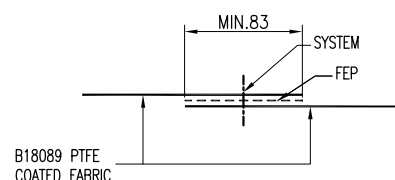
DETAIL 10
(20 LOCATIONS)



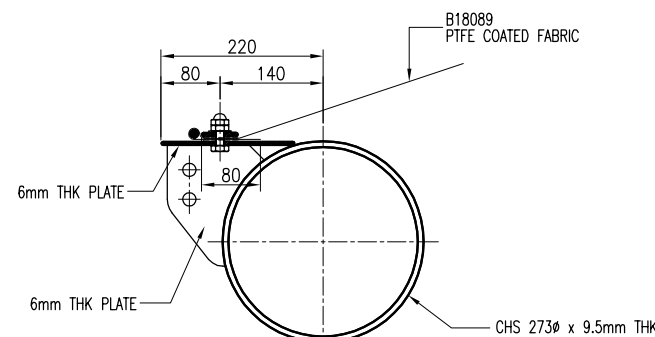
SECTION 10a - 10a



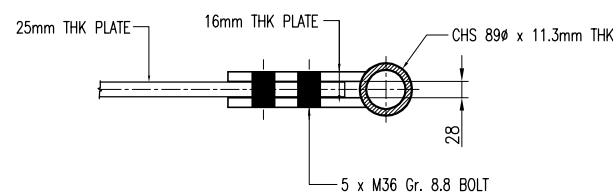
TYPICAL FABRIC FIXED EDGE DETAIL



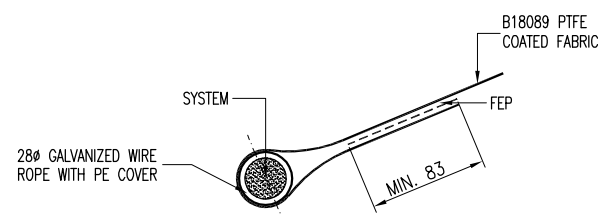
SECTION 11 - 11
(TYPICAL INTERNAL SEAM JOINT)



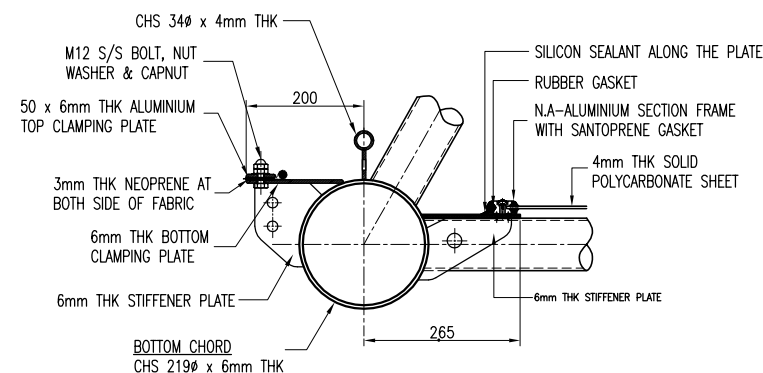
SECTION 13 - 13
(TYPICAL EXTERNAL FIXED EDGE DETAIL)



SECTION 10b - 10b

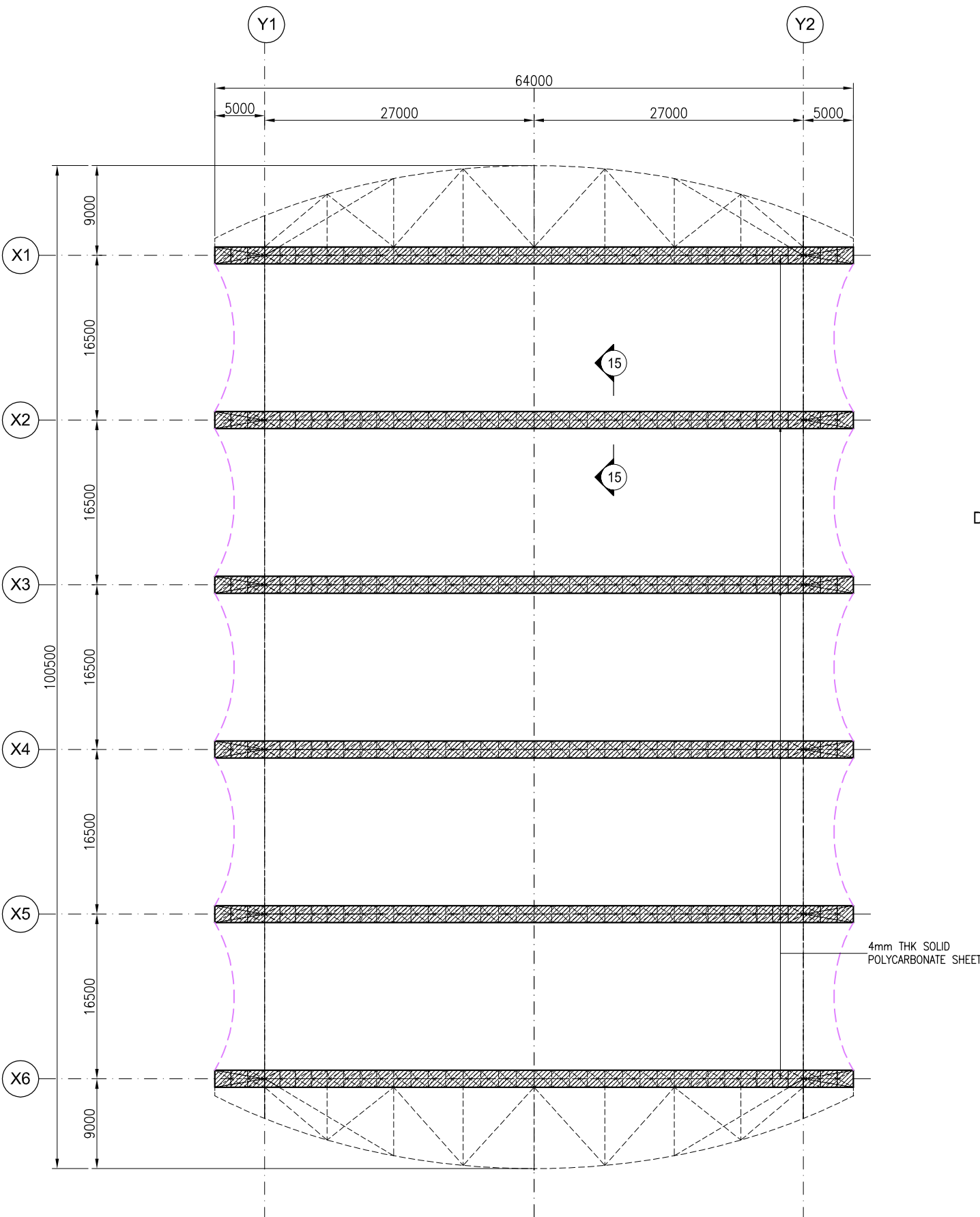


SECTION 12 - 12
(TYPICAL POCKET DETAIL)

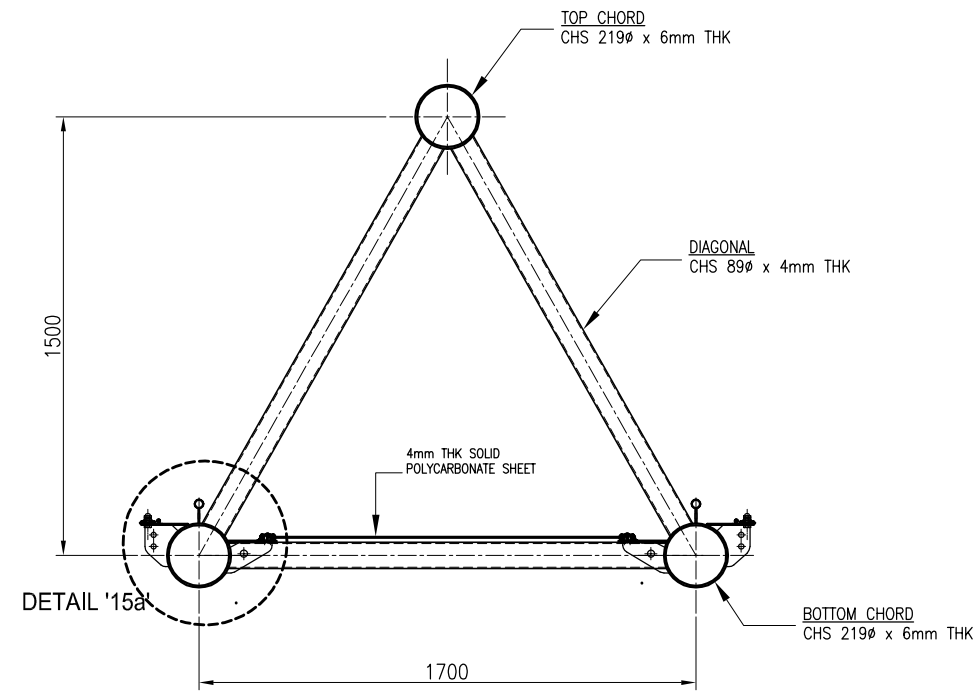


SECTION 14 - 14
(TYPICAL INTERNAL FIXED EDGE DETAIL)

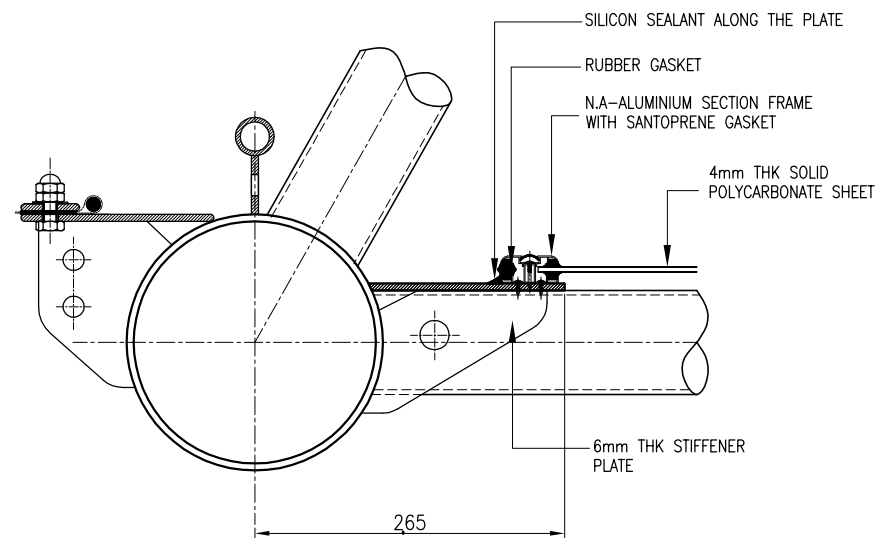




SKYLIGHT LAYOUT PLAN



SECTION 15 - 15



DETAIL '15a'

Kompleks Kolam Renang

NOTE : 72

REF	DATE	DESCRIPTION
00	31.07.2012	AS-BUILT

OWNER :



MAJLIS PERBANDARAN KUANTAN
 Jalan Tanah Putih, 25100 Kuantan,
 Pahang Darul Makmur, Malaysia.
 TEL : 09-5121555/666 FAXS : 5130644

MAIN CONTRACTOR :

SUARA HATI SDN. BHD.
 117-A, 1st. FLOOR, MUIP BUILDING,
 JALAN MAHKOTA, 25000 KUANTAN ,
 PAHANG DARUL MAKMUR
 TEL :609-515 2473, FAX : 603-516 2619

ARCHITECT'S :




& ASSOCIATES ARCHITECTS
BENDIRIAN BERHAD (70880-P)
 B-26, Tingkat Satu, Jalan IM3/10
 Bandar Indera Mahkota
 25200 Kuantan, Pahang Darul Makmur.
 Tel: 09-5736430 / 5736372 Fax: 09-5736443

SPECIALIST ROOF & CLADDING CONTRACTOR:




TRI-ARCH sdn. bhd.
 7-JALAN 2/115A, TAMAN PAGAR RUYONG
 OFF. JALAN KUCHAI LAMA,
 59200 KUALA LUMPUR,
 TEL : 7961 2870 FAX : 7961 8210
 E-mail : triarch90@yahoo.com.my

IN CONJUNCTION WITH:



SEDIABENA sdn. bhd.
 No. 11, Jalan USR, Segar Hill Damak, 41550 Seremban, Negeri Sembilan.
 Tel: 06-7961 2870 Fax: 06-7961 2221
 E-mail: info@sedibena.com
 Website: www.sedibena.com

&



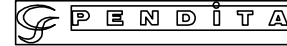
TRANSERVE PTE LTD
 39 PANDAN ROAD, JURONG, SINGAPORE 609281
 Tel: (65) 6268 3099 Fax: (65) 6266 2324 Email: sales@transerve.com.sg

ENGINEER'S C&S and M&E:



JURUNDING HYH SDN. BHD.
 A-7732, Tingkat Satu, Kedai LKNP,
 Jalan Dato' Bahaman, 25200 Kuantan,
 Pahang Darul Makmur.
 Tel : 09-566 3031 Faks : 09-560 1182

QUANTITY SURVEYOR :



PENDITA
 NO. C-9-9, Level 11, Menara Ujang Emas,
 85 Jalan Loke Yew, 55200 Kuala Lumpur.
 Tel : 03-92008268 Fax : 03-92008276 (391855-V)
 email: info@pendita.com.my website: pendita.com.my

PROJECT :

**CADANGAN MENAIK TARAF
 KOLAM RENANG SERTA KERJA-KERJA
 BERKAITAN DI WISMA BELIA,
 INDERA MAHKOTA, KUANTAN. MALAYSIA.**

TITLE :

SKYLIGHT LAYOUT & DETAILS

DATE : 31.07.2012	DRAWN :
SCALE : 1 : 500	CHECKED :
DRAWING NO. : TA-Q326-18	REVISION 00



11.3 ERECTION SEQUENCE



ERECTIONSEQUENCE

LAYOUT PLAN 3D VIEW

HOLDING DOWN BOLT - 3D VIEW HOLDING DOWN BOLT - TOP VIEW

1) HOLDING DOWN BOLT PRECAST IN 12 Nos. OF RC STUMP

COLUMN BASE DETAIL

2) ERECT 4 Nos. OF LOWER COLUMN

FLANGE JOINT

ELEVATION BRACING CONNECTION

3) ERECT TIE & BRACING BETWEEN LOWER COLUMN

PART 1/4 PART 4/4

3D VIEW

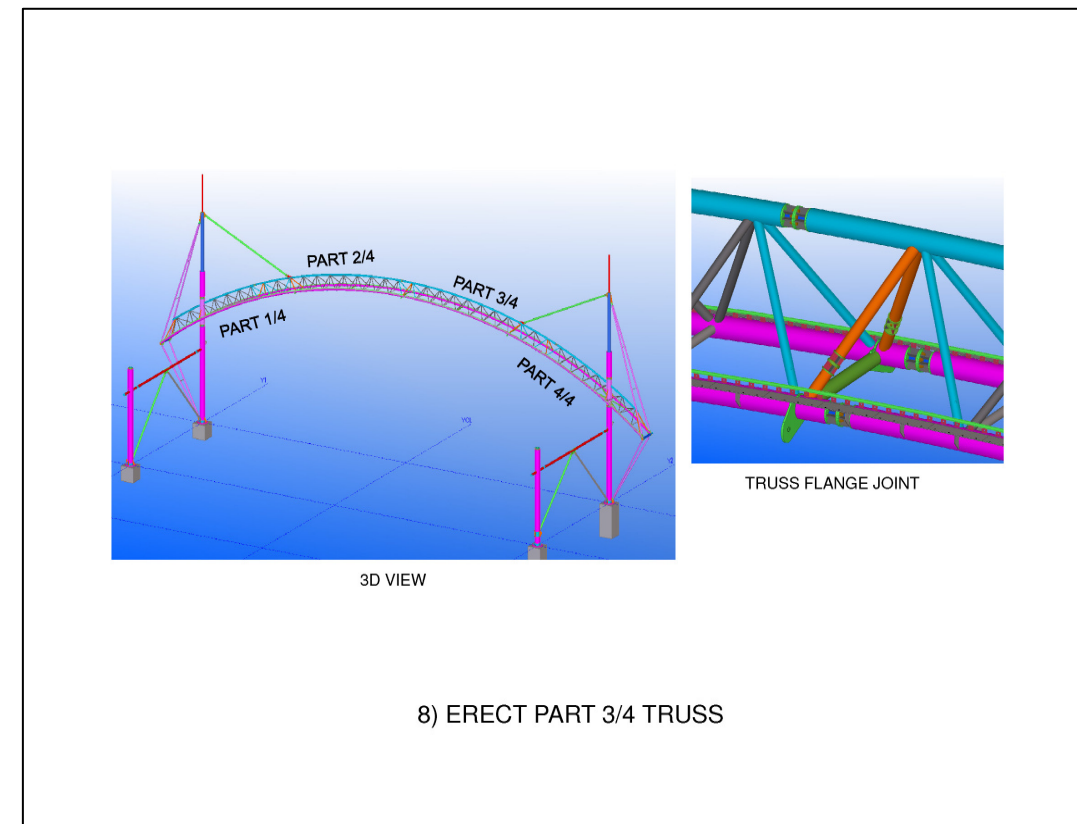
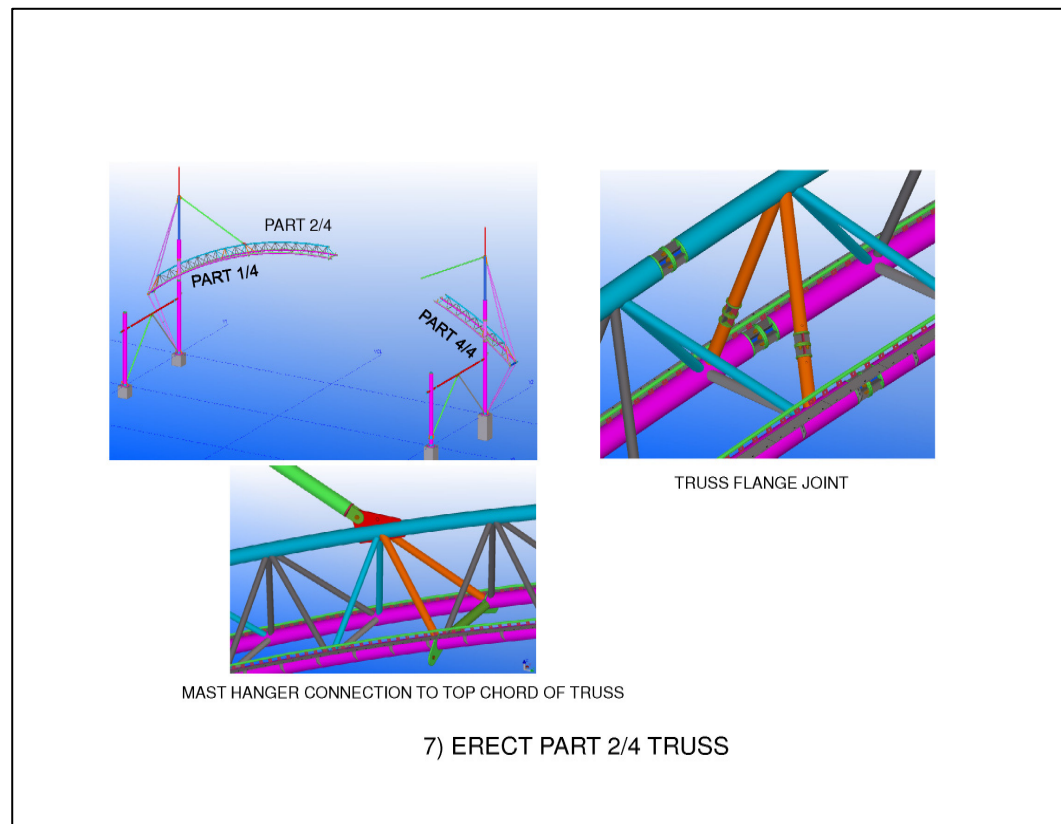
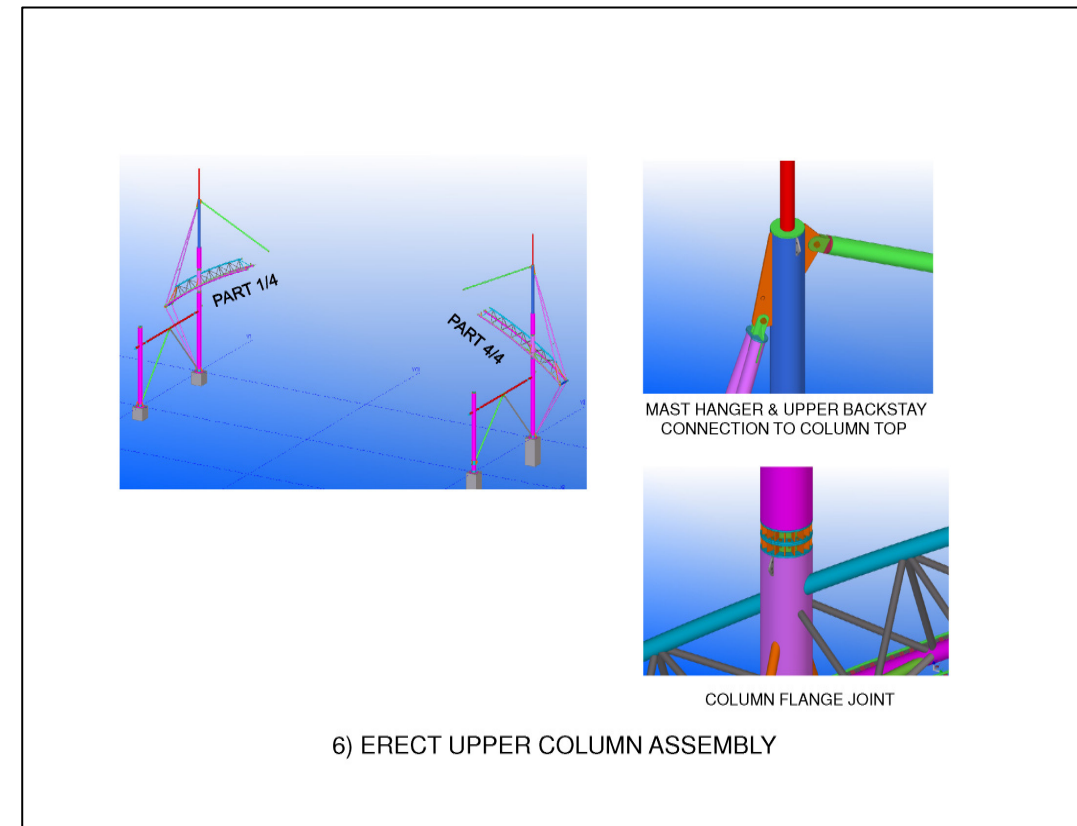
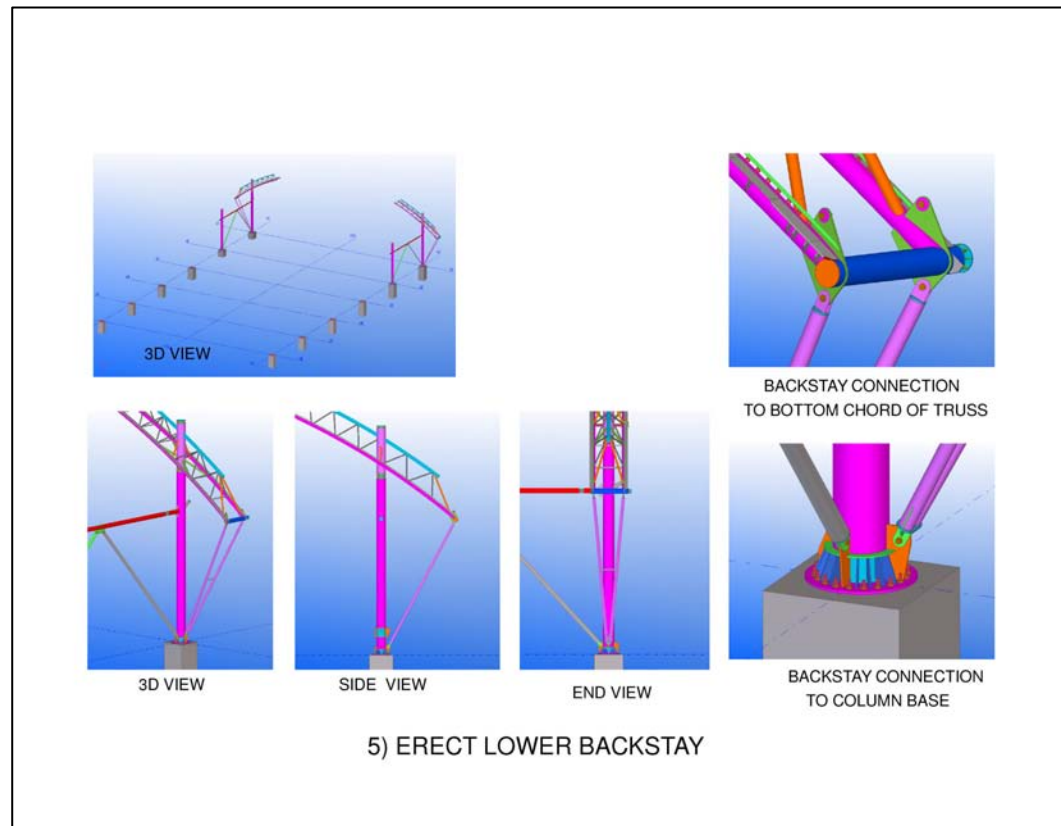
PLAN OF PART 1/4 PLAN OF PART 4/4

COLUMN FLANGE JOINT

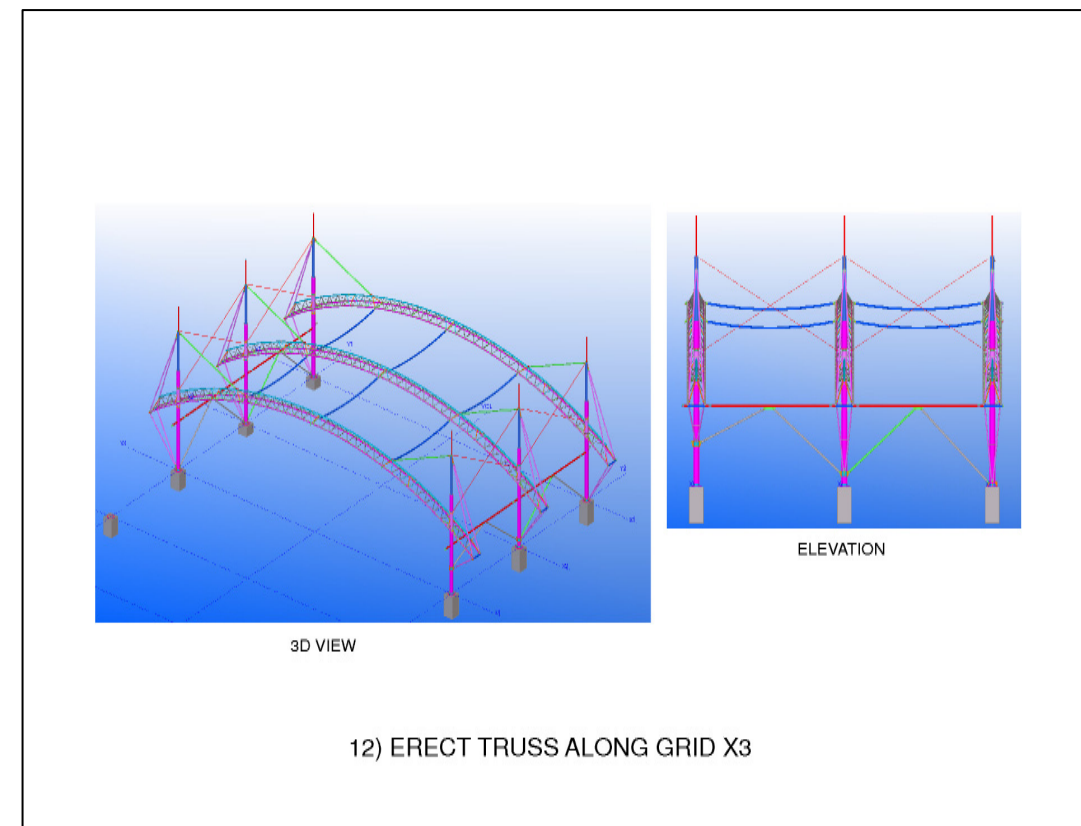
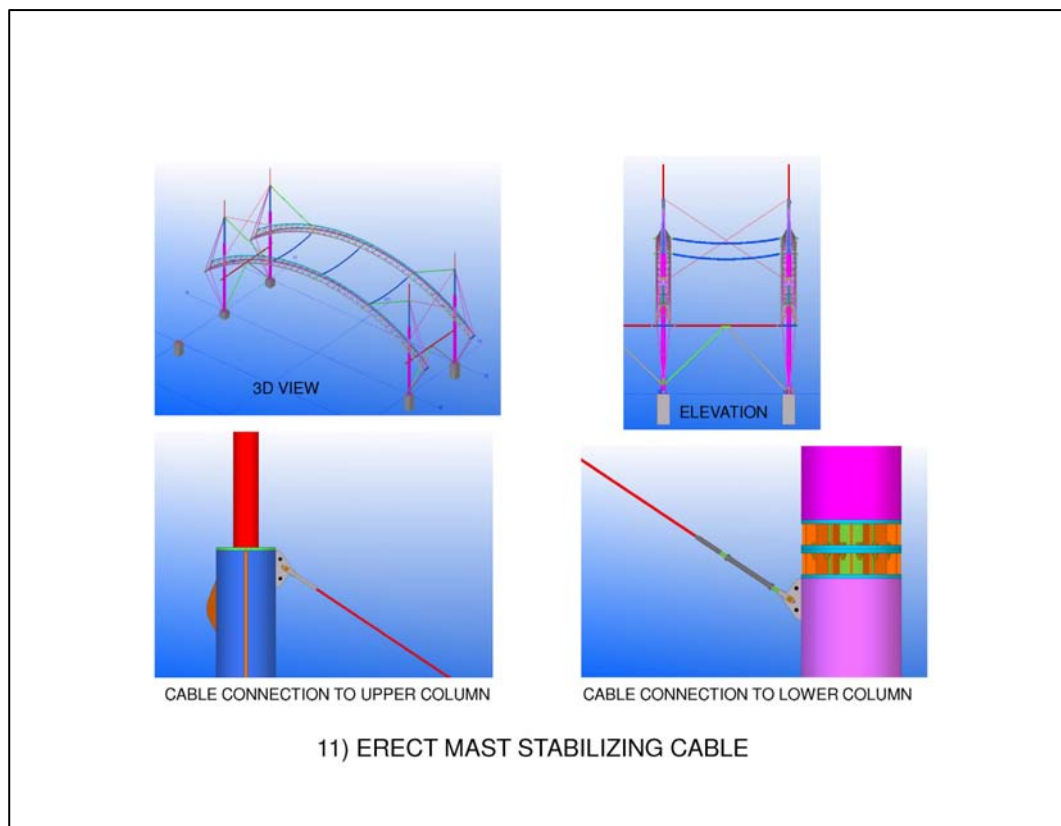
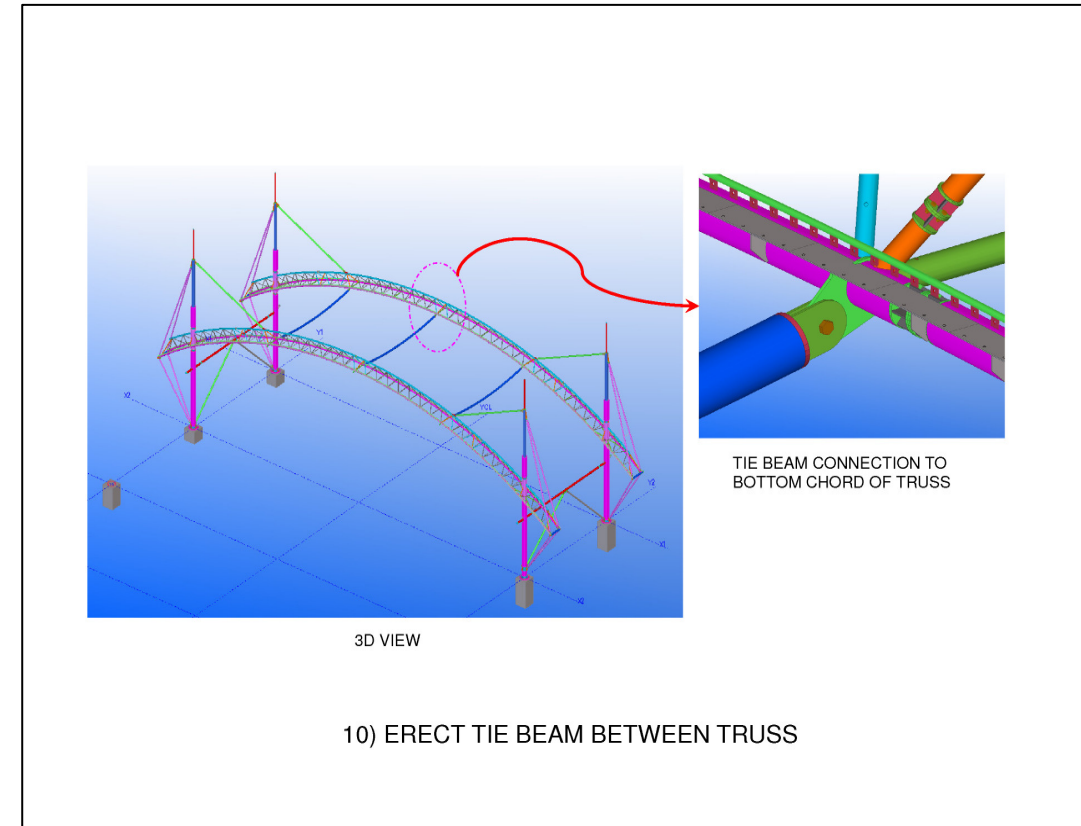
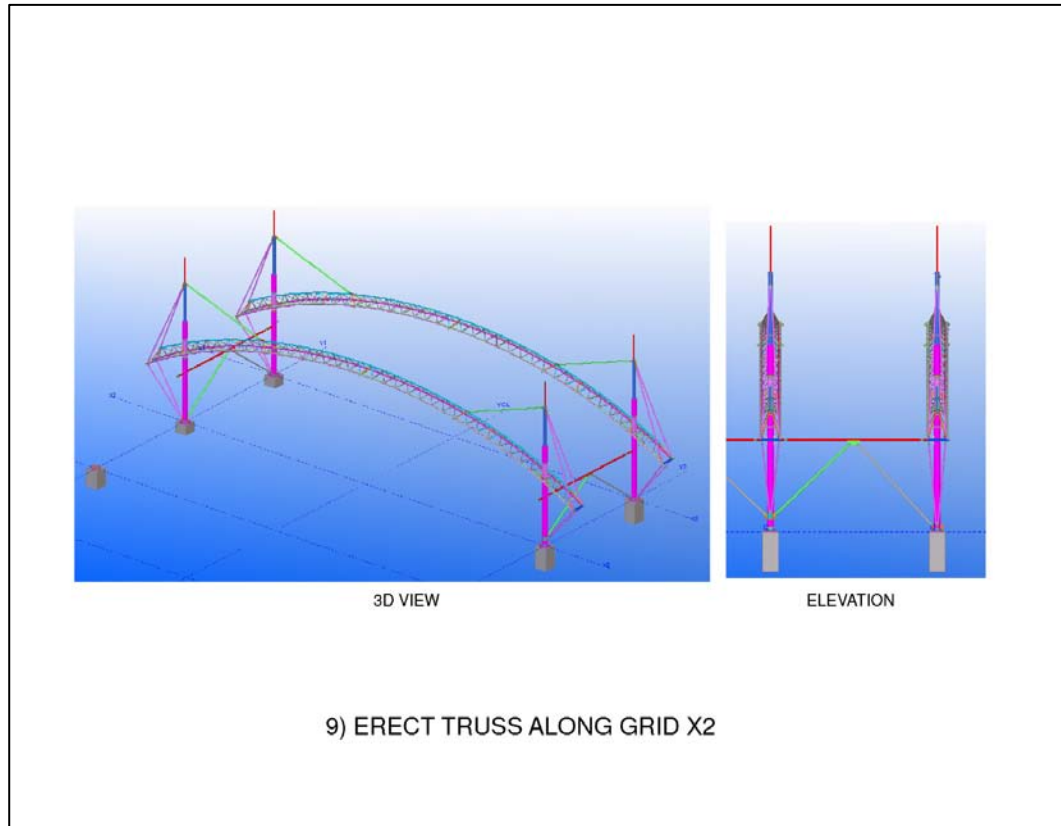
4) ERECT PART 1/4 & PART 4/4 TRUSS ALONG GRID X1



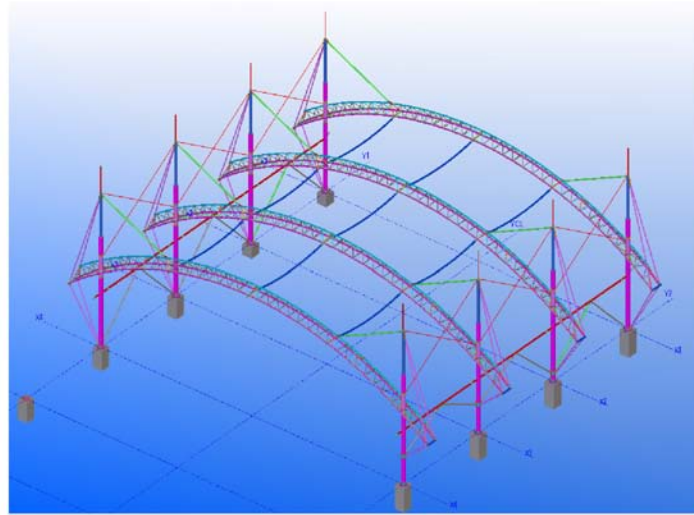
ERECTIONSEQUENCE



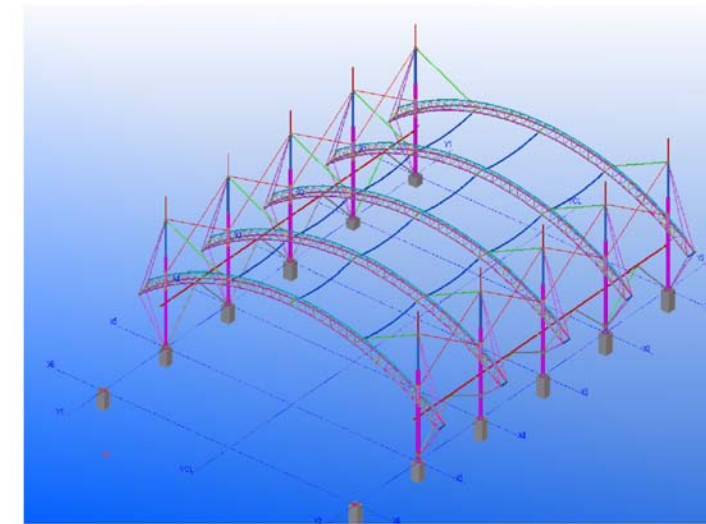
ERECTIONSEQUENCE



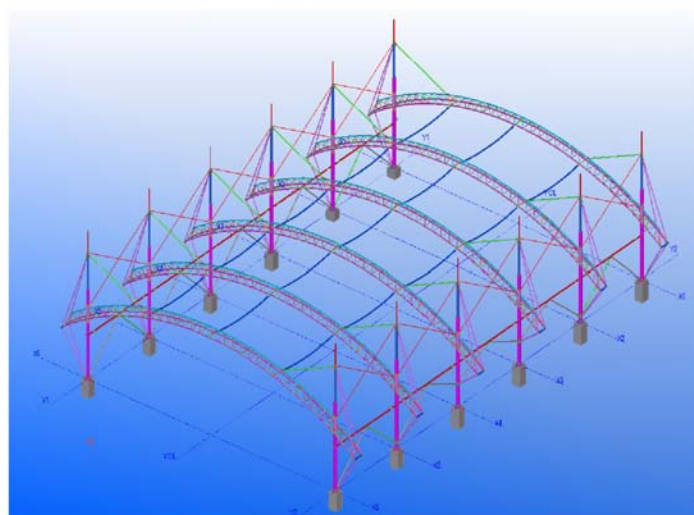
ERECTIONSEQUENCE



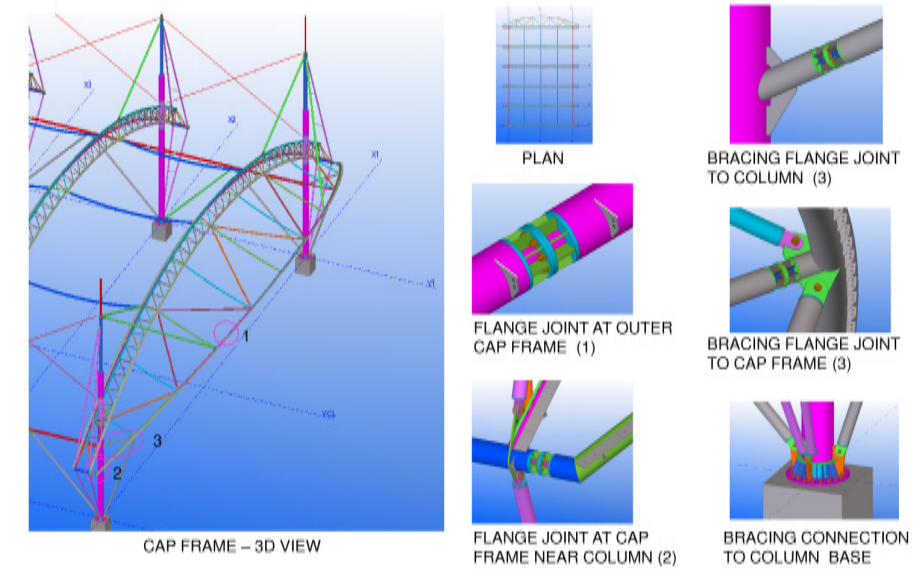
13) ERECT TRUSS ALONG GRID X4



14) ERECT TRUSS ALONG GRID X5



15) ERECT TRUSS ALONG GRID X6



16) ERECT THE ASSEMBLY OF CAP FRAME ALONG GRID X1

ERECTIONSEQUENCE

CAP FRAME – 3D VIEW

PLAN

BRACING CONNECTION TO OUTER CAP FRAME (3)

BRACING CONNECTION TO BOTTOM CHORD OF TRUSS (1)

HANGER & BRACING TO OUTER CAP FRAME (4)

BRACING CONNECTION TO OUTER CAP FRAME (2)

HANGER & BRACING TO OUTER CAP FRAME LOOKING FROM BELOW (4)

17) ERECT THE ASSEMBLY OF CAP FRAME ALONG GRID X6

CATLADDER & CATWALK - 3D VIEW

3D VIEW

CATLADDER

ELEVATION

PLAN

18) ERECT CATLADDER & CATWALK TO TRUSSES

3D VIEW

PLAN

ELEVATION

FABRIC CORNER PLATE AND FIXED EDGE DETAIL

19) ERECT 1ST INTERNAL FABRIC PANEL BETWEEN X1 TO X2

3D VIEW

PLAN

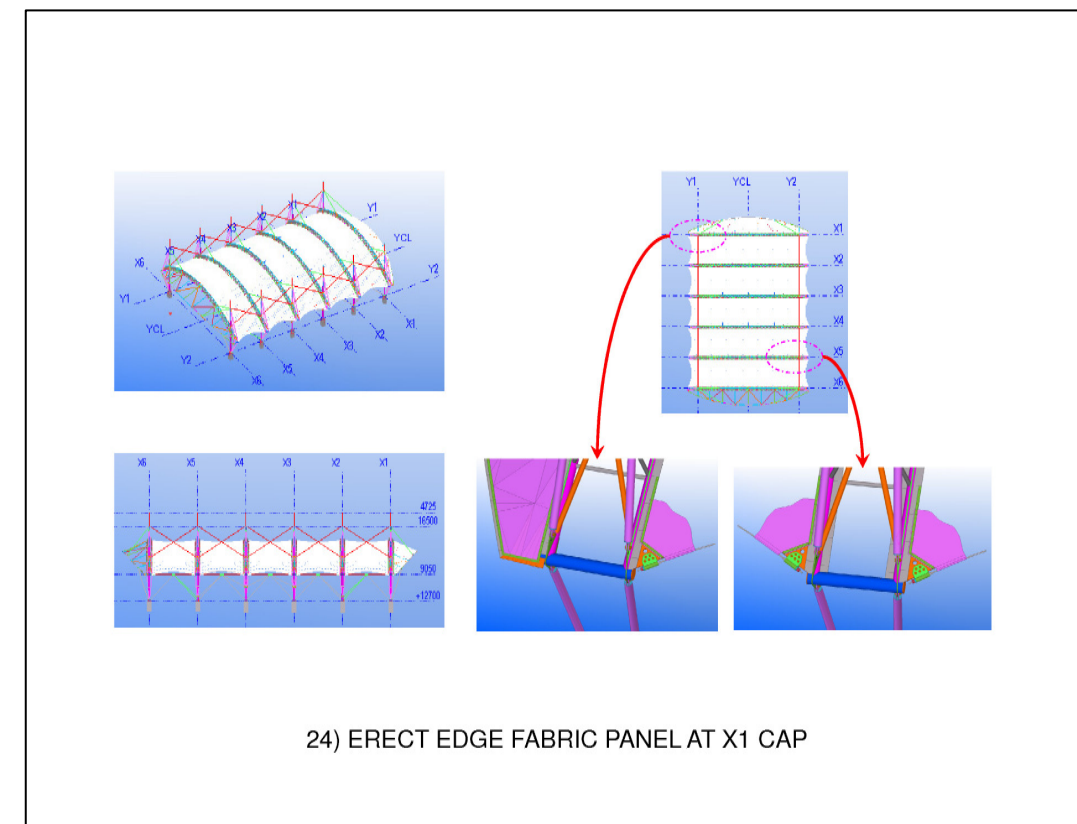
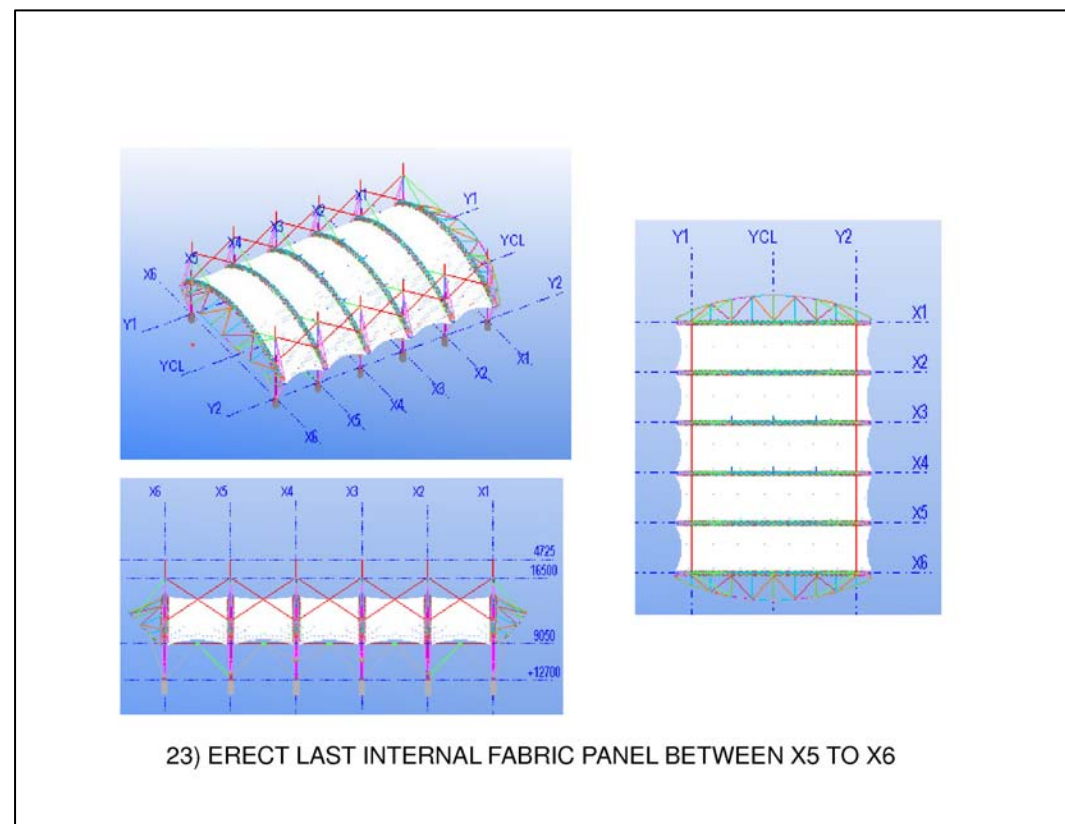
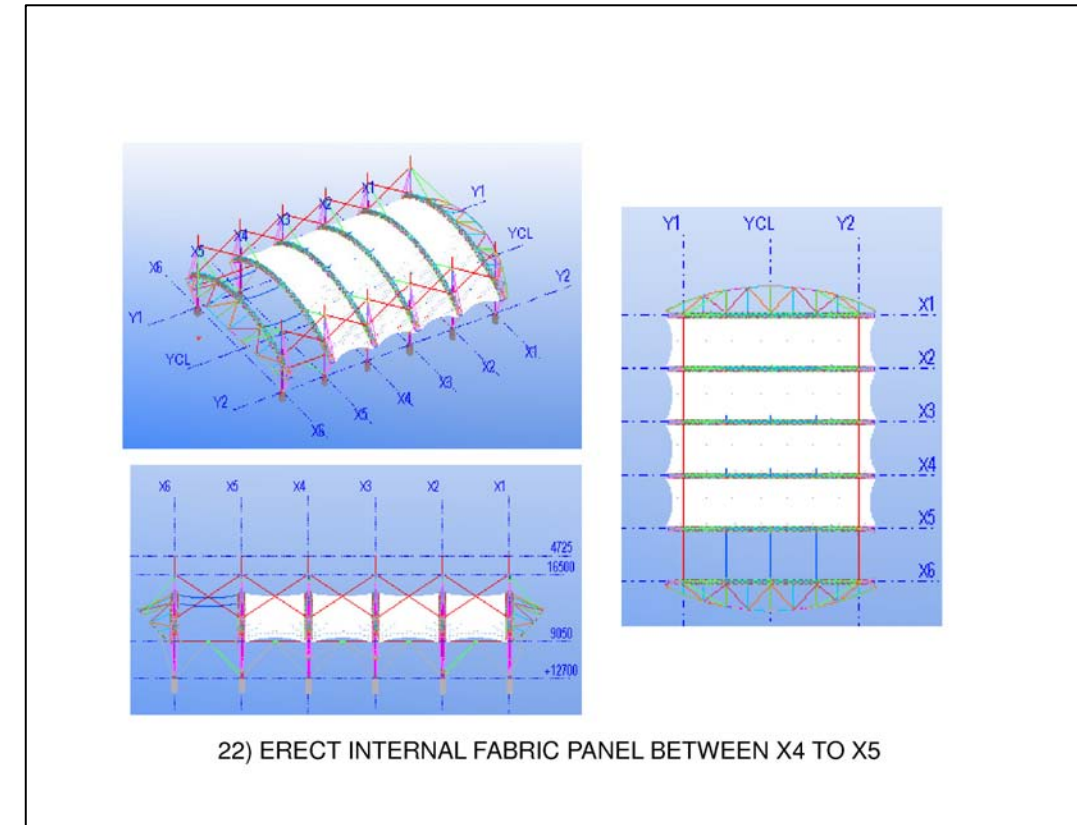
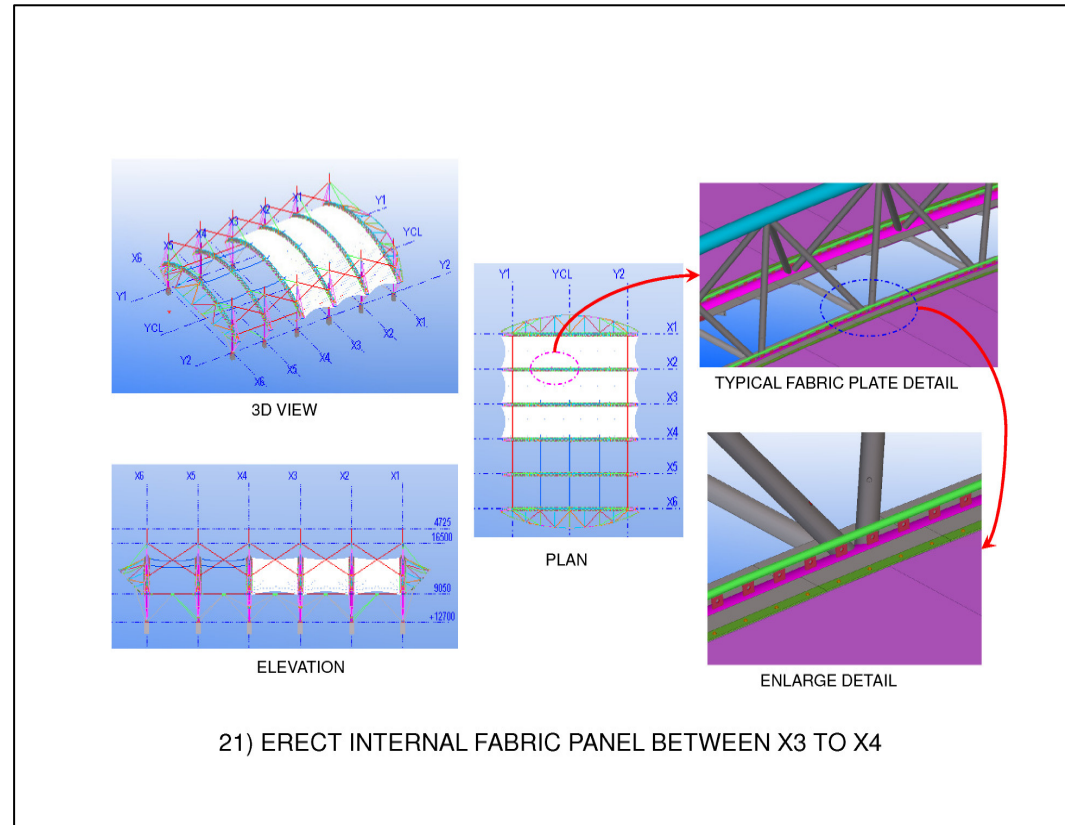
ELEVATION

FABRIC CORNER PLATE DETAIL

20) ERECT 2ND INTERNAL FABRIC PANEL BETWEEN X2 TO X3



ERECTIONSEQUENCE



ERECTIONSEQUENCE

25) ERECT EDGE FABRIC PANEL AT X6 CAP

26) INSTALL SKYLIGHT PANEL ALONG GRID X1 TO X6

27) COMPLETED TENSILE FABRIC ROOF STRUCTURE

11.4 PHOTO IMAGES OF STEEL WORK



PHOTO IMAGES – STEEL WORKS (1 OF 6)



TAPAH FACTORY, MALAYSIA



TAPAH FACTORY, MALAYSIA



TRUSS FABRICATION



TRUSS FABRICATION



TRUSS & COLUMN FABRICATION



COLUMN FLANGE



COLUMN BASE



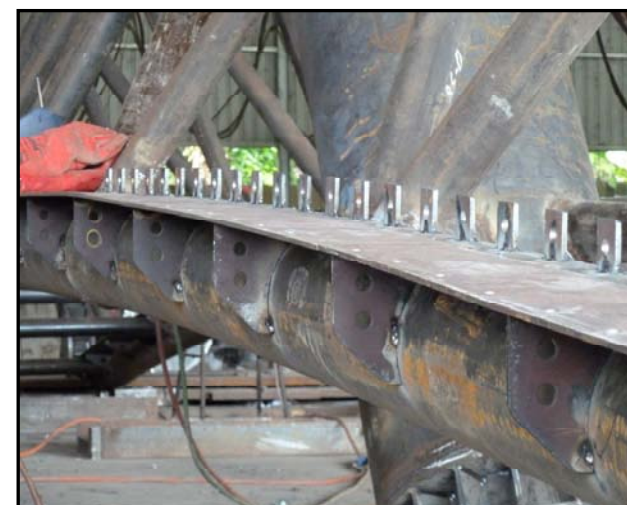
TRUSS WITH COLUMN



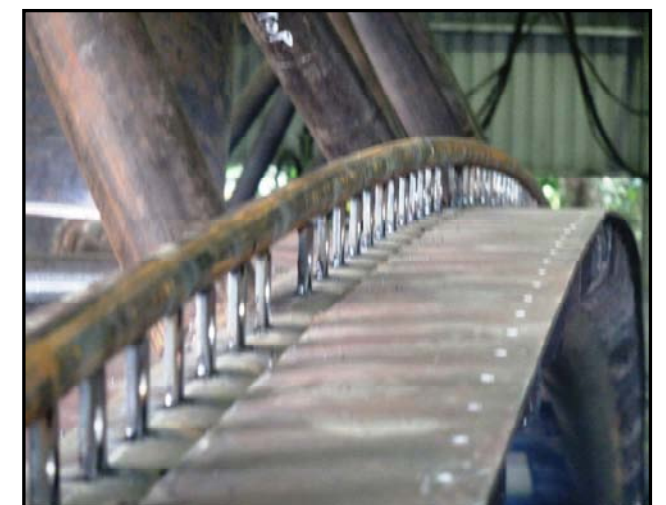
TRUSS FABRICATION



WELDING WORK



CLAMPING PLATE



CLAMPING PLATE



PHOTO IMAGES – STEEL WORKS (2 OF 6)



TRUSS FLANGE JOINT



TRUSS DIAGONALS



ROLLED & WELDED COLUMN



WELDING PREPARATION FOR COLUMN



BEFORE SANDBLASTING



AFTER SANDBLASTING



PAINTED TRUSS



PAINTED TIE



PAINTED COLUMN



COLUMN DELIVERY



UNLOADING OF COLUMN



COLUMN STORAGE



PHOTO IMAGES – STEEL WORKS (3 OF 6)



TRUSS DELIVERY



UNLOADING OF TRUSS



TRUSS STORAGE



TRUSS STORAGE AT SITE



INSTALL HD BOLT



COMPLETED STUMP



ERECT LOWER COLUMN



COLUMN BASE



ERECT LOWER COLUMN



ERECT COLUMN TIE



ERECT COLUMN TIE



ERECTED COLUMN TIE

PHOTO IMAGES – STEEL WORKS (4 OF 6)



ERECT 1/4 TRUSS @ X1



ERECT UPPER COLUMN



ERECT 2/4 TRUSS @ X1



ERECT 4/4 TRUSS @ X1



ERECT UPPER COLUMN



ERECT 3/4 TRUSS @ X1



ERECT 2/4 TRUSS @ X2



ERECT 3/4 TRUSS @ X2



ERECTED TRUSS @ X2



ERECTING TRUSS @ X3



ERECTED TRUSS @ X3



ERECTING TRUSS @ X4



PHOTO IMAGES – STEEL WORKS (5 OF 6)



ERECTED TRUSS @ X4



ERECTING TRUSS @ X5



ERECTED TRUSS @ X6



ERECTING CATWALK



TRUSS FLANGE CONNECTION



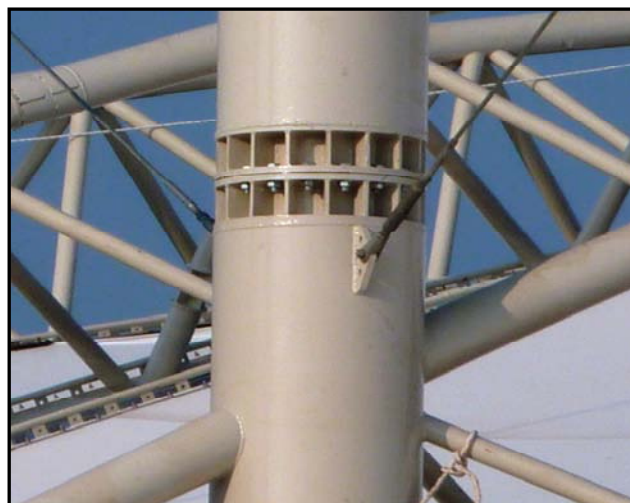
TRUSS FLANGE & TIE JOINT



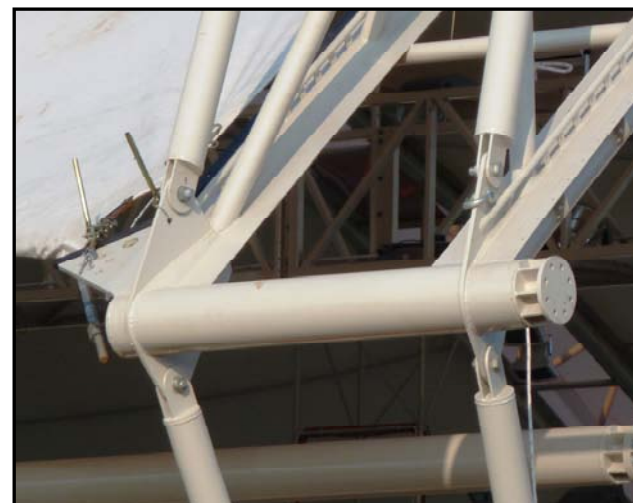
FRONTSTAY CONNECTION



COLUMN TOP CONNECTION



COLUMN FLANGE JOINT



TRUSS END CONNECTION



COLUMN BASE



COLUMN BRACING CONNECTION

PHOTO IMAGES – STEEL WORKS (6 OF 6)



ERECTED TRUSS @ X1



ERECTED TRUSS @ X2



ERECTED TRUSS @ X3



ERECTED TRUSS @ X4



ERECTED TRUSS @ X5



ERECTED TRUSS @ X6



CATWALK IN PROGRESS



COMPLETED CATWALK



11.5 PHOTO IMAGES OF FABRIC WORK



PHOTO IMAGES – FABRIC WORKS (1 OF 6)



VERSEIDAG FABRIC IN SINGAPORE



FABRIC DELIVERY



TRANSPORT TO TAPAH



FABRIC PACKING



FABRIC INSPECTION



FEP DELIVERY



FEP MATERIAL



NEOPRENE



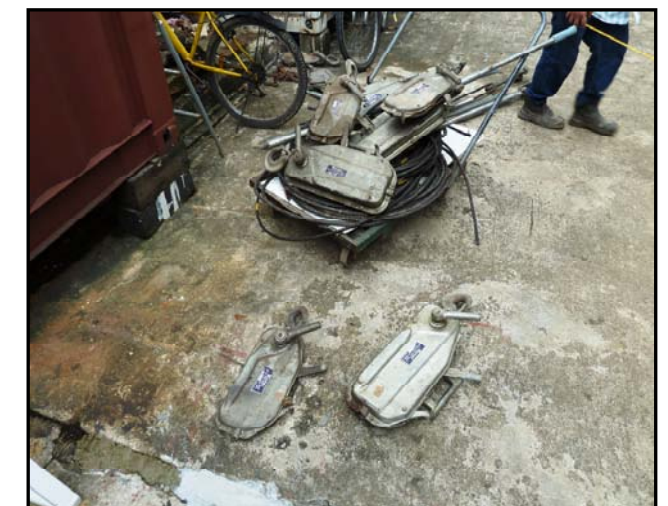
28Ø BORDER CABLE



STABILISING CABLE



FORK END



COMALONG



PHOTO IMAGES – FABRIC WORKS (2 OF 6)



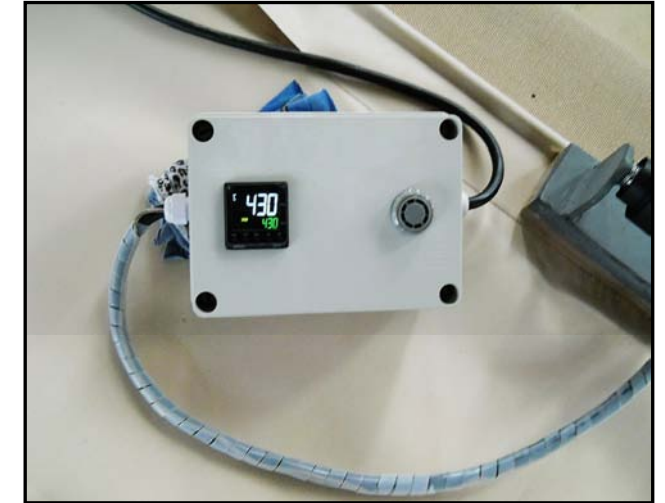
FIXED EDGE PREPARATION



TACKING



TACKING



TEMPERATURE CONTROL



COOLING



SEAMING



TEMPERATURE CONTROL



INTERNAL PANEL



EDGE PANEL WITH POCKET



TRIAL FIT EDGE CABLE



CORNER PREPARATION



CORNER PREPARATION



PHOTO IMAGES – FABRIC WORKS (3 OF 6)



PREPARE TENSIONING TOOL



CLAMPING TOOL (WARP)



CLAMPING TOOL (WEFT)



RATCHET PULLER



TENSIONING ANGLE



FABRIC PANEL AT SITE



FABRIC ERECTION PLATFORM



FIX PLATFORM



LIFTING 1ST FABRIC PANEL



1ST PANEL ON PLATFORM



FIXING HOLDING ROPES



OPENING FABRIC TO Y2



PHOTO IMAGES – FABRIC WORKS (4 OF 6)



OPENING FABRIC TO Y2



OPENING FABRIC TO Y1



OPENING FABRIC TO Y1



1ST FABRIC PANEL INSTALLED



INSTALLING 2ND FABRIC PANEL



OPENING FABRIC TO Y1



OPENING FABRIC TO Y1



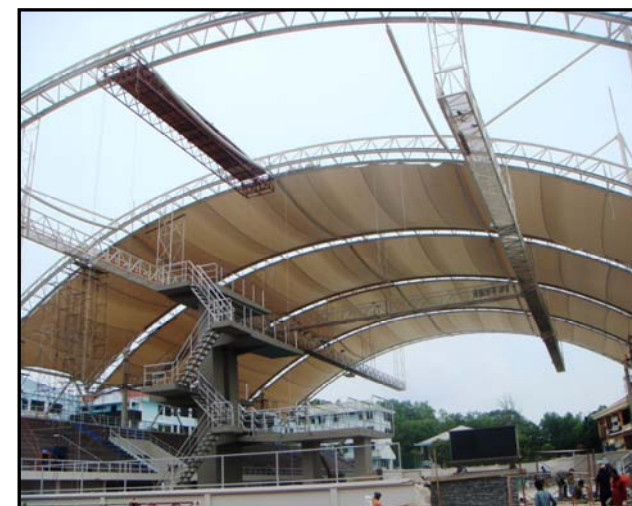
OPENING FABRIC TO Y1



2ND FABRIC PANEL INSTALLED



3RD FABRIC PANEL INSTALLED



4TH FABRIC PANEL INSTALLED



5TH FABRIC PANEL INSTALLED



PHOTO IMAGES – FABRIC WORKS (5 OF 6)



FABRIC TENSIONING



FABRIC TENSIONING



FABRIC TENSIONING



WEFT TENSIONING



WARP TENSIONING



WARP TENSIONING



WARP TENSIONING



FABRIC TENSIONING



WARP TENSIONING



FABRIC TENSIONING



WARP TENSIONING



WARP TENSIONING



PHOTO IMAGES – FABRIC WORKS (6 OF 6)



FIXING FASTENER



FIXING FASTENER



TIE BEAM CLEARANCE



EDGE FIXED



CORNER PLATE



WEFT TENSIONING AT CORNER



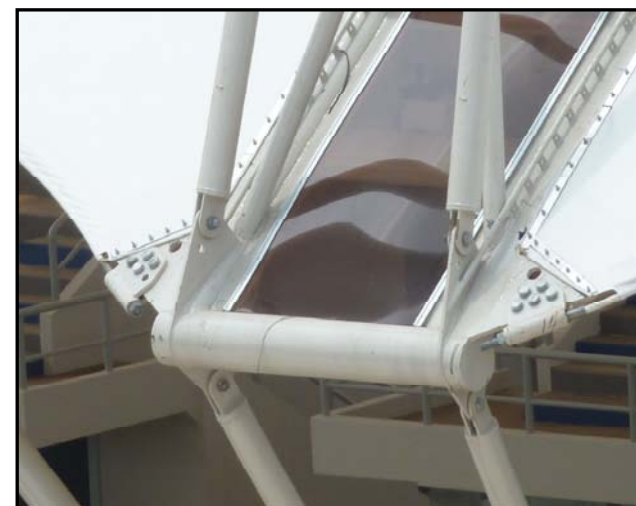
FIXED EDGE



FIXED EDGE



CORNER PLATE



CORNER PLATE



CORNER PLATE



CABLE EDGE



11.6 PHOTO IMAGES OF COMPARISON BEFORE & AFTER ERECTION



PHOTO IMAGE COMPARISON BEFORE & AFTER ERECTION

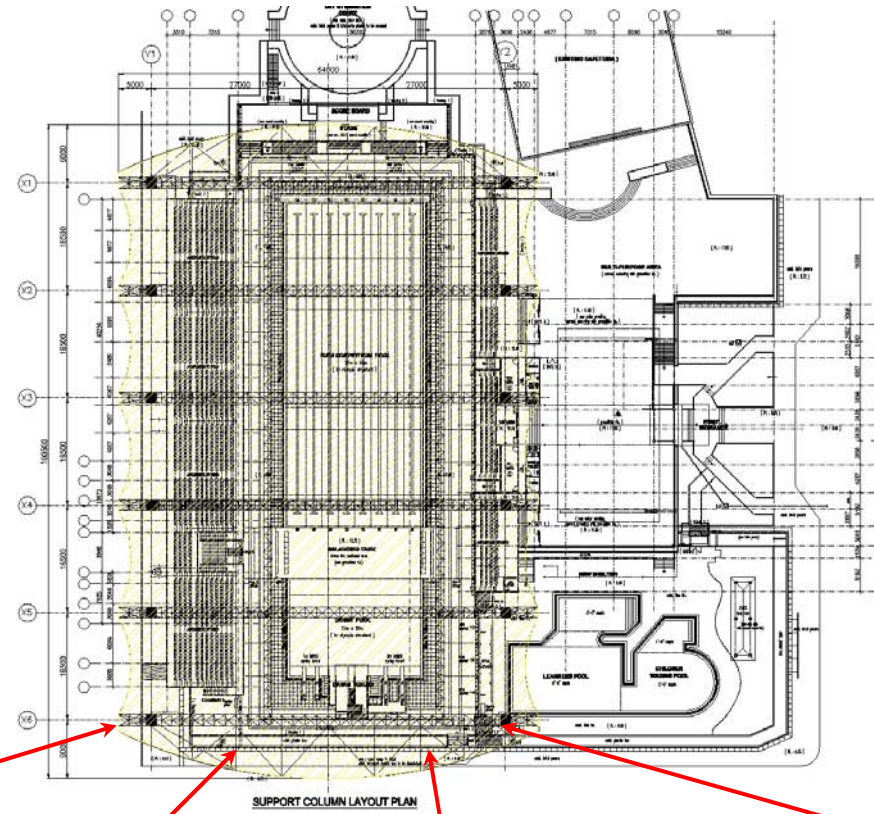
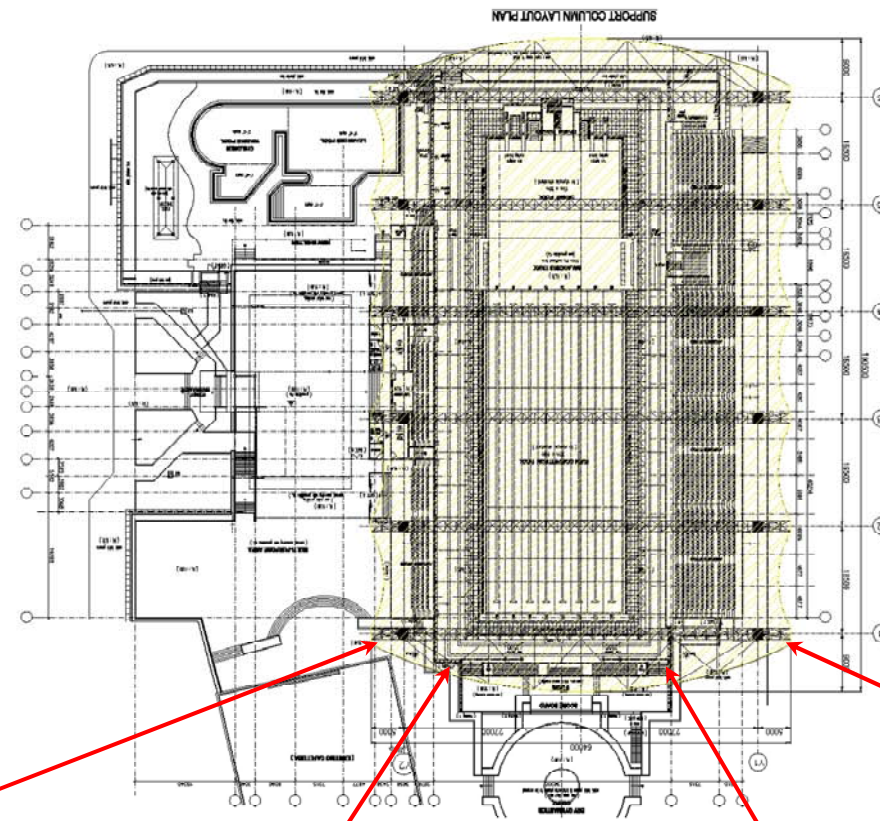


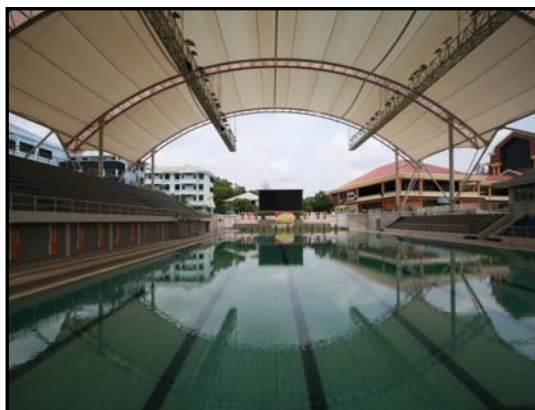
PHOTO IMAGE COMPARISON BEFORE & AFTER ERECTION



11.7 AERIAL VIEW PHASE1 COMPLETION



PROPOSED TENSILE FABRIC ROOF SYSTEM AT KOMPLEKS KOLAM RENANG, WISMA BELIA INDERA MAHKOTA, KUANTAN, PAHANG DARUL MAKMUR, MALAYSIA



INTERNAL VIEW



HANDOVER CEREMONY

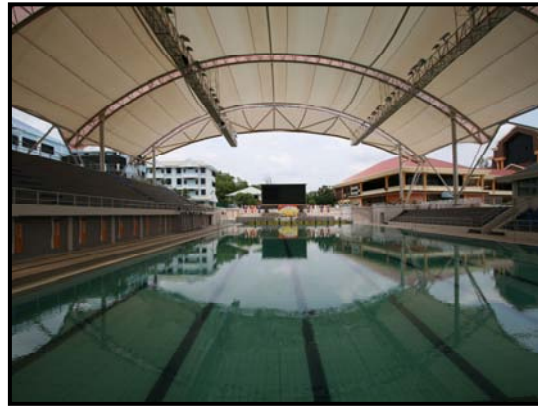


AERIAL VIEW – PHASE 1 COMPLETION

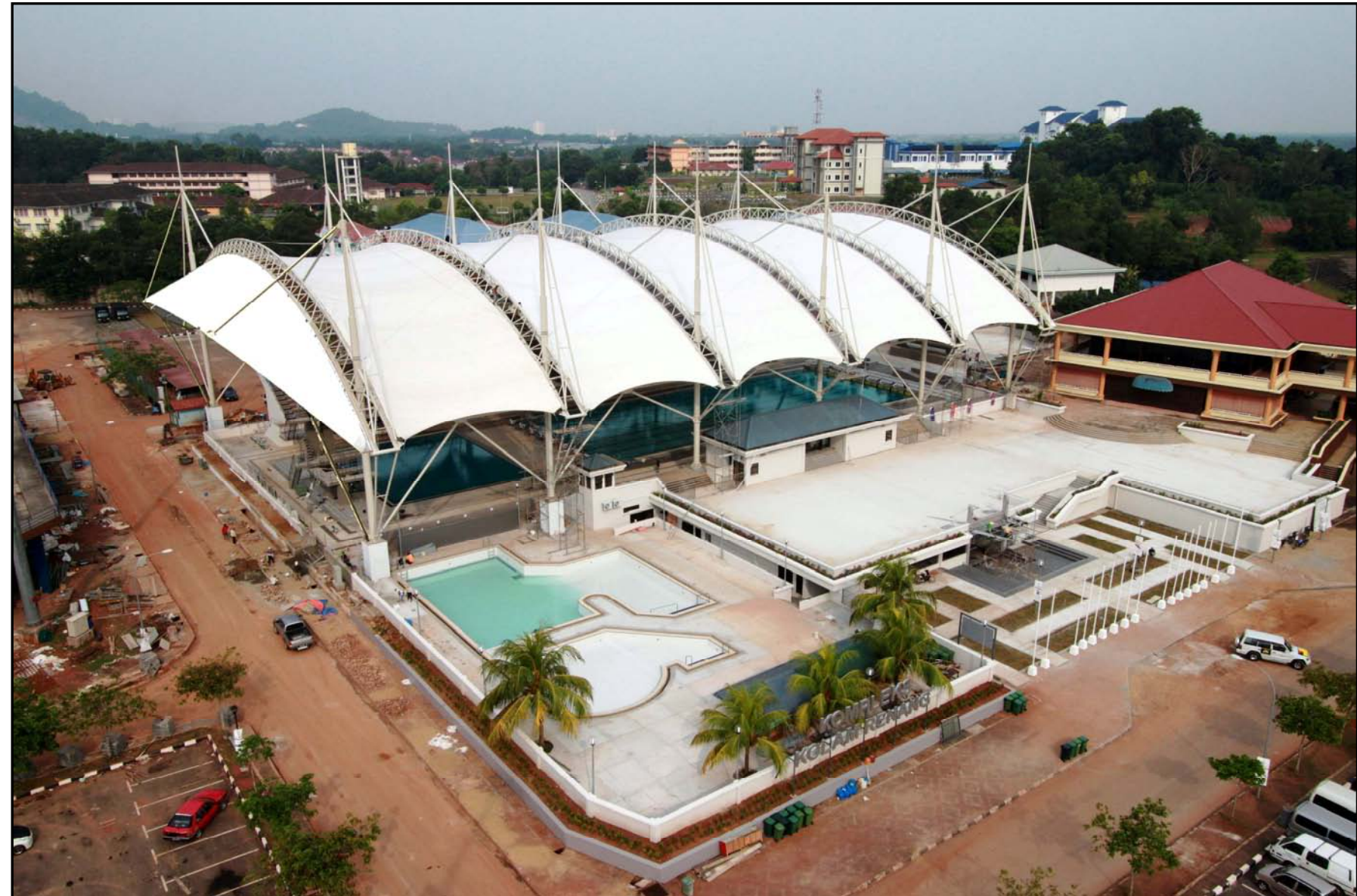
11.8 AERIAL VIEW PHASE2 COMPLETION - IMPRESSION



PROPOSED TENSILE FABRIC ROOF SYSTEM AT KOMPLEKS KOLAM RENANG, WISMA BELIA INDERA MAHKOTA, KUANTAN, PAHANG DARUL MAKMUR, MALAYSIA



INTERNAL VIEW



AERIAL VIEW – PHASE 2 COMPLETION - IMPRESSION

11.9 NEWSPAPER ARTICLES BEFORE THE GAMES



NEWSPAPER ARTICLES – BEFORE THE GAMES

All systems go

AFTER a month's delay, upgrading works for the 15th Malaysia Games swimming pool in Kuantan were finally completed and it was officially handed over to the organising committee yesterday. Since it was the last venue to be completed, Games chief executive officer Ahmad Hairi Hussin made a 'splashing' gimmick when he jumped into the Olympic-size swimming pool from a springboard after making a final inspection on the facility which utilised the latest technology from Germany. Hairi said he was relieved the pool was ready for the Games. The RM21 million upgrading works were supposed to be completed on May 30.



Malaysia Games chief executive officer Ahmad Hairi Hussin looks satisfied with the swimming pool, renovated at a cost of RM21 million, which will be the venue for aquatic events. Pic by Halim Mat Ali

He said upgrading works and construction of new venues — costing about RM238 million — had already been completed, including the Darulmakmur stadium where the opening ceremony will be officiated by Sultan Ahmad Shah of Pahang on Saturday and closed by Prime Minister Datuk Seri Najib Razak on July 16. Some 7,000 athletes and officials will participate in the Games which offer 377 gold, 377 silver and 453 bronze medals. By M. Hamzah Jamaludin

Advertisement for 'SUKAN MALAYSIA XV, PAHANG 2012' featuring a car with 'TOR GAJAJ' branding and a cartoon mascot. Text includes '改造愛車 挺馬運會' and '來自丹甘榜柏拉慕的宛拉賽米 (49岁) 配合彭亨州即将承办马运会而“投资”改造“迷你轿车”，在车顶上设立吉祥物大象、张贴各式标志及国旗，充分展现爱国意识。' and 'SUKAN MALAYSIA XV, PAHANG 2012, Kuantan-Pekan-Temerloh'.

News article titled '22個賽事場地通過測試 彭準備就緒迎馬運會' (22 sports venues passed tests, Peng ready to welcome the games). It features a large group photo of officials and athletes. Text includes '馬運會彭亨州運動員也出席游泳池移交儀式，並與所有嘉賓及馬丹市議會官員合照。' and '變身後媲美世界水平 市會泳池新貌迎馬運會'.

Large newspaper article titled '22賽場準備受當' (22 venues ready to receive). It includes sub-headings like '承商移交泳池' and '各小組將召開會議'. The article discusses the completion of 22 sports venues for the 15th Malaysia Games in Kuantan, Pahang. It mentions the involvement of contractors and the final preparations for the games starting on July 4th.

Large newspaper article titled '市會泳池新貌迎馬運會' (City council pool new look welcomes the games). It features a sub-heading '發揮游泳池最大功能' and includes a table of events. The article details the renovation of the city council swimming pool to meet international standards, highlighting the use of advanced technology and materials. It also lists the dates and locations for various events during the games.

11.10 PHOTO IMAGES DURING THE GAMES



PHOTO IMAGES – DURING THE GAMES



11.11 BIAXIAL TEST REPORT



Bi-axiale tensile test on technical membranes

persons in charge: Dipl.-Ing. K. Saxe/G. Knop/Dipl.-Ing. T. Homm date: 09.01.2012
 location: V15R00H01

customer: Verseidag Indutex GmbH
 Industriestr. 56
 47803 Krefeld

subject of order: biaxiale test on technical membranes
 for the project: Swimming Pool, Wisma Belia, Kuantan,
 Malaysia

test procedure: according to specifications by:
 A.W. Lam

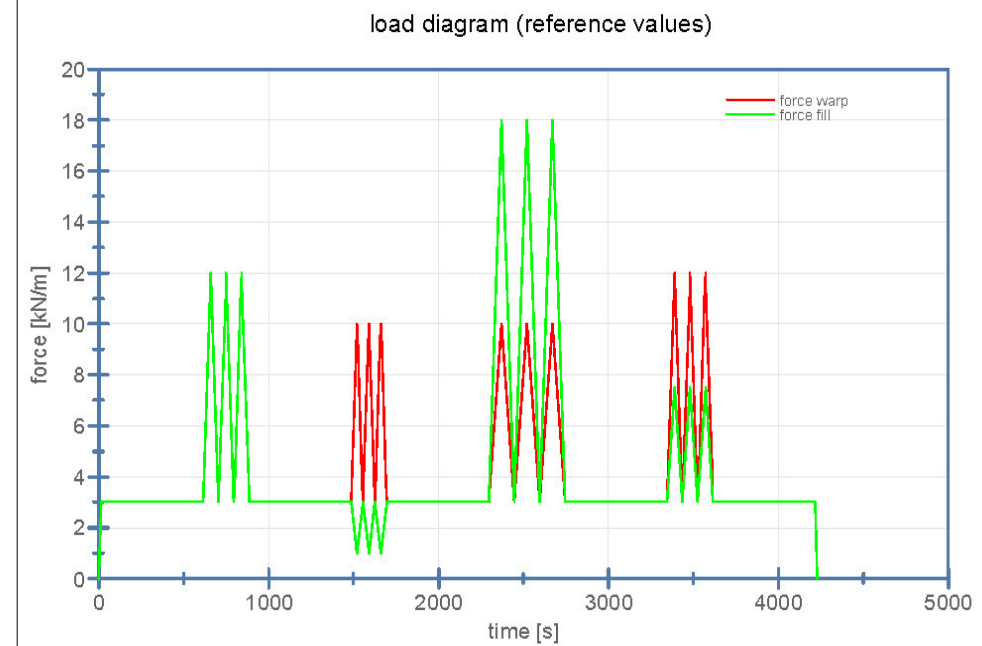
material: Versidag B18089, piece 00980777A04

test: V1112

comments:

Test report on bi-axiale tensile test

date: 09.01.2012 persons in charge: Dipl.-Ing. K. Saxe/G. Knop/Dipl.-Ing. T. Homm
 test: V1112 material: Versidag B18089, piece 00980777A04



axis 1: warp direction - Minimum: 0.10 kN/m
 - Maximum: 12.00 kN/m

axis 2: fill direction - Minimum: 0.10 kN/m
 - Maximum: 18.00 kN/m

loading rate: 0.2 (kN/m)/s at the higher gradient

test temperature: 23.6°C

time interval: 1.0, 2.0, 3.0, 10.0 s

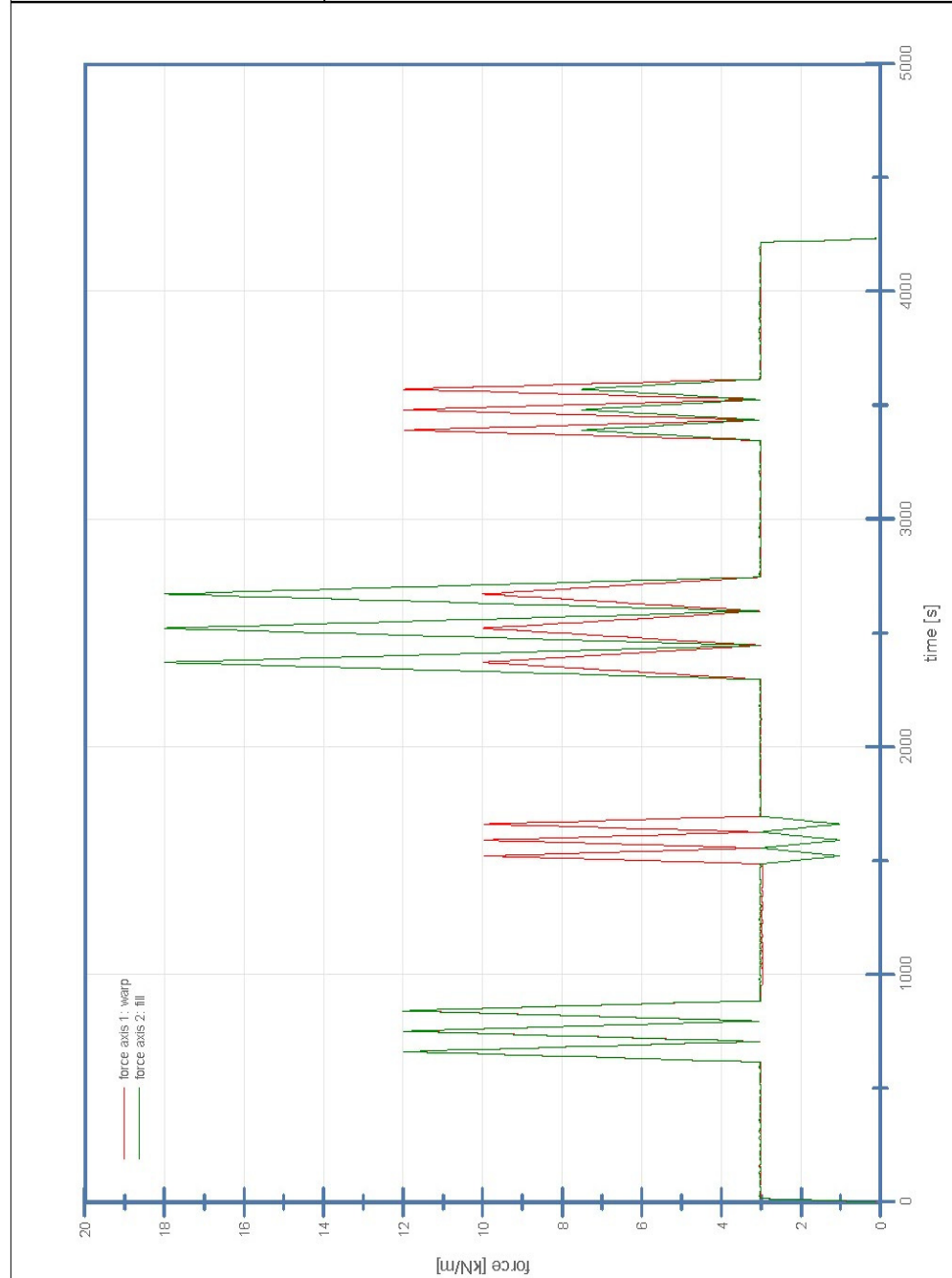
comments:



Control factor of load

test: V1112

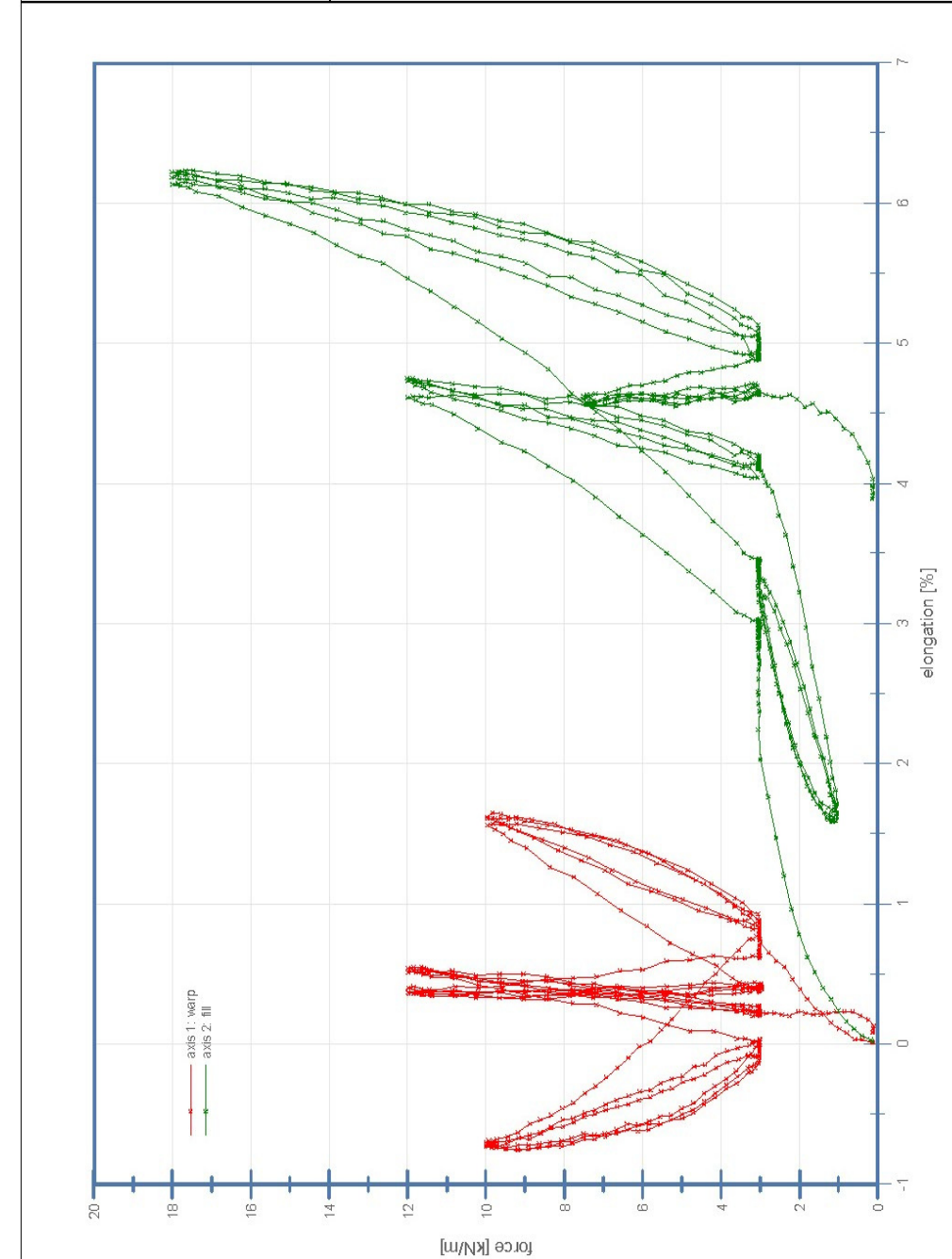
material: Versidag B18089, piece 00980777A04



Force-elongation-diagram to bi-axiale tensile test

test: V1112

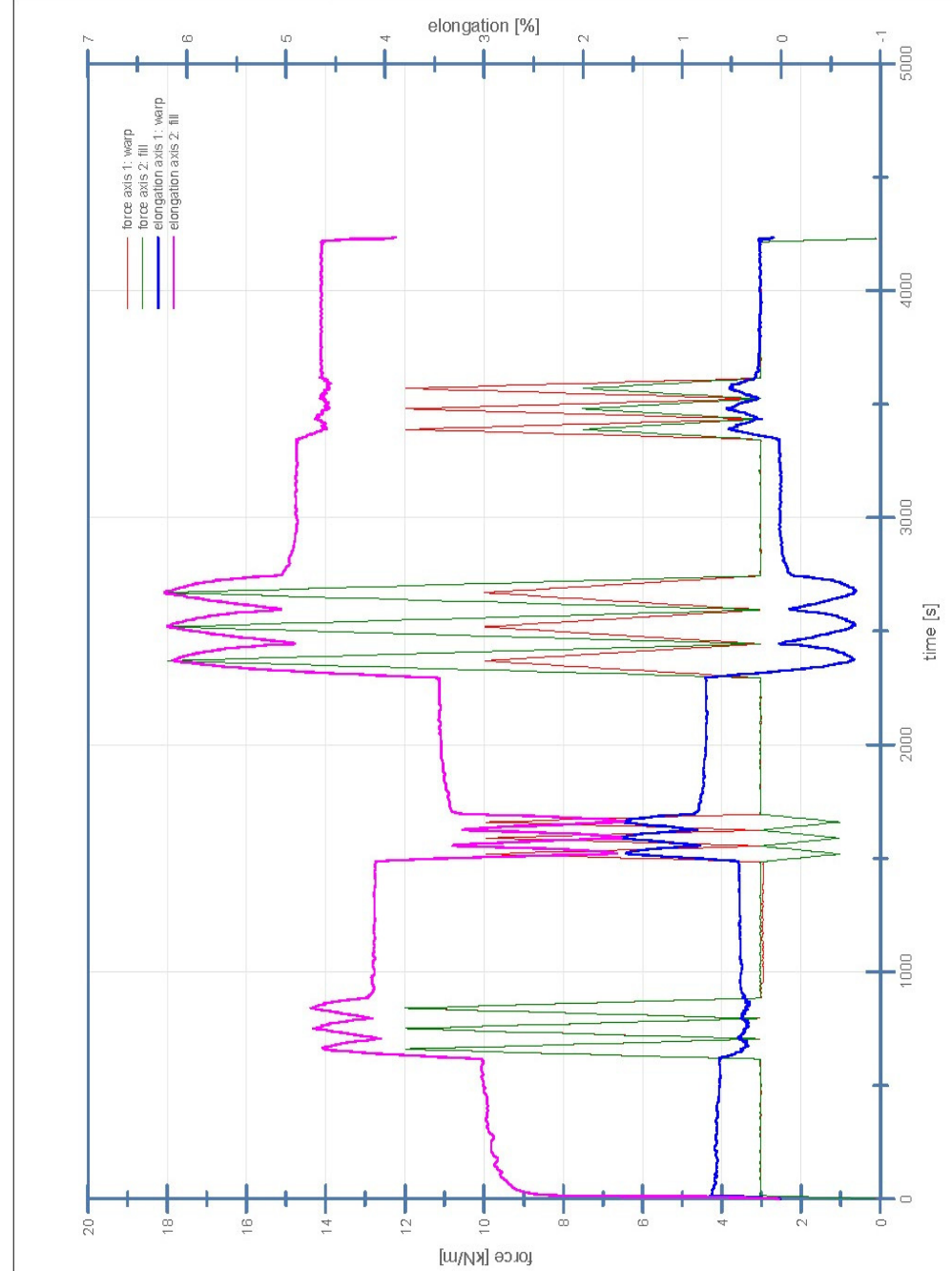
material: Versidag B18089, piece 00980777A04



Force-elongation-time-diagram to bi-axiale tensile test

test: V1112

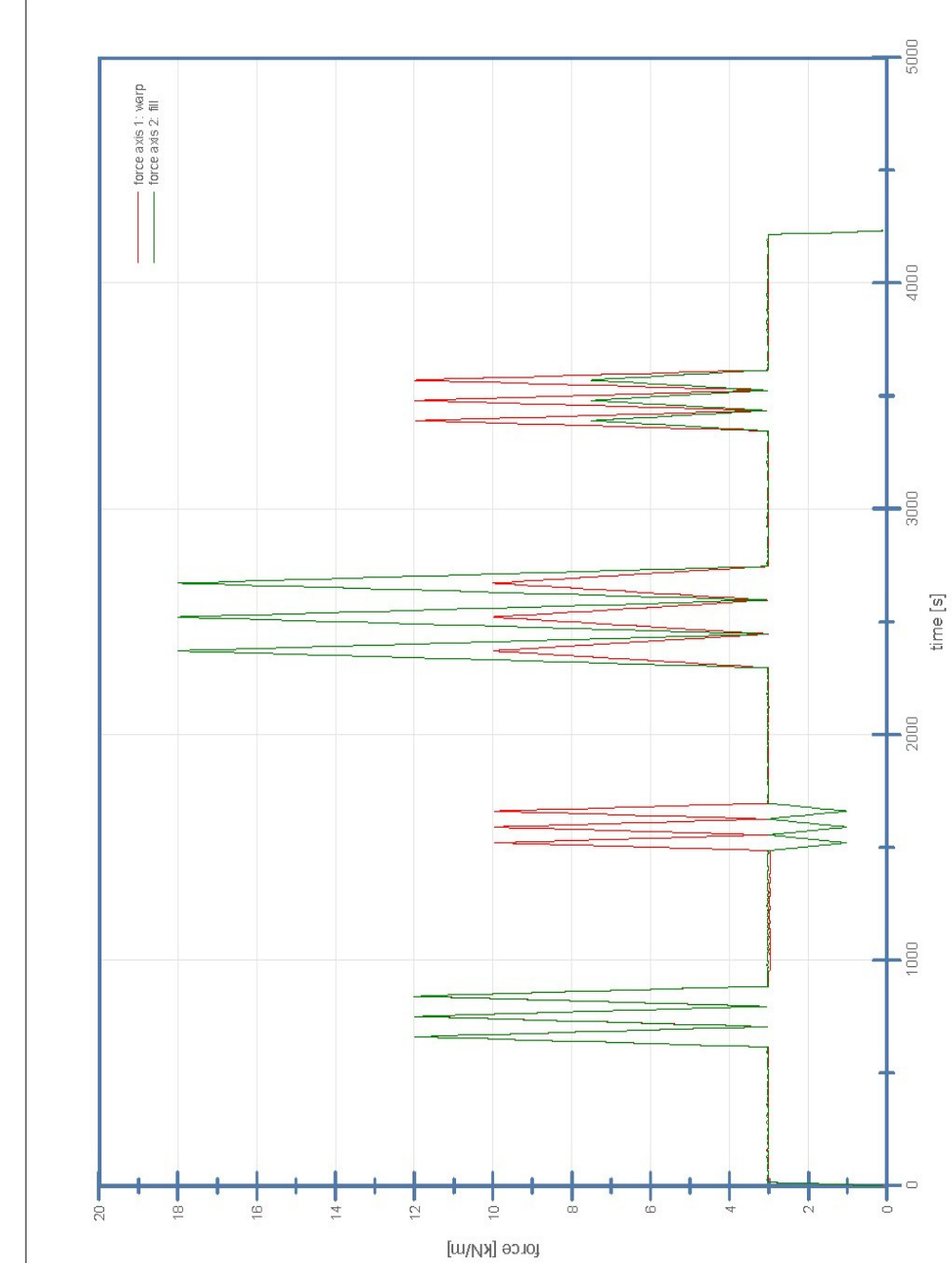
material: Versidag B18089, piece 00980777A04



Force-time-diagram to bi-axiale tensile test

test: V1112

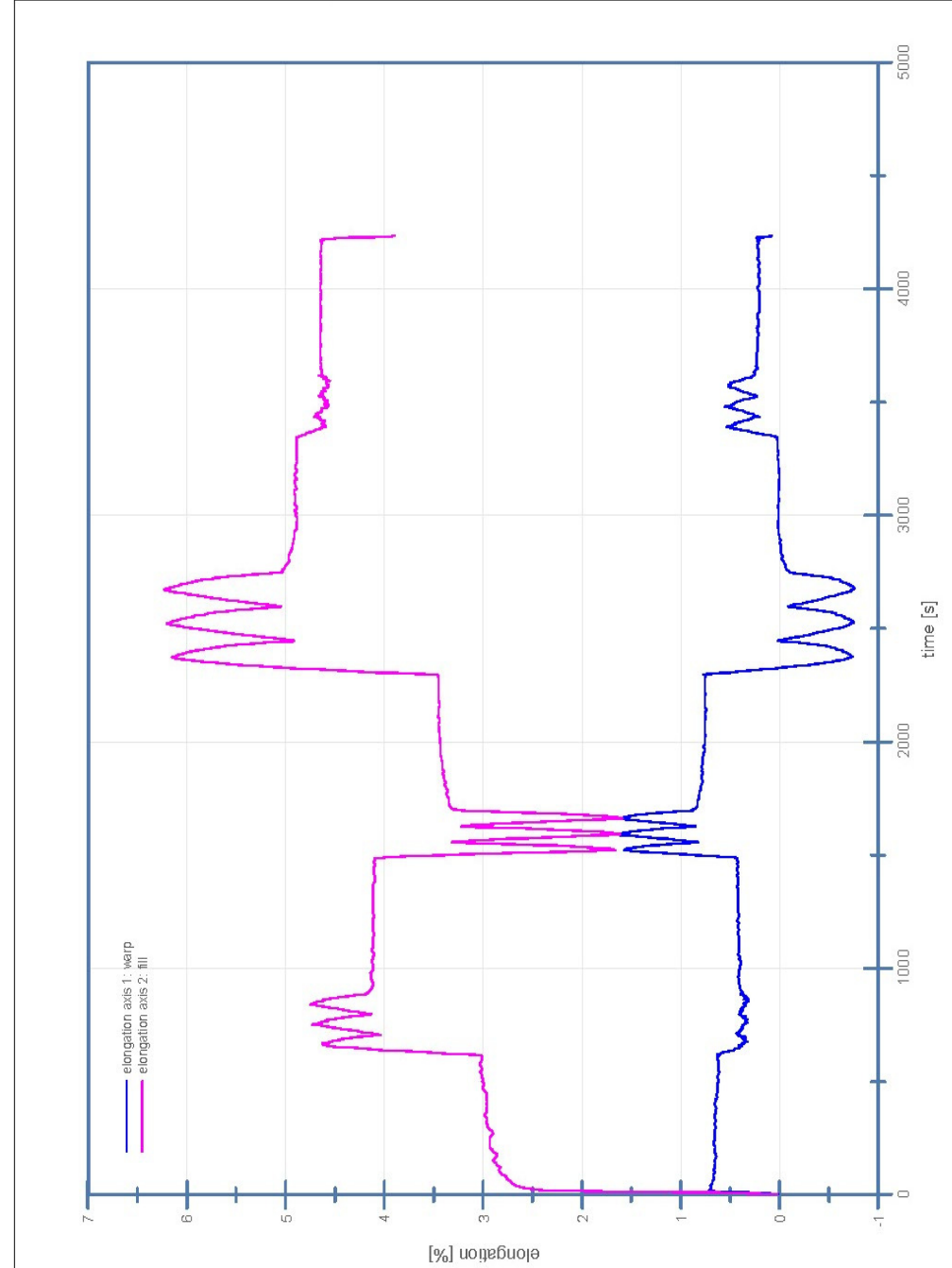
material: Versidag B18089, piece 00980777A04



Elongation-time-diagram to tensile test

test: V1112

material: Versidag B18089, piece 00980777A04



Measured data of bi-axiale tensile test

test: V1112

material: Versidag B18089, piece 00980777A04

page: 3

time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongation [%] fill	time [s]	force [kN/m] warp	force [kN/m] fill	elongation [%] warp	elongation [%] fill
1518.0	9.55	1.15	1.50	1.90	1660.0	9.95	1.03	1.62	1.62
1519.0	9.76	1.07	1.53	1.81	1661.0	9.82	1.06	1.65	1.59
1520.0	9.95	1.03	1.56	1.71	1662.0	9.62	1.14	1.64	1.59
1521.0	9.81	1.07	1.57	1.67	1663.0	9.42	1.18	1.62	1.59
1522.0	9.61	1.13	1.57	1.66	1664.0	9.22	1.25	1.61	1.60
1523.0	9.42	1.18	1.56	1.67	1665.0	9.02	1.30	1.59	1.61
1524.0	9.21	1.25	1.57	1.69	1666.0	8.43	1.45	1.56	1.69
1527.0	8.62	1.44	1.54	1.72	1671.0	7.82	1.64	1.53	1.75
1530.0	8.03	1.60	1.51	1.79	1674.0	7.23	1.80	1.49	1.84
1533.0	7.43	1.76	1.48	1.90	1677.0	6.63	1.99	1.45	1.99
1536.0	6.83	1.95	1.42	2.00	1680.0	6.03	2.16	1.37	2.11
1539.0	6.23	2.11	1.37	2.13	1683.0	5.44	2.33	1.31	2.28
1542.0	5.64	2.27	1.29	2.29	1686.0	4.84	2.51	1.24	2.50
1545.0	5.04	2.46	1.22	2.48	1689.0	4.24	2.68	1.14	2.69
1548.0	4.44	2.62	1.14	2.70	1692.0	3.64	2.86	1.04	2.94
1551.0	3.84	2.79	1.02	2.95	1693.0	3.45	2.91	1.01	2.99
1552.0	3.64	2.86	0.98	3.04	1694.0	3.25	2.97	0.94	3.09
1553.0	3.44	2.91	0.93	3.12	1695.0	3.05	3.03	0.93	3.15
1554.0	3.25	2.97	0.90	3.19	1696.0	3.02	3.03	0.88	3.21
1555.0	3.04	3.02	0.83	3.29	1698.0	3.02	3.04	0.87	3.25
1556.0	3.19	2.98	0.82	3.32	1700.0	3.03	3.03	0.88	3.27
1557.0	3.39	2.92	0.84	3.31	1702.0	3.02	3.04	0.87	3.29
1558.0	3.57	2.89	0.87	3.30	1704.0	3.02	3.03	0.86	3.31
1559.0	3.77	2.84	0.89	3.26	1710.0	3.02	3.02	0.84	3.33
1560.0	3.98	2.75	0.91	3.22	1720.0	3.01	3.03	0.83	3.34
1563.0	4.57	2.58	0.95	3.13	1730.0	3.01	3.03	0.83	3.35
1566.0	5.18	2.41	1.03	3.01	1740.0	3.01	3.02	0.83	3.35
1569.0	5.77	2.23	1.09	2.87	1750.0	3.01	3.02	0.81	3.35
1572.0	6.36	2.07	1.14	2.72	1760.0	3.02	3.02	0.82	3.36
1575.0	6.96	1.88	1.24	2.55	1770.0	3.02	3.02	0.81	3.37
1578.0	7.56	1.73	1.31	2.39	1780.0	3.02	3.03	0.81	3.36
1581.0	8.16	1.56	1.38	2.19	1790.0	3.01	3.03	0.79	3.36
1584.0	8.76	1.39	1.47	2.04	1800.0	3.01	3.02	0.80	3.38
1587.0	9.35	1.22	1.54	1.85	1810.0	3.01	3.04	0.79	3.39
1588.0	9.55	1.16	1.57	1.78	1820.0	3.02	3.04	0.78	3.38
1589.0	9.76	1.10	1.61	1.73	1830.0	3.03	3.03	0.78	3.39
1590.0	9.95	1.04	1.61	1.65	1840.0	3.01	3.03	0.79	3.40
1591.0	9.82	1.07	1.61	1.61	1850.0	3.02	3.03	0.79	3.40
1592.0	9.62	1.13	1.61	1.61	1860.0	3.02	3.02	0.77	3.41
1593.0	9.42	1.19	1.60	1.63	1870.0	3.02	3.01	0.79	3.39
1594.0	9.23	1.25	1.62	1.64	1880.0	3.01	3.03	0.78	3.41
1596.0	8.82	1.37	1.60	1.65	1890.0	3.01	3.03	0.79	3.41
1599.0	8.24	1.54	1.57	1.71	1900.0	3.02	3.04	0.78	3.41
1602.0	7.63	1.72	1.50	1.81	1910.0	3.02	3.03	0.78	3.41
1605.0	7.04	1.89	1.47	1.92	1920.0	3.01	3.04	0.78	3.42
1608.0	6.43	2.07	1.42	2.05	1930.0	3.02	3.04	0.78	3.42
1611.0	5.84	2.21	1.36	2.19	1940.0	3.02	3.03	0.77	3.43
1614.0	5.23	2.39	1.26	2.38	1950.0	3.02	3.01	0.77	3.43
1617.0	4.63	2.57	1.17	2.57	1960.0	3.01	3.04	0.76	3.43
1620.0	4.03	2.74	1.07	2.82	1970.0	3.03	3.03	0.76	3.43
1622.0	3.63	2.86	0.99	2.94	1980.0	3.02	3.04	0.77	3.43
1623.0	3.44	2.91	0.96	3.06	1990.0	3.02	3.02	0.76	3.43
1624.0	3.24	2.96	0.93	3.13	2000.0	3.01	3.03	0.76	3.44
1625.0	3.04	3.03	0.88	3.20	2010.0	3.01	3.04	0.76	3.43
1626.0	2.84	3.09	0.85	3.22	2020.0	3.03	3.03	0.76	3.44
1627.0	2.63	2.93	0.88	3.20	2030.0	3.01	3.02	0.75	3.44
1628.0	2.43	2.87	0.88	3.18	2040.0	3.01	3.03	0.76	3.44
1629.0	2.23	2.82	0.90	3.19	2050.0	3.03	3.03	0.76	3.45
1632.0	1.87	2.64	0.97	3.09	2060.0	3.02	3.04	0.76	3.44
1635.0	1.51	2.49	1.03	2.96	2070.0	3.01	3.03	0.76	3.45
1638.0	1.15	2.31	1.09	2.85	2080.0	3.02	3.03	0.76	3.45
1641.0	0.79	2.12	1.16	2.70	2090.0	3.01	3.02	0.76	3.44
1644.0	0.43	1.96	1.24	2.53	2100.0	3.00	3.04	0.75	3.44
1647.0	0.07	1.79	1.33	2.36	2110.0	3.02	3.03	0.75	3.46
1650.0	0.00	1.62	1.40	2.20	2120.0	3.02	2.99	0.76	3.45
1653.0	0.00	1.44	1.46	2.05	2130.0	3.01	3.03	0.75	3.45
1656.0	0.00	1.27	1.52	1.87	2140.0	3.01	3.03	0.74	3.45
1657.0	0.00	1.20	1.54	1.78	2150.0	3.02	3.02	0.76	3.45
1658.0	0.00	1.13	1.57	1.74	2160.0	3.02	3.04	0.76	3.44
1659.0	0.00	1.09	1.59	1.69	2170.0	3.02	3.02	0.76	3.44



11.12 DESIGN CALCULATION



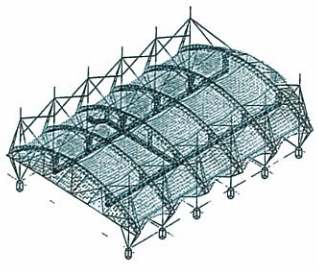
Sedibana Sdn. Bhd.
No. 11 Jalan Asraka U8/B4, Seksyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222

Project No: TPL 40581
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0

Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

CADANGAN MENAIK TARAF KOLAM RENANG SERTA KERJA-KERJA BERKAITAN DI WISMA BELLA INDERA MAHKOTA, KUANTAN PAHANG DARUL MAKMUR, MALAYSIA UNTUK MAJLIS PERBANDARAN KUANTAN

ANALYSIS & DESIGN CALCULATION FOR THE TENSILE MEMBRANE ROOF



Designed & Submitted by: SM Tan

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Asraka U8/B4, Seksyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222

Project No: TPL 40581
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0

Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

TABLE OF CONTENTS	PAGES
1. GENERAL	4 - 9
1.1 INTRODUCTION	
1.2 STRUCTURAL SYSTEM	
1.3 SCOPE OF DOCUMENT	
1.4 REFERENCE DOCUMENT	
1.5 UNITS	
1.6 DESIGN CODE & STANDARD	
2. ANALYSIS AND DESIGN CRITERIA	10 - 12
2.1 COORDINATES SYSTEM	
2.2 METHOD OF ANALYSIS	
2.3 STRUCTURAL STEEL DESIGN MODEL	
2.4 STEEL MATERIAL	
2.5 DESIGN METHOD	
3. LOADING ASSUMPTION	13 - 19
3.1 SELF WEIGHT	
3.2 DEAD LOAD OF CATWALK	
3.3 PRESTRESS LOAD	
3.4 IMPOSED LIVE LOAD	
3.5 WIND LOAD	
4. BASIC LOAD CASES & LOAD COMBINATION	20 - 21
4.1 BASIC LOAD CASES	
4.2 LOAD COMBINATION FOR SERVICE LIMIT STATE	
4.3 LOAD COMBINATION FOR ULTIMATE LIMIT STATE	
5. BOUNDARY CONDITION	22
6. DESIGN OF STEEL MEMBERS	23 - 26
7. DESIGN OF CABLES	27
8. DESIGN OF HOLDING DOWN BOLT	28 - 30
9. DESIGN OF CONNECTIONS	31 - 32
10. APPENDIX A - STAADPRO INPUT & OUTPUT DATA	
A1. STAADPRO INPUT DATA	a1 - a90
A2. STAADPRO JOB INFORMATION	a91
A3. REACTIONS, REACTION SUMMARY & ENVELOPE	a92 - a98
A4. STEEL DESIGN CHECK	a99 - a202
A5. STEEL NODE NUMBER CORRESPOND TO FABRIC FIX POINT	a203
A6. BEAM MAXIMUM FORCES BY SECTION PROPERTY	a204

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Asraka U8/B4, Seksyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222

Project No: TPL 40581
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0

Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

TABLE OF CONTENTS	PAGES
11. APPENDIX B - FABRIC STATIC OUTPUT DATA	
B1. EDGE PANEL NEXT TO DIVING POOL	
FABRIC NODE NUMBER LAYOUT PLAN	b1
- PRESTRESS LOAD CASE	b2 - b4
- LIVE LOAD CASE	b5 - b7
- WIND UPLIFT	b8 - b10
- WIND PRESSURE	b11 - b13
- WIND FROM ENTRANCE	b14 - b16
- WIND FROM AUDIENCE STAND	b17 - b19
B2. INTERNAL PANEL	
FABRIC NODE NUMBER LAYOUT PLAN	b20
- PRESTRESS LOAD CASE	b21 - b23
- LIVE LOAD CASE	b24 - b26
- WIND UPLIFT	b27 - b29
- WIND PRESSURE	b30 - b32
- WIND FROM ENTRANCE	b33 - b35
- WIND FROM AUDIENCE STAND	b36 - b38
B3. EDGE PANEL NEXT TO SCORE BOARD	
FABRIC NODE NUMBER LAYOUT PLAN	b39
- PRESTRESS LOAD CASE	b40 - b42
- LIVE LOAD CASE	b43 - b45
- WIND UPLIFT	b46 - b48
- WIND PRESSURE	b49 - b51
- WIND FROM ENTRANCE	b52 - b54
- WIND FROM AUDIENCE STAND	b55 - b57
12. APPENDIX C - TECHNICAL DATA	
C1. CABLE	c1 - c2
C2. VERSEIDAG MEMBRANE PTFE B18089	c3 - c4

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Asraka U8/B4, Seksyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222

Project No: TPL 40581
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0

Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

1. GENERAL

1.1 INTRODUCTION

The proposed tensile fabric roof structure is part of the upgrading work over the existing Wisma Bella Indera Mahkota swimming pool complex at Kuantan. It is the aquatic events venue for the 15th Malaysia Games held in Kuantan, Pahang Darul Makmur from 7th July to 16th July 2012.

The PTFE (polytetrafluoroethylene) coated glass fiber roof covered a main competition pool of 21m x 50m and a diving pool of 15m x 20m, both are of olympic standard. The membrane used is B18089 of Verseidag, Germany. The foot print of the roof is approximately 100m x 64m on plan.

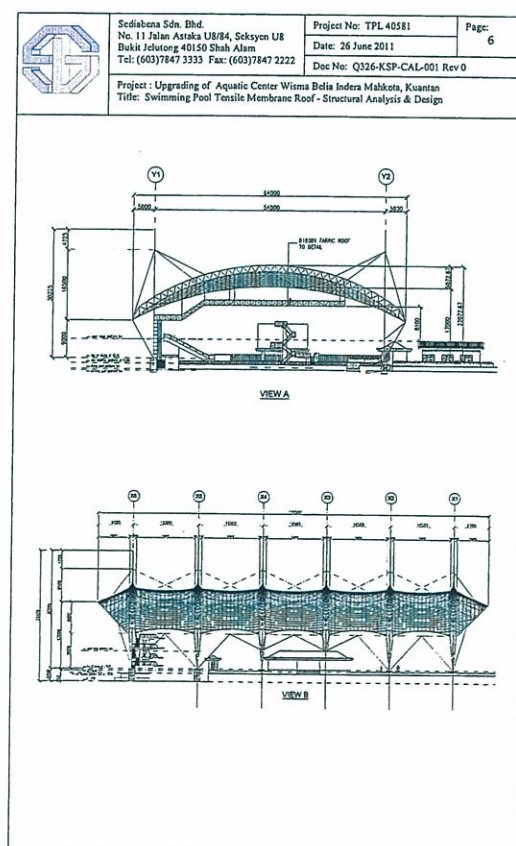
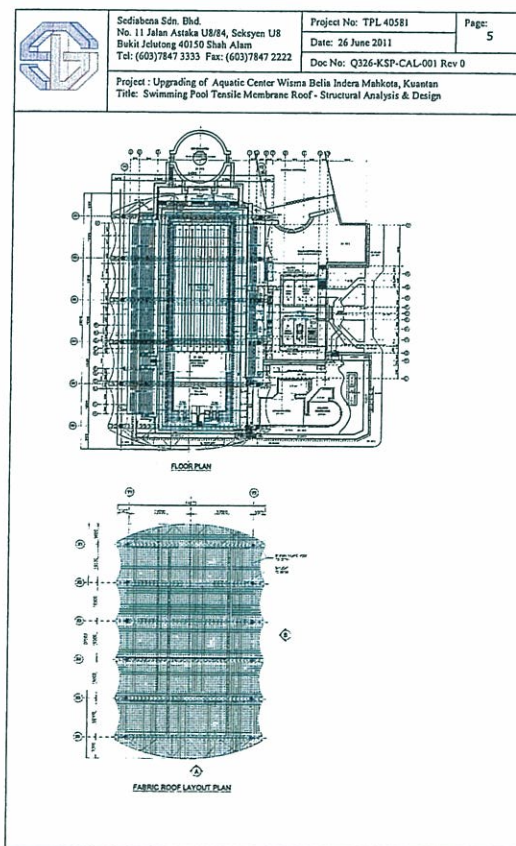
The swimming pool roof is a barrel vault like structure of 82.5m length with both end a 9m cantilevered eyelid canopy which is about 24 deg tilted downward.

The steel roof structure comprise of 6 nos of 3D triangular truss spaced at 16.5m. Each truss is integrated with steel mast at 54m center to center at both end. The overall height of columns are 30m and top of truss is 22m above the general pool level respectively. These columns are stabilized with frontstay and upper and lower backstay. There are 1 column near the main entrance which 'punch' through the roof of the VIP room. The overall structure are braced longitudinally along the column gridline and also 3 tie beam at 3 location of bottom chord of the 3D truss. The base of column mast is then fixed to RC stump of 2.8m above the general pool level.

Approximately 220m run of 1.2m wide catwalk is hanged from these 3D truss at 15 location to provide access for maintenance of light fitting which is also fixed on the railing of catwalk.

The fabric roof consist of 5 internal panel and 2 end panel of approximately 6000m² area in total. The internal fabric panel is secured across the bottom chord of 2 nos of 3D truss and inside of the triangular truss is then fixed with polycarbonate.

Q326-Kuantan



Sedibana Sdn. Bhd.
No. 11 Jalan Asraka U8/B4, Seksyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222

Project No: TPL 40581
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0

Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

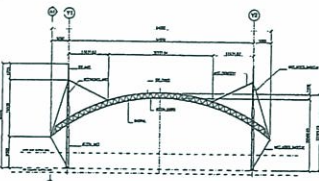
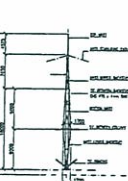
1.2 STRUCTURAL SYSTEM

The steel roof structure comprise of 6 nos of 3D triangulated truss of 1 top chord 15.5m height and 2 bottom chord of 1.7m wide. These trusses are spaced at 16.5m and integrated with steel column at 54m center. The overall length of the truss is 64m with 11.6m rise at the center. Each of these integrated truss with column height of 30m is stabilized with 1 front stay and 2 upper and lower backstay.

The stability of the structure is dependent on ties and bracing along the column longitudinally. They are also tied quarterly at 3 locations across the bottom chord of the trusses. At the upper part of the column, a pair of crossly brace safety cable is introduced.

Due to site access and constraint, the steel structure is designed such that it will be able to be lifted by a small tonnage crane eg. 30 tons and so bolted connection is decided.

The 64m truss is then make into 4 segment with flange joint connection. The 30m high column is also flange jointed just before and after the 3D truss. So is the bracing and ties along the columns, at the end canopies are assembled in parts by bolting system.

SECTION A-A

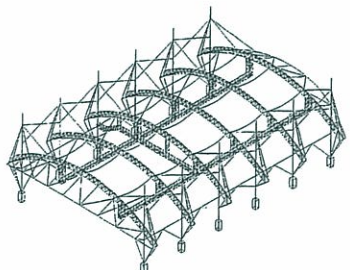
SECTION A1-A1

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Asraka U8/B4, Seksyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222

Project No: TPL 40581
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0

Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design



3D VIEW OF CATWALK WITH STEEL TRUSS

1.3 SCOPE OF DOCUMENT

This document details the structural analysis and design of the steel roof structure with the fabric roof cover when in placed and subject to applied loading.

For ease of this analysis, secondary structure like catwalk etc are not modeled in the design model. A separate design check is done.

The design of the foundation and RC stump to resist the forces from the roof structures is exclude in this document as it is not included in the roof contract.

Q326-Kuantan



	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/84, Sokayen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581	Page: 9
	Date: 26 June 2011		Doc No: Q326-KSP-CAL-001 Rev 0
Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design			

1.4 REFERENCE DOCUMENTS

Malaysia Standard MS 1553 : 2002 Code of Practice on Wind Loading For Building Structure

1.5 UNIT

The S.I system shall be used : ie mm, m, kN and etc

1.6 DESIGN CODE AND STANDARD

CP 3 : Chapter V-2 : 1993 Incorporating Amendment Nos. 1, 2, 3, 4 and 5 - Wind Loads

BS 6399 : Part 1 : 1996 - Code of practice for dead and imposed loads

BS 6399 : Part 3 : 1988 - Code of practice for imposed roof loads

BS 5950-1 : 2000 - Code of practice for design - Rolled and welded sections

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/84, Sokayen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581	Page: 10
	Date: 26 June 2011		Doc No: Q326-KSP-CAL-001 Rev 0
Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design			

2. ANALYSIS AND DESIGN CRITERIA

2.1 COORDINATES SYSTEM

The design model structural axis system is as follow:

- +X from grid line X6 to X1
- +Y from grid line Y2 to Y1
- +Z vertically up

2.2 METHOD OF ANALYSIS

The analysis of the tensioned membrane structure is done in two parts. Firstly is to do the form finding of the membrane. Then by using the forces from the static analysis of the prestressed membrane and applied to the steel structure and do a design check of the steel structure.

2.2.1) Fabric Roof

The task of determining appropriate forms of the membrane based on the given outline is using the software EASY from Germany.

The EASY form finding method is based on the method of force density algorithm. After the equilibrium shape is formed, the form is then applied with external load, ie imposed load, wind load and etc. and static analysis of the fabric is then carried out.

External load which will be applied to the surface of the membrane will be represented by nodal forces.

2.2.2) Structural Steel System

The output forces from the membrane for all the load case from EASY is then extract for use as input forces to the structural steel and then for design purposes.

The finite element software used for the steel analysis is STAAD PRO2007, developed by Research Engineers International, USA.

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/84, Sokayen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581	Page: 11
	Date: 26 June 2011		Doc No: Q326-KSP-CAL-001 Rev 0
Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design			

2.3 STRUCTURE STEEL DESIGN MODEL

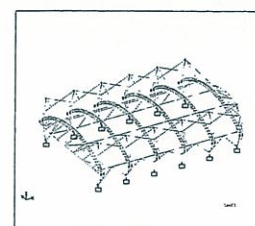
The steel structure has been modeled as a 3 dimensional frame model along the center line of the steel section. The ends of frame member are connected by nodes. All the steel member in this case uses all circular hollow section.

All the steel member are assumed to be frame type except the mast frontstay, backstay, ties between truss, bracings between column. These are assumed to be truss member which will have a bolted connection at both end.

The stabilizing cable between top of mast are assumed to be tension only Member with solid round bar representing the cables.

For ease of reference, the steel member of the design model has been group as follow;

- a) member 1 to 456 = bottom curved chord of 3D truss
- b) member 457 to 536 = edge member of eyelid canopy
- c) member 537 to 782 = bottom horizontal chord of 3D truss
- d) member 783 to 992 = top curved chord of 3D truss
- e) member 993 to 1928 = diagonal chord of 3D truss
- f) member 1929 to 1962 = bracing and prop member to eyelid canopy
- g) member 1963 to 1977 = tie member between 3D truss
- h) member 1978 to 2041 = lower, intermediate and upper mast
- i) member 2042 to 2061 = tie member at between lower masts
- j) member 2062 to 2077 = mast front stay
- k) member 2078 to 2193 = mast backstay
- l) member 2194 to 2227 = internal short tie of backstay
- m) member 2228 to 2255 = longitudinal bracing between lower mast
- n) member 2256 to 2275 = stabilizing cable at intermediate mast



3D VIEW

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/84, Sokayen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581	Page: 12
	Date: 26 June 2011		Doc No: Q326-KSP-CAL-001 Rev 0
Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design			

The following properties is used for the analysis on the steel member :-

- Young's Modulus = 2.10E08KN/m²
- Shear Modulus = 8.0E07 KN/ m²
- Poisson Ratio = 0.3
- Mass density of steel = 7850 kg/m³
- Gravitational acceleration = 9.81 m/s²
- Coefficient of thermal expansion = 11.7E-06 /deg C

2.4 STEEL MATERIAL

Generally the following steel material or equivalents is proposed;

Circular hollow section to BS EN 10210 S275 or equal
Plates to BS EN 10025 S275 or equal

The choice of material used will be subject to availability of material.

Therefore for the analysis and design of the structure steel roof, assumed yield stress of 275 N/mm².

2.5 DESIGN METHOD

For the in-placed analysis there will be 2 limit state analysis, service limit state and the ultimate limit state.

The service limit state relate to performance under normal service conditions, e.g deflections. And ultimate limit state are related to safety and load carrying capacity of the structure where the specified loads is multiplied by relevant partial factor.

The design facility available in STAADPRO software shall be used to code check the members for member forces and moment due to the various loading combinations for both limit states.

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/84, Sokayen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581	Page: 13
	Date: 26 June 2011		Doc No: Q326-KSP-CAL-001 Rev 0
Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design			

3. LOADING ASSUMPTION

The fabric roof and steel structure is subjected to the following loading:

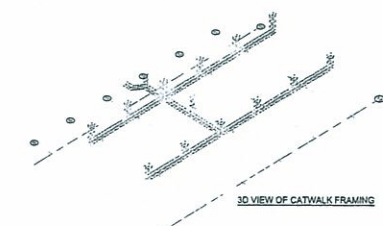
- Self weight of steel truss, column, bracing etc.
- Dead load of catwalk
- Prestress force in the membrane
- Imposed live load on membrane roof and catwalk
- Wind load

3.1 Self weight (SW).

Self weight of steel member = automatically calculated in the software
Self weight of fabric = 1.15 kg/ m²
(Insignificant so it is ignored in the membrane load)

3.2 Dead Load of catwalk (DCW)

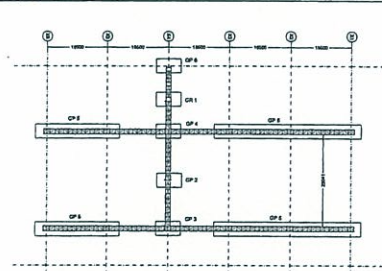
The catwalk is supported from the 3D truss at 15 Groups of generally 4 point from the bottom chord at 1.7m x 1.275m apart each except at gridline X4 where it is the main access.



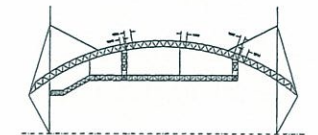
3D VIEW OF CATWALK FRAMING

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/84, Sokayen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581	Page: 14
	Date: 26 June 2011		Doc No: Q326-KSP-CAL-001 Rev 0
Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design			



PLAN - GROUP OF APPLIED LOAD FROM CATWALK



SECTION VIEW AT GRIDLINE X4

The weight of catwalk with expanded mesh + M&E load assumed to be 150 kg/m run

- Group 1 load per point = [(7.544+7.2)/2 x 150] / 2 = 553 kg (5.53 KN)
- Group 2 load per point = [(25/2) x 150] / 2 = 937 kg (9.4 KN)
- Group 3 load per point = [(16.5 + 6.25) x 150] / 4 = 853 kg (8.53 KN)
- Group 4 load per point = [(6.25 + 16.5 + 7.55/2) x 150] / 4 = 995 kg (9.95 KN)
- Group 5 load per point = (16.5x150) / 4 = 618 kg (6.2 KN)
- Group 6 load per point = [(7.544/2 + 3.3) x 150] / 2 = 530 kg (5.3 KN)

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/84, Sokayen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581	Page: 15
	Date: 26 June 2011		Doc No: Q326-KSP-CAL-001 Rev 0
Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design			

3.3 Prestress Load (PRE)

Prestress is induced to increase membrane stiffness and obtain a stable form which is in equilibrium. In this case, a prestress force of 3KN/m is assumed.

3.4 Imposed Live Load

3.4.1) Membrane roof (VL)

Imposed live load on membrane roof = 0.25 KN/m²
This load is applied vertically downward to the fabric roof.

3.4.2) Catwalk (LCW)

For localized catwalk design, assumed live load = 1.5 KN/m²

For global analysis of the structure roof, assumed live load applied simultaneously on all catwalk = 0.75 KN/m²

Using the same loading group as in the dead load case,
Live load = 0.75 KN/m² x 1.2m internal clearance of catwalk = 0.9 KN/m

- Group 1 load per point = [(7.544+7.2)/2 x 0.9] / 2 = 3.32 KN
- Group 2 load per point = [(25/2) x 0.9] / 2 = 5.62 KN
- Group 3 load per point = [(16.5 + 6.25) x 0.9] / 4 = 5.12 KN
- Group 4 load per point = [(6.25 + 16.5 + 7.55/2) x 0.9] / 4 = 5.96 KN
- Group 5 load per point = (16.5x0.9) / 4 = 3.71 KN
- Group 6 load per point = [(7.544/2 + 3.3) x 0.9] / 2 = 3.18 KN

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/84, Sokayen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581	Page: 16
	Date: 26 June 2011		Doc No: Q326-KSP-CAL-001 Rev 0
Project: Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design			

3.5 Wind Load

Reference to Malaysia Standard MS 1553 :2002 : Code of Practice on wind loading for Building Structure

As Kuantan fall in Zone II as shown in Figure 3.1, so basic wind speed of 32.5 m/s is adopted for the wind load calculation.

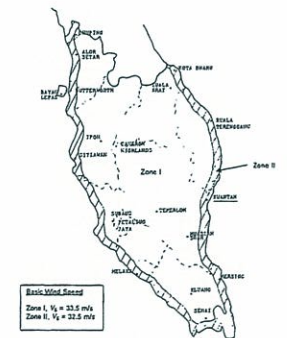


Figure 3.1 Peninsular Malaysia

Reference to CP3 : Chapter V : Part 2 1993 for dynamic wind pressure

Dynamic pressure due to wind is given by :

$$q = k V_s^2 \text{ N/m}^2$$

where $k = 0.613$
 $V_s = V_x S1xS2xS3$
Basic wind speed $V = 32.5 \text{ m/s}$

Q326-Kuantan



	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/B4, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page: 17
	Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		
	<p>S1 - topography factor = 1.0 S2 - ground roughness, structure size and height above ground factor</p> <p>Ground roughness = 3 Maximum height = 20 m Class = C Therefore S2 = 0.85</p> <p>S3 - statistical factor = 1.0</p> <p>$V_s = 32.5 \times 1.0 \times 0.85 \times 1.0 = 27.6 \text{ m/s}$ $q = 0.613 \times 27.6 \times 27.6 = 467 \text{ N/m}^2$ say 0.5 KN/m^2</p> <p>Assumed the fabric roof is dupitch canopy of roof angle approx = 20 deg</p> <p>Therefore from Table 13, Assumed the entrance and audience stand is 100% obstruct, Solidity ratio $\phi = 1$ (obstruct) Min Overall $C_p = -1.3$ and Max Overall $C_p = +0.6$</p> <p>3.5.1) Wind Uplift (WU) Wind uplift $W_u = -1.3 \times 0.5 = -0.65 \text{ KN/m}^2$</p> <p>3.5.2) Wind Pressure (WP) Wind pressure $W_p = +0.6 \times 0.5 = 0.3 \text{ KN/m}^2$</p>		

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/B4, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page: 18
	Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		
	<p>3.5.3) Wind from Entrance (WENT) Wind Perpendicular to Grid line Y2</p> <p>3.5.4) Audience stand (WAS) Wind Perpendicular to Grid line Y1</p> <p>3.5.5) Wind from Driving Pool Side when End bay is Wind Pressure (WDP_P) Wind Perpendicular to Grid line X6</p>		

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/B4, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page: 19
	Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		
	<p>3.5.6) Wind from Driving Pool Side when End bay is Wind Uplift (WDP_U) Wind Perpendicular to Grid line X6</p> <p>3.5.7) Wind from Score Board Side when End Bay is Wind Pressure (WSB_P) Wind Perpendicular to Grid line X1</p> <p>3.5.8) Wind from Score Board Side when End Bay is Wind Uplift (WSB_U) Wind Perpendicular to Grid line X1</p>		

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/B4, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page: 20
	Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		
	<p>4. BASIC LOAD CASES & LOAD COMBINATION</p> <p>The membrane roof and steel structure system are analyzed based on the following load cases and load combinations.</p> <p>4.1 BASIC LOAD CASES</p> <p>LOAD 1 (SW) = Self weight of steel structure automatically calculated by the software</p> <p>LOAD 2 (DCW) = Dead load of catwalk + ME load</p> <p>LOAD 3 (LCW) = Imposed Live Load on catwalk</p> <p>LOAD 4 (PRE) = Prestress load from membrane roof WITHOUT any external load</p> <p>The following external load is applied on to a stable and prestressed membrane form. So the following load case actually consist of prestressing load.</p> <p>LOAD 5 (VL) = Imposed Live Load on membrane roof</p> <p>LOAD 6 (WU) = Wind uplift on membrane roof</p> <p>LOAD 7 (WP) = Wind Pressure on membrane roof</p> <p>LOAD 8 (WENT) = Wind from Entrance side (Y2)</p> <p>LOAD 9 (WAS) = Wind from Audience Stand (Y1)</p> <p>LOAD 10 (WDP_P) = Wind from Driving Pool side (X6), End bay wind pressure</p> <p>LOAD 11 (WDP_U) = Wind from Driving Pool side (X6), End bay wind uplift</p> <p>LOAD 12 (WSB_P) = Wind from Score Board side (X1), End bay wind pressure</p> <p>LOAD 13 (WSB_U) = Wind from Score Board side (X1), End bay wind uplift</p> <p>All the above load case are unfactored load.</p>		

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/B4, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page: 21
	Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		
	<p>4.2 SERVICE LOAD COMBINATION</p> <p>LOAD 100 = SW + DCW + PRE LOAD 101 = SW + DCW + LCW + VL LOAD 102 = SW + DCW + WU LOAD 103 = SW + DCW + WP LOAD 104 = SW + DCW + WENT LOAD 105 = SW + DCW + WAS LOAD 106 = SW + DCW + WDP_P LOAD 107 = SW + DCW + WDP_U LOAD 108 = SW + DCW + WSB_P LOAD 109 = SW + DCW + WSB_U</p> <p>4.3 ULTIMATE LOAD COMBINATION</p> <p>LOAD 200 = 1.4(SW + DCW + PRE) LOAD 201 = 1.4(SW + DCW) + 1.6(LCW + VL) LOAD 202 = 1.0(SW + DCW) + 1.4WU LOAD 203 = 1.2(SW + DCW) + 1.2WP LOAD 204 = 1.2(SW + DCW) + 1.2(WENT) LOAD 205 = 1.2(SW + DCW) + 1.2(WAS) LOAD 206 = 1.2(SW + DCW) + 1.2(WDP_P) LOAD 207 = 1.0(SW + DCW) + 1.4(WDP_U) LOAD 208 = 1.2(SW + DCW) + 1.2(WSB_P) LOAD 209 = 1.0(SW + DCW) + 1.4(WSB_U)</p> <p>The design of the member sizes are based on the above load combination.</p>		

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/B4, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page: 22
	Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		
	<p>5. BOUNDARY CONDITION</p> <p>The steel structure is supported on top of 12 nos of RC stump at spacing of 16.5m x 54m to each other. The mast base supports are assumed to be fixed condition which restrained in X, Y direction horizontally and Z direction vertically and also restrained in the X, Y and Z moment.</p>		

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/B4, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page: 23
	Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		
	<p>6. DESIGN OF STEEL MEMBERS</p> <p>The design of the member size complied to BS5950 where the ultimate strength is used and the relevant load factor is applied to the imposed loading. For deciding the correct pipe size for every member, compression will be the deciding factor and the compression capacity depends on the slenderness ratio (l/r) and the tension capacity only depends on the sectional area.</p> <p>The final member size for individual member are determined from the worst force and moment from the ultimate load combination.</p> <p>The software is able to check the sizes assigned based on the output from the worst load combination. The member sizes layout is attached for reference. The member design output refers to Appendix.</p> <p>6.1 MEMBER SIZES LAYOUT</p> <p>DIAGONAL - 89B X 4 DIAGONAL - 114B X 4.5 TOP CURVED CHORD - 219B X 6 EDGE CHORD - 273B X 9.5 BOTTOM CURVED CHORD - 219B X 6 HORIZONTAL BOTTOM - 89B X 4 HORIZONTAL BOTTOM & DIAGONAL - 139B X 6 HORIZONTAL BOTTOM - 139B X 8</p>		

Q326-Kuantan

	Sediabona Sdn. Bhd. No. 11 Jalan Astaka U8/B4, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL-40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page: 24
	Project : Upgrading of Aquatic Center Wisma Belia Indera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		
	<p>DIAGONAL - 89B X 4 DIAGONAL - 114B X 4.5 TOP CURVED CHORD - 219B X 6 EDGE CHORD - 273B X 9.5 EDGE BRACE - 168.3B X 6 EDGE DIAGONAL BRACE - 168.3B X 10</p>		

Q326-Kuantan



Sedibana Sdn. Bhd.
No. 11 Jalan Astaka U8/B4, Sekyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222
Project No: TPL 40581 Page: 25
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0
Project : Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

EDGE DIAGONAL BRACE - 168.3Ø X 8 TIE BTW 3D TRUSS - 273Ø X 8

LOWER MAST - 609Ø X 16 INTERMEDIATE MAST - 406.4Ø X 12.5

MAST FRONT STAY - 219Ø X 9 MAST BACKSTAY - 168Ø X 6

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Astaka U8/B4, Sekyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222
Project No: TPL 40581 Page: 26
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0
Project : Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

TIE BETWEEN MAST BACKSTAY - 73Ø X 5 LONGITUDINAL BRACE - 215Ø X 6

LONGITUDINAL BRACE - 219Ø X 9 LONGITUDINAL TIE - 273Ø X 9

SAFETY CABLE BETWEEN MAST - 16Ø

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Astaka U8/B4, Sekyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222
Project No: TPL 40581 Page: 27
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0
Project : Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

7. DESIGN OF CABLES

7.1 STABILIZING CABLE AT TOP OF MAST

From the steel structure analysis output,
maximum axial force = 30 KN

Proposed to use 16mm Φ 1x19 galvanized steel wire rope

Min breaking load = 211 KN >>> 30 KN

Therefore is ok to use 16mm Φ wire rope.

7.2 MEMBRANE BORDER CABLE

From the membrane static output for the internal panel,
Prestress load case , cable force = 47 KN
Imposed live load, cable force = 20 KN
Wind uplift case , cable force = 250 KN
Wind pressure case , cable force = 35 KN
Wind from Entrance (one side uplift & one side pressure) = 184 KN
Wind from grandstand (one side pressure & one side uplift) = 184 KN

maximum unfactored tension force in the border cable = 250 KN from WU

Proposed to use 28mm Φ 6 x 37 IWRC galvanized steel wire rope,
Min breaking load = 49600 kg = 506 KN
Safety factor = 506 / 250 = 2.024

Therefore is ok to use 28mm Φ wire rope.

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Astaka U8/B4, Sekyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222
Project No: TPL 40581 Page: 28
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0
Project : Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

8. DESIGN OF HOLDING DOWN BOLTS

Reaction summary extracted from analysis output as shown,

	Node	UX	UY	UZ	Mx (kNm)	My (kNm)	Mz (kNm)
Max FX	808	208.12500000000000	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000
Min FX	792	-208.12500000000000	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000
Max FY	792	0.00000000000000	208.12500000000000	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000
Min FY	808	0.00000000000000	-208.12500000000000	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000
Max FZ	792	0.00000000000000	0.00000000000000	208.12500000000000	0.00000000000000	0.00000000000000	0.00000000000000
Min FZ	776	0.00000000000000	0.00000000000000	-208.12500000000000	0.00000000000000	0.00000000000000	0.00000000000000
Max MX	792	0.00000000000000	0.00000000000000	0.00000000000000	134.244	88.432	329.248
Min MX	792	0.00000000000000	0.00000000000000	0.00000000000000	-134.244	-88.432	-329.248
Max MY	808	0.00000000000000	0.00000000000000	0.00000000000000	-88.432	134.244	329.248
Min MY	808	0.00000000000000	0.00000000000000	0.00000000000000	88.432	-134.244	-329.248
Max MZ	808	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000	329.248
Min MZ	808	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000	0.00000000000000	-329.248

From the reaction forces summary output, max reaction forces are;

$F_x = 233 / -233$ KN $M_x = 530 / -774$ KNm
 $F_y = 229 / -229$ KN $M_y = 279 / -279$ KNm
 $F_z = 567 / -334$ KN $M_z = 125 / -125$ KNm

Note : +ve Fz is the compression and -ve Fz is the tensile force

Proposed 20 x M30 grade 8.8 in a circular arrangement at 1m diameter, and assumed only 4 bolts on each side at 0.89m apart are resisting;

BASE PLATE DETAIL - TYPE G1

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Astaka U8/B4, Sekyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222
Project No: TPL 40581 Page: 29
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0
Project : Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

SECTION G1a-G1b

Ft due to Mx per bolt = 774 / (4x0.89) = 217.4 KN
Direct Ft per bolt = 334 / 20 = 16.7 KN
Total tensile per bolt Ft = 217.4 + 16.7 = 234.1 KN

Fs due to Mz per bolt = 125 / (4x0.89) = 35.1 KN
Direct Fs per bolt = (233² + 229²)ᵃ / 20 = 16.3 KN
Total Fs per bolt = 35.1 + 16.3 = 51.4 KN

Tensile strength of Grade 8.8 bolt = 450 N/mm²
Shear strength of Grade 8.8 bolt = 375 N/mm²

ft = 234.1x10e3 / 561 = 417 N/mm² < 450 N/mm² OK
fs = 51.4x10e3 / 561 = 92 N/mm² < 375 N/mm² OK

Combined stress check,
417/450 + 92/375 = 1.172 < 1.4 OK

Embedment length check,
fbu = $\beta (f_{cu})^n$

Where fbu = design ultimate anchorage bond stress
 β = 0.28 for plain bar
fcu = 35 N/mm² for concrete grade

fbu = 0.28 (35)ᵃ = 1.656

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Astaka U8/B4, Sekyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222
Project No: TPL 40581 Page: 30
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0
Project : Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

anchorage force / ($\pi \times \Phi \times L$) = fbu

embedment length L = anchorage force / ($\pi \times \Phi \times f_{bu}$)
= 234.1x10e3 / ($\pi \times 30 \times 1.656$)
= 1500 mm

Therefore provide minimum 1500mm embedment length is OK.

Base plate thickness check

Assumed the plate is bend in double curvature over the width of 590mm for 4 bolts and ignored the 16mm and 20mm thk stiffener plate,
M = 234.1 x (1.0 - 0.609)/2 x 1/2 = 22.88 KNm
Z_{provide} = 1/6 x 590 x 30² = 88500 mm³
fb = 22.88x10e6 / 88500 = 258 N/mm² < 275 N/mm² OK
Therefore use 30mm thk base plate with stiffener plate is OK.

TYPICAL HOLDING DOWN BOLT DETAIL

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Astaka U8/B4, Sekyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222
Project No: TPL 40581 Page: 31
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0
Project : Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

9. DESIGN OF PIN CONNECTIONS

9.1 MAST FRONT HANGER

Max axial force as extracted from analysis output = 217 KN

PROPOSED TO USE 1 x M48 GRADE 8.8 BOLT WITH 16mm THICK TONGUE PLATE,

Tensile strength of Grade 8.8 bolt = 450 N/mm²
Shear strength of Grade 8.8 bolt = 375 N/mm²

fs = [(217/2)x1e3] / 1470 = 74 N/mm² < 375 N/mm² OK
bearing stress of tongue plate, fbs = [(217/2)x1e3] / (48x16)
= 141 N/mm² < 460 N/mm² OK
Where 460 N/mm² is the bearing strength for S275 plate.

9.2 TIE BETWEEN 3D TRUSS

Max axial force as extracted from analysis output = 323 KN

PROPOSED TO USE 1 x M36 GRADE 8.8 BOLT WITH 12mm THICK TONGUE PLATE,

Tensile strength of Grade 8.8 bolt = 450 N/mm²
Shear strength of Grade 8.8 bolt = 375 N/mm²

fs = [(365/2)x10e3] / 817 = 224 N/mm² < 375 N/mm² OK
bearing stress of tongue plate, fbs = [(365/2)x1e3] / (26x12)
= 422 N/mm² < 460 N/mm² OK
Where 460 N/mm² is the bearing strength for S275 plate.

Q326-Kuantan

Sedibana Sdn. Bhd.
No. 11 Jalan Astaka U8/B4, Sekyen U8
Bukit Jelutong 40150 Shah Alam
Tel: (603)7847 3333 Fax: (603)7847 2222
Project No: TPL 40581 Page: 32
Date: 26 June 2011
Doc No: Q326-KSP-CAL-001 Rev 0
Project : Upgrading of Aquatic Center Wisma Bella Indera Mahkota, Kuantan
Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design

Proposed to use 1 x M48 grade 8.8 bolt with 16mm thick tongue plate,

Tensile strength of Grade 8.8 bolt = 450 N/mm²
Shear strength of Grade 8.8 bolt = 375 N/mm²

fs = [(323/2)x1e3] / 1470 = 110 N/mm² < 375 N/mm² OK
bearing stress of tongue plate, fbs = [(323/2)x1e3] / (48x16)
= 210 N/mm² < 460 N/mm² OK
Where 460 N/mm² is the bearing strength for S275 plate.

9.3 BRACE AT LOWER MAST

Max axial force as extracted from analysis output = 365 KN

PROPOSED TO USE 1 x M36 GRADE 8.8 BOLT WITH 12mm THICK TONGUE PLATE,

Tensile strength of Grade 8.8 bolt = 450 N/mm²
Shear strength of Grade 8.8 bolt = 375 N/mm²

fs = [(365/2)x10e3] / 817 = 224 N/mm² < 375 N/mm² OK
bearing stress of tongue plate, fbs = [(365/2)x1e3] / (26x12)
= 422 N/mm² < 460 N/mm² OK
Where 460 N/mm² is the bearing strength for S275 plate.

Q326-Kuantan



Q326-KSP-R4b-Deg.std

Table with 4 columns of numerical data, likely representing material properties or test results for Q326-KSP-R4b-Deg.std.

Page: 8

Q326-KSP-R4b-Deg.std

Table with 4 columns of numerical data, likely representing material properties or test results for Q326-KSP-R4b-Deg.std.

Page: 9

Q326-KSP-R4b-Deg.std

Table with 4 columns of numerical data, likely representing material properties or test results for Q326-KSP-R4b-Deg.std.

Page: 14

Q326-KSP-R4b-Deg.std

Table with 4 columns of numerical data, likely representing material properties or test results for Q326-KSP-R4b-Deg.std.

Page: 15

Q326-KSP-R4b-Deg.std

Table with 4 columns of numerical data, likely representing material properties or test results for Q326-KSP-R4b-Deg.std.

Page: 12

Q326-KSP-R4b-Deg.std

Table with 4 columns of numerical data, likely representing material properties or test results for Q326-KSP-R4b-Deg.std.

Page: 13

Q326-KSP-R4b-Deg.std

Table with 4 columns of numerical data, likely representing material properties or test results for Q326-KSP-R4b-Deg.std.

Page: 14

Q326-KSP-R4b-Deg.std

Table with 4 columns of numerical data, likely representing material properties or test results for Q326-KSP-R4b-Deg.std.

Page: 15

Q326-KSP-R4b-Deg.std 016

534	FX	5.26	FY	0	FZ	-2.02
535	FX	4.98	FY	-1.53	FZ	2.4
536	FX	5.23	FY	0	FZ	2.4
537	FX	4.81	FY	-2.36	FZ	2.8
538	FX	4.8	FY	-2.36	FZ	3.12
539	FX	4.44	FY	-1.64	FZ	2.84
540	FX	5.03	FY	-1.37	FZ	2.99
541	FX	3.6	FY	-1.33	FZ	2.5
542	FX	4.2	FY	-1.89	FZ	3.62
543	FX	3.59	FY	-2.34	FZ	3.87
***R4-IN7-2						
118	FX	-40.85	FY	21.9	FZ	15.03
119	FX	-40.85	FY	-21.9	FZ	15.03
120	FX	40.85	FY	21.9	FZ	15.52
121	FX	40.85	FY	-21.9	FZ	15.52
122	FX	-4.5	FY	0.05	FZ	-0.76
123	FX	-4.3	FY	0.03	FZ	-0.72
124	FX	-4.63	FY	0.03	FZ	-0.82
125	FX	-4.88	FY	0.01	FZ	-0.88
126	FX	-5.31	FY	0.01	FZ	-0.96
127	FX	-4.96	FY	0	FZ	-0.87
128	FX	-5.07	FY	0.01	FZ	-0.87
129	FX	-5.42	FY	0.01	FZ	-0.92
130	FX	-5.35	FY	0	FZ	-0.88
131	FX	-5.27	FY	0	FZ	-0.85
132	FX	-5.33	FY	0	FZ	-0.84
133	FX	-5.37	FY	0	FZ	-0.84
134	FX	-5.65	FY	0.01	FZ	-0.92
135	FX	-5.46	FY	-0.01	FZ	-0.88
136	FX	-5.43	FY	0.01	FZ	-0.82
137	FX	-5.43	FY	0	FZ	-0.85
138	FX	-5.43	FY	-0.01	FZ	-0.82
139	FX	-5.46	FY	0.01	FZ	-0.82
140	FX	-5.65	FY	-0.01	FZ	-0.92
141	FX	-5.37	FY	0	FZ	-0.84
142	FX	-5.33	FY	0	FZ	-0.84
143	FX	-5.27	FY	0	FZ	-0.85
144	FX	-5.35	FY	0	FZ	-0.88
145	FX	-5.42	FY	0.01	FZ	-0.92
146	FX	-5.07	FY	-0.01	FZ	-0.87
147	FX	-4.96	FY	0	FZ	-0.87
148	FX	-5.31	FY	-0.01	FZ	-0.96
149	FX	-4.88	FY	-0.01	FZ	-0.88
150	FX	-4.63	FY	-0.03	FZ	-0.82
151	FX	-5.2	FY	-0.02	FZ	-0.94
152	FX	-4.3	FY	-0.03	FZ	-0.72
153	FX	-4.85	FY	-0.05	FZ	-0.76
154	FX	-4.12	FY	-0.05	FZ	-0.52
155	FX	-4.65	FY	-0.08	FZ	-0.44
156	FX	4.66	FY	0.08	FZ	-0.44
42	FX	4.11	FY	0.06	FZ	-0.55
43	FX	4.85	FY	0.05	FZ	-0.8
44	FX	4.3	FY	0.03	FZ	-0.74
45	FX	5.2	FY	0.02	FZ	-0.97
46	FX	4.63	FY	0.03	FZ	-0.85
47	FX	4.88	FY	0.01	FZ	-0.9
48	FX	5.32	FY	0.01	FZ	-0.99
49	FX	4.96	FY	0	FZ	-0.88
50	FX	5.07	FY	0.01	FZ	-0.89
51	FX	5.42	FY	0.01	FZ	-0.94
52	FX	5.35	FY	0	FZ	-0.87
53	FX	5.27	FY	0	FZ	-0.87
54	FX	5.32	FY	0	FZ	-0.86
55	FX	5.2	FY	-0.01	FZ	-0.86
56	FX	5.65	FY	0.01	FZ	-0.9
57	FX	5.46	FY	-0.01	FZ	-0.85
58	FX	5.43	FY	0.01	FZ	-0.84
59	FX	5.43	FY	0	FZ	-0.84
60	FX	5.43	FY	0.01	FZ	-0.84
61	FX	5.46	FY	0.01	FZ	-0.85
62	FX	5.65	FY	-0.01	FZ	-0.9
63	FX	5.37	FY	0	FZ	-0.86

Page: 16

Q326-KSP-R4b-Deg.std 017

64	FX	5.32	FY	0	FZ	-0.86
65	FX	5.27	FY	0	FZ	-0.87
66	FX	5.35	FY	0	FZ	-0.86
67	FX	5.42	FY	0.01	FZ	-0.94
68	FX	5.07	FY	-0.01	FZ	-0.89
69	FX	4.96	FY	0	FZ	-0.88
70	FX	5.32	FY	-0.01	FZ	-0.99
71	FX	4.88	FY	-0.01	FZ	-0.9
72	FX	4.63	FY	-0.03	FZ	-0.85
73	FX	5.2	FY	-0.02	FZ	-0.97
74	FX	4.3	FY	-0.03	FZ	-0.74
75	FX	4.85	FY	-0.05	FZ	-0.8
76	FX	4.11	FY	-0.06	FZ	-0.55
77	FX	4.66	FY	-0.08	FZ	-0.48
***R4-IN7-2						
136	FX	-40.85	FY	21.9	FZ	15.03
137	FX	-40.85	FY	-21.9	FZ	15.03
138	FX	40.85	FY	21.9	FZ	15.52
139	FX	40.85	FY	-21.9	FZ	15.52
140	FX	-4.5	FY	0.05	FZ	-0.76
141	FX	-4.3	FY	0.03	FZ	-0.72
142	FX	-4.63	FY	0.03	FZ	-0.82
143	FX	-4.88	FY	0.01	FZ	-0.88
144	FX	-5.31	FY	0.01	FZ	-0.96
145	FX	-4.96	FY	0	FZ	-0.87
146	FX	-5.07	FY	0.01	FZ	-0.87
147	FX	-5.42	FY	0.01	FZ	-0.92
148	FX	-5.35	FY	0	FZ	-0.88
149	FX	-5.27	FY	0	FZ	-0.85
150	FX	-5.33	FY	0	FZ	-0.84
151	FX	-5.37	FY	0	FZ	-0.84
152	FX	-5.65	FY	0.01	FZ	-0.92
153	FX	-5.46	FY	-0.01	FZ	-0.88
154	FX	-5.43	FY	0.01	FZ	-0.82
155	FX	-5.43	FY	0	FZ	-0.85
156	FX	-5.43	FY	-0.01	FZ	-0.82
157	FX	-5.46	FY	0.01	FZ	-0.82
158	FX	-5.65	FY	-0.01	FZ	-0.92
159	FX	-5.37	FY	0	FZ	-0.84
160	FX	-5.33	FY	0	FZ	-0.84
161	FX	-5.27	FY	0	FZ	-0.85
162	FX	-5.35	FY	0	FZ	-0.88
163	FX	-5.42	FY	0.01	FZ	-0.92
164	FX	-5.07	FY	-0.01	FZ	-0.87
165	FX	-4.96	FY	0	FZ	-0.87
166	FX	-5.31	FY	-0.01	FZ	-0.96
167	FX	-5.33	FY	0	FZ	-0.84
168	FX	-5.37	FY	0	FZ	-0.84
169	FX	-5.65	FY	0.01	FZ	-0.92
170	FX	-5.46	FY	-0.01	FZ	-0.88
171	FX	-5.43	FY	0.01	FZ	-0.82
172	FX	-5.43	FY	0	FZ	-0.85
173	FX	-5.43	FY	-0.01	FZ	-0.82
174	FX	-5.46	FY	0.01	FZ	-0.82
175	FX	-5.65	FY	-0.01	FZ	-0.92
176	FX	-5.37	FY	0	FZ	-0.84
177	FX	-5.33	FY	0	FZ	-0.84
178	FX	-5.27	FY	0	FZ	-0.85
179	FX	-5.35	FY	0	FZ	-0.88
180	FX	-5.42	FY	0.01	FZ	-0.92
181	FX	-5.07	FY	-0.01	FZ	-0.87
182	FX	-4.96	FY	0	FZ	-0.87
183	FX	-5.31	FY	-0.01	FZ	-0.96
184	FX	-5.33	FY	0	FZ	-0.84
185	FX	-5.37	FY	0	FZ	-0.84
186	FX	-5.65	FY	0.01	FZ	-0.92
187	FX	-5.46	FY	-0.01	FZ	-0.88
188	FX	-5.43	FY	0.01	FZ	-0.82
189	FX	-5.43	FY	0	FZ	-0.85
190	FX	-5.43	FY	-0.01	FZ	-0.82
191	FX	-5.46	FY	0.01	FZ	-0.82
192	FX	-5.65	FY	-0.01	FZ	-0.92
193	FX	-5.37	FY	0	FZ	-0.84
194	FX	-5.33	FY	0	FZ	-0.84
195	FX	-5.27	FY	0	FZ	-0.85
196	FX	-5.35	FY	0	FZ	-0.88
197	FX	-5.42	FY	0.01	FZ	-0.92
198	FX	-5.07	FY	-0.01	FZ	-0.87
199	FX	-4.96	FY	0	FZ	-0.87
200	FX	-5.31	FY	-0.01	FZ	-0.96
201	FX	-5.33	FY	0	FZ	-0.84
202	FX	-5.37	FY	0	FZ	-0.84
203	FX	-5.65	FY	0.01	FZ	-0.92
204	FX	-5.46	FY	-0.01	FZ	-0.88
205	FX	-5.43	FY	0.01	FZ	-0.82
206	FX	-5.43	FY	0	FZ	-0.85
207	FX	-5.43	FY	-0.01	FZ	-0.82
208	FX	-5.46	FY	0.01	FZ	-0.82
209	FX	-5.65	FY	-0.01	FZ	-0.92
210	FX	-5.37	FY	0	FZ	-0.84
211	FX	-5.33	FY	0	FZ	-0.84
212	FX	-5.27	FY	0	FZ	-0.85
213	FX	-5.35	FY	0	FZ	-0.88
214	FX	-5.42	FY	0.01	FZ	-0.92
215	FX	-5.07	FY	-0.01	FZ	-0.87
216	FX	-4.96	FY	0	FZ	-0.87
217	FX	-5.31	FY	-0.01	FZ	-0.96
218	FX	-5.33	FY	0	FZ	-0.84
219	FX	-5.37	FY	0	FZ	-0.84
220	FX	-5.65	FY	0.01	FZ	-0.92
221	FX	-5.46	FY	-0.01	FZ	-0.88
222	FX	-5.43	FY	0.01	FZ	-0.82
223	FX	-5.43	FY	0	FZ	-0.85
224	FX	-5.43	FY	-0.01	FZ	-0.82
225	FX	-5.46	FY	0.01	FZ	-0.82
226	FX	-5.65	FY	-0.01	FZ	-0.92
227	FX	-5.37	FY	0	FZ	-0.84
228	FX	-5.33	FY	0	FZ	-0.84
229	FX	-5.27	FY	0	FZ	-0.85
230	FX	-5.35	FY	0	FZ	-0.88
231	FX	-5.42	FY	0.01	FZ	-0.92
232	FX	-5.07	FY	-0.01	FZ	-0.87
233	FX	-4.96	FY	0	FZ	-0.87
234	FX	-5.31	FY	-0.01	FZ	-0.96
235	FX	-5.33	FY	0	FZ	-0.84
236	FX	-5.37	FY	0	FZ	-0.84
237	FX	-5.65	FY	0.01	FZ	-0.92
238	FX	-5.46	FY	-0.01	FZ	-0.88
239	FX	-5.43	FY	0.01	FZ	-0.82
240	FX	-5.43	FY	0	FZ	-0.85
241	FX	-5.43	FY	-0.01	FZ	-0.82
242	FX	-5.46	FY	0.01	FZ	-0.82
243	FX	-5.65	FY	-0.01	FZ	-0.92
244	FX	-5.37	FY	0	FZ	-0.84
245	FX	-5.33	FY	0	FZ	-0.84
246	FX	-5.27	FY	0	FZ	-0.85
247	FX	-5.35	FY	0	FZ	-0.88
248	FX	-5.42	FY	0.01	FZ	-0.92
249	FX	-5.07	FY	-0.01	FZ	-0.87
250	FX	-4.96	FY	0	FZ	-0.87
251	FX	-5.31	FY	-0.01	FZ	-0.96
252	FX	-5.33	FY	0	FZ	-0.84
253	FX	-5.37	FY	0	FZ	-0.84
254	FX	-5.65	FY	0.01	FZ	-0.92
255	FX	-5.46	FY	-0.01	FZ	-0.88
256	FX	-5.43	FY	0.01	FZ	-0.82
257	FX	-5.43	FY	0	FZ	-0.85
258	FX	-5.43	FY	-0.01	FZ	-0.82
259	FX	-5.46	FY	0.01	FZ	-0.82
260	FX	-5.65	FY	-0.01	FZ	-0.92
261	FX	-5.37	FY	0	FZ	-0.84
262	FX	-5.33	FY	0	FZ	-0.84
263	FX	-5.27	FY	0	FZ	-0.85
264	FX	-5.35	FY	0	FZ	-0.88
265	FX	-5.42	FY	0.01	FZ	-0.9

Q326-KSP-Rtb-Deg.std

148 FX -16.44 FY -0.22 FZ -3.69
149 FX -15.04 FY -0.23 FZ -3.16
150 FX -14.33 FY -0.27 FZ -3.15
151 FX -16.26 FY -0.33 FZ -3.53
152 FX -13.69 FY -0.36 FZ -2.81
153 FX -15.49 FY -0.5 FZ -3
154 FX -12.23 FY -0.51 FZ -2.08
155 FX -8.44 FY -0.41 FZ -1.29
41 FX 8.39 FY 0.4 FZ -1.34
42 FX 12.22 FY 0.5 FZ -2.12
43 FX 15.48 FY 0.47 FZ -3.06
44 FX 13.69 FY 0.35 FZ -2.04
45 FX 16.26 FY 0.32 FZ -3.58
46 FX 14.33 FY 0.26 FZ -3.18
47 FX 15.86 FY 0.17 FZ -3.55
48 FX 16.43 FY 0.21 FZ -3.73
49 FX 15.42 FY 0.18 FZ -3.47
50 FX 15.86 FY 0.17 FZ -3.55
51 FX 17.11 FY 0.16 FZ -3.82
52 FX 17.03 FY 0.13 FZ -3.77
53 FX 16.9 FY 0.12 FZ -3.7
54 FX 17.18 FY 0.1 FZ -3.74
55 FX 17.42 FY 0.08 FZ -3.78
56 FX 18.43 FY 0.02 FZ -3.99
57 FX 17.86 FY 0.04 FZ -3.85
58 FX 17.79 FY 0.02 FZ -3.82
59 FX 17.82 FY 0 FZ -3.83
60 FX 17.79 FY -0.02 FZ -3.82
61 FX 17.86 FY -0.04 FZ -3.85
62 FX 18.42 FY -0.07 FZ -3.99
63 FX 17.42 FY -0.08 FZ -3.78
64 FX 17.18 FY -0.1 FZ -3.74
65 FX 16.9 FY -0.12 FZ -3.7
66 FX 17.03 FY -0.13 FZ -3.77
67 FX 17.11 FY -0.16 FZ -3.82
68 FX 15.86 FY -0.17 FZ -3.55
69 FX 15.42 FY -0.18 FZ -3.47
70 FX 16.44 FY -0.21 FZ -3.73
71 FX 15.04 FY -0.23 FZ -3.39
72 FX 14.33 FY -0.26 FZ -3.18
73 FX 16.26 FY -0.32 FZ -3.58
74 FX 13.69 FY -0.35 FZ -2.84
75 FX 15.49 FY -0.48 FZ -3.06
76 FX 12.22 FY -0.49 FZ -2.12
77 FX 8.44 FY -0.39 FZ -1.32

Page: 24

Q326-KSP-Rtb-Deg.std

444 FX -17.18 FY 0.1 FZ -3.72
445 FX -17.42 FY 0.09 FZ -3.75
446 FX -16.43 FY 0.07 FZ -3.86
447 FX -17.86 FY 0.04 FZ -3.83
448 FX -17.79 FY 0.02 FZ -3.8
449 FX -17.82 FY 0 FZ -3.8
450 FX -17.79 FY -0.02 FZ -3.8
451 FX -17.86 FY -0.04 FZ -3.82
452 FX -18.42 FY -0.07 FZ -3.97
453 FX -17.42 FY -0.08 FZ -3.78
454 FX -17.18 FY -0.1 FZ -3.72
455 FX -16.9 FY -0.12 FZ -3.68
456 FX -17.03 FY -0.13 FZ -3.74
457 FX -17.11 FY -0.16 FZ -3.79
458 FX -15.86 FY -0.17 FZ -3.55
459 FX -15.42 FY -0.18 FZ -3.47
460 FX -16.44 FY -0.21 FZ -3.73
461 FX -15.04 FY -0.23 FZ -3.39
462 FX -14.33 FY -0.26 FZ -3.18
463 FX -16.26 FY -0.32 FZ -3.58
464 FX -13.69 FY -0.35 FZ -2.84
465 FX -15.49 FY -0.48 FZ -3.06
466 FX -12.22 FY -0.49 FZ -2.12
467 FX 8.44 FY -0.39 FZ -1.32
316 FX 12.22 FY 0.5 FZ -2.12
317 FX 15.48 FY 0.47 FZ -3.06
318 FX 16.26 FY 0.32 FZ -3.58
319 FX 14.33 FY 0.26 FZ -3.18
320 FX 15.86 FY 0.17 FZ -3.55
321 FX 16.43 FY 0.21 FZ -3.73
322 FX 15.42 FY 0.18 FZ -3.47
323 FX 15.86 FY 0.17 FZ -3.55
324 FX 17.11 FY 0.16 FZ -3.82
325 FX 17.03 FY 0.13 FZ -3.77
326 FX 16.9 FY 0.12 FZ -3.7
327 FX 17.18 FY 0.1 FZ -3.74
328 FX 17.42 FY 0.08 FZ -3.78
329 FX 18.43 FY 0.02 FZ -3.99
330 FX 17.86 FY 0.04 FZ -3.85
331 FX 17.79 FY 0.02 FZ -3.82
332 FX 17.82 FY 0 FZ -3.83
333 FX 17.79 FY -0.02 FZ -3.82
334 FX 17.86 FY -0.04 FZ -3.85
335 FX 18.42 FY -0.07 FZ -3.99
336 FX 17.42 FY -0.08 FZ -3.78
337 FX 17.18 FY -0.1 FZ -3.74
338 FX 16.9 FY -0.12 FZ -3.7
339 FX 17.03 FY -0.13 FZ -3.77
340 FX 17.11 FY -0.16 FZ -3.82
341 FX 15.86 FY -0.17 FZ -3.55
342 FX 15.42 FY -0.18 FZ -3.47
343 FX 16.44 FY -0.21 FZ -3.73
344 FX 15.04 FY -0.23 FZ -3.39
345 FX 14.33 FY -0.26 FZ -3.18
346 FX 16.26 FY -0.32 FZ -3.58
347 FX 13.69 FY -0.35 FZ -2.84
348 FX 15.49 FY -0.48 FZ -3.06
349 FX 12.22 FY -0.49 FZ -2.12
350 FX 8.44 FY -0.39 FZ -1.32

Page: 28

A24

Q326-KSP-Rtb-Deg.std

222 FX -17.03 FY -0.13 FZ -3.74
223 FX -17.11 FY -0.16 FZ -3.79
224 FX -15.86 FY -0.17 FZ -3.52
225 FX -15.42 FY -0.18 FZ -3.47
226 FX -16.44 FY -0.22 FZ -3.69
227 FX -15.04 FY -0.23 FZ -3.36
228 FX -14.33 FY -0.26 FZ -3.18
229 FX -16.26 FY -0.32 FZ -3.53
230 FX -13.69 FY -0.36 FZ -2.81
231 FX -15.49 FY -0.5 FZ -3
232 FX -12.23 FY -0.51 FZ -2.08
233 FX -8.44 FY -0.41 FZ -1.29
80 FX 8.39 FY 0.4 FZ -1.34
81 FX 12.22 FY 0.5 FZ -2.12
82 FX 15.48 FY 0.47 FZ -3.06
83 FX 13.69 FY 0.35 FZ -2.84
84 FX 16.26 FY 0.32 FZ -3.58
85 FX 14.33 FY 0.26 FZ -3.18
86 FX 15.04 FY 0.23 FZ -3.38
87 FX 16.43 FY 0.21 FZ -3.73
88 FX 17.79 FY 0.16 FZ -3.82
89 FX 15.86 FY 0.17 FZ -3.55
90 FX 17.11 FY 0.16 FZ -3.82
91 FX 17.03 FY 0.13 FZ -3.77
92 FX 16.9 FY 0.12 FZ -3.7
93 FX 17.18 FY 0.1 FZ -3.74
94 FX 17.42 FY 0.08 FZ -3.78
95 FX 18.43 FY 0.02 FZ -3.99
96 FX 17.86 FY 0.04 FZ -3.85
97 FX 17.79 FY 0.02 FZ -3.82
98 FX 17.82 FY 0 FZ -3.83
99 FX 17.79 FY -0.02 FZ -3.82
100 FX 17.86 FY -0.04 FZ -3.85
101 FX 18.42 FY -0.07 FZ -3.99
102 FX 17.42 FY -0.08 FZ -3.78
103 FX 17.18 FY -0.1 FZ -3.74
104 FX 16.9 FY -0.12 FZ -3.7
105 FX 17.03 FY -0.13 FZ -3.77
106 FX 17.11 FY -0.16 FZ -3.82
107 FX 17.18 FY -0.18 FZ -3.86
108 FX 15.42 FY -0.18 FZ -3.47
109 FX 16.44 FY -0.21 FZ -3.73
110 FX 15.04 FY -0.23 FZ -3.39
111 FX 14.33 FY -0.26 FZ -3.18
112 FX 16.26 FY -0.32 FZ -3.58
113 FX 13.69 FY -0.35 FZ -2.84
114 FX 15.49 FY -0.48 FZ -3.06
115 FX 12.22 FY -0.49 FZ -2.12
116 FX 8.44 FY -0.39 FZ -1.32

Page: 25

A25

Q326-KSP-Rtb-Deg.std

296 FX -18.42 FY -0.07 FZ -3.87
297 FX -17.42 FY -0.09 FZ -3.75
298 FX -17.18 FY -0.1 FZ -3.72
299 FX -16.9 FY -0.12 FZ -3.68
300 FX -17.03 FY -0.13 FZ -3.74
301 FX -17.11 FY -0.16 FZ -3.79
302 FX -15.86 FY -0.17 FZ -3.52
303 FX -15.42 FY -0.18 FZ -3.44
304 FX -16.44 FY -0.22 FZ -3.69
305 FX -15.04 FY -0.23 FZ -3.36
306 FX -14.33 FY -0.26 FZ -3.18
307 FX -16.26 FY -0.32 FZ -3.53
308 FX -13.69 FY -0.36 FZ -2.81
309 FX -15.49 FY -0.5 FZ -3
310 FX -12.23 FY -0.51 FZ -2.08
311 FX -8.44 FY -0.41 FZ -1.29
158 FX 8.39 FY 0.4 FZ -1.34
159 FX 12.22 FY 0.5 FZ -2.12
160 FX 15.48 FY 0.47 FZ -3.06
161 FX 13.69 FY 0.35 FZ -2.84
162 FX 16.26 FY 0.32 FZ -3.58
163 FX 14.33 FY 0.26 FZ -3.18
164 FX 15.04 FY 0.23 FZ -3.38
165 FX 16.43 FY 0.21 FZ -3.73
166 FX 15.42 FY 0.18 FZ -3.47
167 FX 15.86 FY 0.17 FZ -3.55
168 FX 17.11 FY 0.16 FZ -3.82
169 FX 17.03 FY 0.13 FZ -3.77
170 FX 16.9 FY 0.12 FZ -3.7
171 FX 17.18 FY 0.1 FZ -3.74
172 FX 17.42 FY 0.08 FZ -3.78
173 FX 18.43 FY 0.02 FZ -3.99
174 FX 17.86 FY 0.04 FZ -3.85
175 FX 17.79 FY 0.02 FZ -3.82
176 FX 17.82 FY 0 FZ -3.83
177 FX 17.79 FY -0.02 FZ -3.82
178 FX 17.86 FY -0.04 FZ -3.85
179 FX 18.42 FY -0.07 FZ -3.99
180 FX 17.42 FY -0.08 FZ -3.78
181 FX 17.18 FY -0.1 FZ -3.74
182 FX 16.9 FY -0.12 FZ -3.7
183 FX 17.03 FY -0.13 FZ -3.77
184 FX 17.11 FY -0.16 FZ -3.82
185 FX 15.86 FY -0.17 FZ -3.55
186 FX 15.42 FY -0.18 FZ -3.47
187 FX 16.44 FY -0.21 FZ -3.73
188 FX 15.04 FY -0.23 FZ -3.39
189 FX 14.33 FY -0.26 FZ -3.18
190 FX 16.26 FY -0.32 FZ -3.58
191 FX 13.69 FY -0.35 FZ -2.84
192 FX 15.49 FY -0.48 FZ -3.06
193 FX 12.22 FY -0.49 FZ -2.12
194 FX 8.44 FY -0.39 FZ -1.32

Page: 26

A26

Q326-KSP-Rtb-Deg.std

370 FX -17.79 FY 0.02 FZ -3.8
371 FX -17.82 FY 0 FZ -3.8
372 FX -17.79 FY -0.02 FZ -3.8
373 FX -17.86 FY -0.04 FZ -3.83
374 FX -18.42 FY -0.07 FZ -3.97
375 FX -17.42 FY -0.09 FZ -3.75
376 FX -17.18 FY -0.1 FZ -3.72
377 FX -16.9 FY -0.12 FZ -3.68
378 FX -17.03 FY -0.13 FZ -3.74
379 FX -15.86 FY -0.17 FZ -3.52
380 FX -15.42 FY -0.18 FZ -3.44
381 FX -16.44 FY -0.22 FZ -3.69
382 FX -15.04 FY -0.23 FZ -3.36
383 FX -14.33 FY -0.26 FZ -3.15
384 FX -16.26 FY -0.32 FZ -3.53
385 FX -13.69 FY -0.36 FZ -2.81
386 FX -15.49 FY -0.5 FZ -3
387 FX -12.23 FY -0.51 FZ -2.08
388 FX -8.44 FY -0.41 FZ -1.29
236 FX 8.39 FY 0.4 FZ -1.34
237 FX 12.22 FY 0.5 FZ -2.12
238 FX 15.48 FY 0.47 FZ -3.06
239 FX 13.69 FY 0.35 FZ -2.84
240 FX 16.26 FY 0.32 FZ -3.58
241 FX 14.33 FY 0.26 FZ -3.18
242 FX 15.04 FY 0.23 FZ -3.38
243 FX 16.43 FY 0.21 FZ -3.73
244 FX 15.42 FY 0.18 FZ -3.47
245 FX 15.86 FY 0.17 FZ -3.55
246 FX 17.11 FY 0.16 FZ -3.82
247 FX 17.03 FY 0.13 FZ -3.77
248 FX 16.9 FY 0.12 FZ -3.7
249 FX 17.18 FY 0.1 FZ -3.74
250 FX 17.42 FY 0.08 FZ -3.78
251 FX 18.43 FY 0.02 FZ -3.99
252 FX 17.86 FY 0.04 FZ -3.85
253 FX 17.79 FY 0.02 FZ -3.82
254 FX 17.82 FY 0 FZ -3.83
255 FX 17.79 FY -0.02 FZ -3.82
256 FX 17.86 FY -0.04 FZ -3.85
257 FX 18.42 FY -0.07 FZ -3.99
258 FX 17.42 FY -0.08 FZ -3.78
259 FX 17.18 FY -0.1 FZ -3.74
260 FX 16.9 FY -0.12 FZ -3.7
261 FX 17.03 FY -0.13 FZ -3.77
262 FX 17.11 FY -0.16 FZ -3.82
263 FX 15.86 FY -0.17 FZ -3.55
264 FX 15.42 FY -0.18 FZ -3.47
265 FX 16.44 FY -0.21 FZ -3.73
266 FX 15.04 FY -0.23 FZ -3.39
267 FX 14.33 FY -0.26 FZ -3.18
268 FX 16.26 FY -0.32 FZ -3.58
269 FX 13.69 FY -0.35 FZ -2.84
270 FX 15.49 FY -0.48 FZ -3.06
271 FX 12.22 FY -0.49 FZ -2.12
272 FX 8.44 FY -0.39 FZ -1.32

Page: 27

A27

Q326-KSP-Rtb-Deg.std

426 FX 6.44 FY -0.04 FZ -3.51
427 FX 6.19 FY -0.06 FZ -3.43
428 FX 8.08 FY -0.1 FZ -4.62
429 FX 7.78 FY -0.08 FZ -4.47
430 FX 8.55 FY -0.09 FZ -4.92
431 FX 9.97 FY -0.1 FZ -5.79
432 FX 10.48 FY -0.1 FZ -6.65
433 FX 10.22 FY -0.1 FZ -6.05
434 FX 11.34 FY -0.09 FZ -6.72
435 FX 11.55 FY -0.09 FZ -6.88
436 FX 11.57 FY -0.08 FZ -6.96
437 FX 9.96 FY -0.12 FZ -7.15
438 FX 12.35 FY -0.05 FZ -7.42
439 FX 13.04 FY -0.04 FZ -7.89
440 FX 15.48 FY -0.17 FZ -8.92
441 FX 12.72 FY -0.01 FZ -7.71
442 FX 12.91 FY FZ -7.8
443 FX 15.72 FY -0.01 FZ -7.71
444 FX 17.86 FY 0.01 FZ -7.7
445 FX 13.06 FY 0.01 FZ -7.88
446 FX 12.38 FY 0.05 FZ -7.44
447 FX 11.96 FY 0.06 FZ -7.2
448 FX 11.57 FY 0.08 FZ -6.96
449 FX 10.24 FY 0.1 FZ -6.06
450 FX 9.7 FY 0.1 FZ -5.72
398 FX 9.96 FY 0.1 FZ -5.79
399 FX 8.64 FY 0.09 FZ -4.96
400 FX 7.83 FY 0.09 FZ -4.51
401 FX 8.14 FY 0.1 FZ -4.65
402 FX 6.28 FY 0.06 FZ -3.47
403 FX 6.48 FY 0.05 FZ -3.55
404 FX 4.85 FY 0.03 FZ -2.74
405 FX 4.85 FY 0 FZ -2.85
469 FX -3.63 FY 2.02 FZ 3.48
470 FX -4.78 FY 0.65 FZ 3.45
471 FX -4.57 FY 0.82 FZ 2.37
472 FX -7.52 FY 0.42 FZ 3.01
473 FX -7.19 FY 0.41 FZ 2.04
474 FX -8.2 FY 0.69 FZ 3.09
475 FX -9.09 FY 0.68 FZ 3.14
476 FX -10.31 FY 0.45 FZ 3.65
477 FX -10.16 FY 0.44 FZ 3.21
478 FX -11.35 FY 0.07 FZ 3.4
479 FX -11.89 FY 0.08 FZ 3.64
480 FX -11.52 FY 1.53 FZ 3.58
481 FX -12.34 FY 0.04 FZ 3.52
482 FX -12.81 FY 0.03 FZ 3.79
483 FX -12.29 FY 0.02 FZ 3.46
484 FX -12.11 FY -0.02 FZ 3.46
485 FX -12.82 FY -0.03 FZ 3.79
486 FX -12.33 FY -0.04 FZ 3.51
487 FX -11.51 FY -0.53 FZ 3.97
488 FX -11.89 FY -0.09 FZ 3.64
489 FX -11.34 FY -0.07 FZ 3.39
490 FX -10.15 FY -0.44 FZ 3.21
491 FX -10.26 FY -0.45 FZ 3.62
492 FX -9.08 FY -0.68 FZ 3.14
493 FX -8.15 FY -0.69 FZ 3.06
502 FX -7.12 FY -0.81 FZ 3
503 FX -7.49 FY -0.42 FZ 2.99
504 FX -4.52 FY -0.83 FZ 2.33
505 FX -4.66 FY -0.65 FZ 2.61
506 FX -5.48 FY -0.04 FZ 3.48

Page: 29

A29

Q326-KSP-Rtb-Deg.std

527 FX 15.38 FY 0 FZ 10.3
528 FX 14.69 FY 0.49 FZ 9.45
529 FX 12.74 FY -2.81 FZ 9.09
530 FX 10.48 FY -1.37 FZ 8.21
543 FX 6.36 FY -6.9 FZ 8.54
2 FX -5.44 FY -0.26 FZ -2.66
3 FX -5.13 FY -0.41 FZ -2.51
4 FX -4.19 FY -0.62 FZ -2.9
5 FX -3.95 FY -0.72 FZ -3.34
6 FX -3.42 FY -0.86 FZ -3.82
7 FX -3.67 FY -0.93 FZ -4.32
8 FX -2.21 FY -0.91 FZ -4.83
9 FX -16.23 FY -1.05 FZ -4.69
10 FX -18.01 FY -1.03 FZ -5.18
11 FX -18.34 FY -0.98 FZ -5.42
12 FX -17.23 FY -0.88 FZ -4.51
13 FX -19.64 FY -0.87 FZ -5.14
14 FX -21.49 FY -0.79 FZ -4.59
15 FX -21.14 FY -0.67 FZ -5.4
16 FX -20.07 FY -0.51 FZ -6.63
17 FX -22.52 FY -0.43 FZ -8.46
18 FX -23.49 FY -0.3 FZ -9.92
19 FX -22.21 FY -0.14 FZ -11.57
20 FX -20.17 FY 0 FZ -14.82
21 FX -22.21 FY 0.14 FZ -15.47
22 FX -23.5 FY 0.29 FZ -17.94
23 FX -22.53 FY 0.43 FZ -19.62
24 FX -19.11 FY 0.51 FZ -21.65
25 FX -21.2 FY 0.67 FZ -24.22
26 FX -21.51 FY 0.79 FZ -26.66
27 FX -19.68 FY 0.86 FZ -29.17
28 FX -17.3 FY 0.88 FZ -31.59
29 FX -18.39 FY 0.98 FZ -34.11
30 FX -18.11 FY 1.03 FZ -36.28
31 FX -16.36 FY 1.05 FZ -37.7
32 FX -12.83 FY 0.92 FZ -37.73
33 FX -13.78 FY 0.93 FZ -39.33
34 FX -14.85 FY 0.98 FZ -41.08
35 FX -10.15 FY 0.74 FZ -41.7
36 FX -8.93 FY 0.63 FZ -43.05
37 FX -6.82 FY 0.45 FZ -45.27
38 FX -5.52 FY 0.23 FZ -47.75
39 FX -4.32 FY 0.17 FZ -50.33
509 FX 5.75 FY 4.4 FZ 7.5
510 FX 5.25 FY 2.88 FZ 5.2
512 FX 11.3 FY 3.63 FZ 9.89
513 FX 11.17 FY 4.53 FZ 10.51
514 FX 11.56 FY 6.7 FZ 12.66
516 FX 13.08 FY 6.15 FZ 11.61
517 FX 16.15 FY 1.04 FZ 11.64
518 FX 16.44 FY 2.86 FZ 10.95
520 FX 16.27 FY -0.62 FZ 10.98
521 FX 18.3 FY -0.14 FZ 12.84
522 FX 16.21 FY 4.02 FZ 12.24
524 FX 17.5 FY -0.34 FZ 12.09
525 FX 19.48 FY -0.21 FZ 13.79
526 FX 17.38 FY -0.09 FZ 12.11
528 FX 17.38 FY 0.09 FZ 12.11
529 FX 19.49 FY 0.21 FZ 13.8
530 FX 17.5 FY 0.35 FZ 12.09
532 FX 16.29 FY -4.02 FZ 12.24
533 FX 16.32 FY 0.15 FZ 12.66
534 FX 16.3 FY 0.62 FZ 11.01
536 FX 16.49 FY -2.85 FZ 10.85
537 FX 16.23 FY 1.05 FZ 11.64
538 FX 13.21 FY -6.16 FZ 11.65
540 FX 11.7 FY -6.69 FZ 11.71
541 FX 11.32 FY -4.5 FZ 10.56
542 FX 11.55 FY -3.65 FZ 9.59
544 FX 5.37 FY -2.9 FZ 5.84
545 FX 5.7 FY -4.3 FZ 4.44
546 FX 3.63 FY -3.47 FZ 5.44

Page: 30

A30

Q326-KSP-Rtb-Deg.std

40 FX 221.74 FY 99.95 FZ 91.76
70 FX 221.94 FY -99.96 FZ 91.76
119 FX -9.49 FY -0.77 FZ 0.71
120 FX -16.89 FY -1.1 FZ 0.81
121 FX -7.75 FY -1.47 FZ 1.39
122 FX -8.16 FY -1.97 FZ 1.62
123 FX -10.39 FY -1.9 FZ 2.08
124 FX -10.97 FY -1.91 FZ 2.34
125 FX -12.4 FY -2.72 FZ 2.67
126 FX -14.13 FY -2.09 FZ 3.1
127 FX -14.28 FY -1.9 FZ 3.23
128 FX -15.06 FY -1.78 FZ 3.45
129 FX -16.25 FY -1.7 FZ 3.73
130 FX -16.47 FY -1.5 FZ 3.95
131 FX -16.58 FY -1.22 FZ 4.19
132 FX -16.91 FY -1.08 FZ 4.03
133 FX -17.08 FY -0.87 FZ 4.09
134 FX -17.18 FY -0.63 FZ 4.21
135 FX -17.44 FY -0.44 FZ 4.21
136 FX -17.46 FY -0.21 FZ 4.22
137 FX -17.5 FY 0 FZ 4.22
138 FX -17.46 FY 0.21 FZ 4.22
139 FX -17.45 FY 0.43 FZ 4.19
140 FX -17.8 FY 0.67 FZ 4.26
141 FX -17.08 FY 0.87 FZ 4.09
142 FX -16.91 FY 1.08 FZ 3.92
143 FX -16.58 FY 1.27 FZ 3.92
144 FX -16.48 FY 1.49 FZ 3.84
145 FX -16.23 FY 1.7 FZ 3.75
146 FX -15.05 FY 1.79 FZ 3.45
147 FX -14.28 FY 1.9 FZ 3.23
148 FX -14.18 FY 2.08 FZ 3.09
149 FX -12.41 FY 2.01 FZ 2.69
150 FX -11.71 FY 1.9 FZ 2.38
151 FX -10.37 FY 1.92 FZ 2.09
152 FX -8.16 FY 1.57 FZ 1.62
153 FX -7.18 FY 1.46 FZ 1.27
154 FX -6.34 FY 1.33 FZ 1.05
155 FX -9.76 FY 0.81 FZ 0.73
41 FX 9.77 FY -0.84 FZ 0.73
42 FX 6.36 FY -1.13 FZ 1.02
43 FX 7.76 FY -1.48 FZ 1.37
44 FX 8.16 FY -1.97 FZ 1.62
45 FX 10.39 FY -1.93 FZ 2.08
46 FX 10.97 FY -1.91 FZ 2.34
47 FX 12.41 FY -2.72 FZ 2.67
48 FX 14.27 FY -2.1 FZ 3.12
49 FX 14.33 FY -1.9 FZ 3.23
50 FX 15.06 FY -1.78 FZ 3.45
51 FX 16.25 FY -1.7 FZ 3.74
52 FX 16.47 FY -1.49 FZ 3.92
53 FX 16.58 FY -1.27 FZ 3.92
54 FX 16.91 FY -1.07 FZ 4.02
55 FX 17.08 FY -0.87 FZ 4.03
56 FX 17.18 FY -0.63 FZ 4.25
57 FX 17.44 FY -0.43 FZ 4.2
58 FX 17.46 FY -0.21 FZ 4.21
59 FX 17.5 FY 0 FZ 4.22
60 FX 17.46 FY 0.21 FZ 4.21
61 FX 17.45 FY 0.43 FZ 4.19
62 FX 17.81 FY 0.67 FZ 4.26
63 FX 17.08 FY 0.87 FZ 4.09
64 FX 16.91 FY 1.08 FZ 4.02
65 FX 16.58 FY 1.27 FZ 3.92
66 FX 16.48 FY 1.49 FZ 3.84
67 FX 16.24 FY 1.7 FZ 3.74
68 FX 15.05 FY 1.79 FZ 3.44
69 FX 14.33 FY -1.9 FZ 3.23
70 FX 14.31 FY 2.11 FZ 3.12
71 FX 12.41 FY 2.01 FZ 2.68
72 FX 10.98 FY 1.93 FZ 2.38
73 FX 10.37 FY 1.93 FZ 2.08
74 FX 8.16 FY 1.57 FZ 1.62
75 FX 7.78 FY 1.48 FZ 1.36
76 FX 6.34 FY 1.13 FZ 1.02

Page: 31

A31



Q326-KSP-R4b-Deg.std
 77 FX 9.63 FY 0.77 F2 0.66
 ***RS-INT-2-WU
 186 FX -221.02 FY 99.82 F2 91.63
 234 FX -221.81 FY -99.81 F2 91.67
 79 FX 221.74 FY 99.95 F2 91.75
 117 FX 221.94 FY -99.96 F2 91.76
 157 FX -9.49 FY -0.77 F2 0.71
 196 FX -6.36 FY -1.1 F2 1.01
 199 FX -7.75 FY -1.47 F2 1.39
 240 FX -8.16 FY -1.57 F2 1.62
 201 FX -10.39 FY -1.91 F2 2.08
 202 FX -10.97 FY -1.91 F2 2.34
 203 FX -12.4 FY -2 F2 2.67
 204 FX -14.15 FY -2.09 F2 3.1
 206 FX -15.06 FY -1.79 F2 3.45
 207 FX -16.25 FY -1.7 F2 3.73
 208 FX -16.47 FY -1.5 F2 3.85
 209 FX -16.59 FY -1.28 F2 3.92
 210 FX -16.91 FY -1.08 F2 4.03
 211 FX -17.08 FY -0.87 F2 4.09
 212 FX -17.81 FY -0.67 F2 4.22
 213 FX -17.41 FY 2.17 F2 4.22
 214 FX -17.46 FY -0.23 F2 4.22
 215 FX -17.5 FY 0 F2 4.22
 216 FX -17.46 FY 0.23 F2 4.22
 217 FX -17.45 FY 0.43 F2 4.19
 218 FX -17.8 0.67 F2 4.25
 219 FX -17.08 FY 0.87 F2 4.09
 220 FX -16.91 FY 1.08 F2 4.03
 221 FX -16.59 FY 1.27 F2 3.92
 222 FX -16.48 FY 1.49 F2 3.84
 223 FX -16.23 FY 1.7 F2 3.75
 224 FX -15.05 FY 1.79 F2 3.45
 225 FX -14.28 FY 1.9 F2 3.23
 226 FX -14.18 FY 2.08 F2 3.09
 227 FX -12.41 FY 2.01 F2 2.69
 228 FX -11 FY 1.9 F2 2.32
 229 FX -10.37 FY 1.92 F2 2.09
 230 FX -9.16 FY 1.97 F2 1.62
 231 FX -7.78 FY 1.46 F2 1.37
 232 FX -6.38 FY 1.13 F2 1.08
 233 FX -9.76 FY 0.81 F2 0.73
 80 FX 9.77 FY -0.84 F2 0.73
 81 FX 8.16 FY -1.57 F2 1.6
 82 FX 7.76 FY -1.48 F2 1.37
 83 FX 8.16 FY -1.57 F2 1.6
 84 FX 10.39 FY -1.93 F2 2.08
 85 FX 10.97 FY -1.91 F2 2.34
 86 FX 12.42 FY -2.01 F2 2.68
 87 FX 14.27 FY -1 F2 3.12
 88 FX 14.31 FY -1.9 F2 3.23
 89 FX 15.06 FY -1.79 F2 3.45
 90 FX 16.25 FY -1.7 F2 3.74
 91 FX 16.47 FY -1.49 F2 3.85
 92 FX 16.59 FY -1.28 F2 3.92
 93 FX 16.91 FY -1.08 F2 4.03
 94 FX 17.08 FY -0.87 F2 4.09
 95 FX 17.81 FY -0.67 F2 4.22
 96 FX 17.41 FY -0.43 F2 4.2
 97 FX 17.46 FY -0.23 F2 4.21
 98 FX 17.5 FY 0 F2 4.22
 99 FX 17.46 FY 0.23 F2 4.21
 100 FX 17.45 FY 0.44 F2 4.2
 101 FX 18.16 FY 1.07 F2 4.22
 102 FX 17.08 FY 0.87 F2 4.09
 103 FX 16.91 FY 1.08 F2 4.03
 104 FX 16.59 FY 1.27 F2 3.92
 105 FX 16.48 FY 1.49 F2 3.84
 106 FX 16.24 FY 1.7 F2 3.74
 107 FX 15.05 FY 1.79 F2 3.44
 108 FX 14.31 FY 1.9 F2 3.23
 109 FX 14.31 FY 2.1 F2 3.12
 110 FX 12.41 FY 2.01 F2 2.68
 111 FX 10.98 FY 1.91 F2 2.32

Page: 32

Q326-KSP-R4b-Deg.std
 334 FX 17.45 FY 0.44 F2 4.2
 335 FX 17.81 FY 0.67 F2 4.26
 336 FX 17.08 FY 0.87 F2 4.09
 337 FX 16.91 FY 1.08 F2 4.02
 338 FX 16.59 FY 1.27 F2 3.92
 339 FX 16.48 FY 1.49 F2 3.84
 340 FX 16.24 FY 1.7 F2 3.74
 341 FX 15.05 FY 1.79 F2 3.44
 342 FX 14.31 FY 1.9 F2 3.12
 343 FX 14.31 FY 2.1 F2 3.12
 344 FX 12.41 FY 2.1 F2 2.68
 345 FX 10.98 FY 1.91 F2 2.32
 346 FX 10.37 FY 1.92 F2 2.08
 347 FX 9.16 FY 1.97 F2 1.62
 348 FX 7.78 FY 1.48 F2 1.36
 349 FX 6.34 FY 1.13 F2 1.02
 350 FX -10.35 FY -1.91 F2 2.08
 ***RS-EDGE-SBOARD-WU
 429 FX 0.21 FY 0.08 F2 0.01
 431 FX 0.21 FY -0.08 F2 0.03
 472 FX -6.22 FY 6.93 F2 8.17
 476 FX -10.47 FY 3.21 F2 8.28
 480 FX -12.84 FY 4.56 F2 9.6
 484 FX -14.8 FY 5.9 F2 9.82
 488 FX -15.45 FY 6.2 F2 10.18
 492 FX -14.71 FY -1.51 F2 9.82
 496 FX -12.75 FY -4.56 F2 9.59
 500 FX -10.35 FY -3.51 F2 8.25
 504 FX -6.05 FY -6.82 F2 8.14
 428 FX 5.31 FY 0.23 F2 -2.58
 427 FX 6.39 FY 0.43 F2 -2.51
 426 FX 8.21 FY 0.6 F2 -2.86
 425 FX 9.93 FY 0.76 F2 -3.23
 424 FX 14.63 FY 0.96 F2 -4.87
 423 FX 13.69 FY 0.92 F2 -4.24
 422 FX 12.67 FY 0.93 F2 -3.57
 421 FX 16.36 FY 1.03 F2 -4.63
 420 FX 18.02 FY 1.02 F2 -5.05
 419 FX 18.27 FY 0.97 F2 -5.43
 418 FX 17.23 FY 0.88 F2 -5.37
 417 FX 19.74 FY 0.85 F2 -5.05
 416 FX 21.49 FY 0.78 F2 -5.5
 415 FX 21.15 FY 0.67 F2 -5.26
 414 FX 19.09 FY 0.51 F2 -4.52
 413 FX 22.49 FY 0.43 F2 -5.46
 412 FX 23.5 FY 0.29 F2 -5.79
 411 FX 22.19 FY 0.14 F2 -5.31
 410 FX 20.14 FY 0 F2 -4.68
 409 FX 22.19 FY -0.14 F2 -5.32
 408 FX 23.5 FY -0.29 F2 -5.79
 407 FX 22.52 FY -0.43 F2 -5.5
 406 FX 19.15 FY -0.51 F2 -4.54
 405 FX 21.18 FY -0.66 F2 -5.27
 404 FX 21.52 FY -0.78 F2 -5.51
 403 FX 19.79 FY -0.85 F2 -5.05
 402 FX 17.31 FY -0.87 F2 -4.42
 401 FX 18.34 FY -0.97 F2 -4.95
 399 FX 18.11 FY -1.03 F2 -5.08
 398 FX 16.4 FY -1.04 F2 -4.62
 397 FX 12.83 FY -0.9 F2 -3.66
 396 FX 12.82 FY -0.94 F2 -4.26
 395 FX 14.83 FY -0.95 F2 -4.98
 394 FX 10.16 FY -0.73 F2 -3.31
 394 FX 8.18 FY -0.64 F2 -2.87
 393 FX 6.87 FY -0.43 F2 -2.76
 392 FX 5.38 FY -0.26 F2 -2.53
 659 FX -3.46 FY 5.24 F2 6.68
 470 FX -5.66 FY 2.88 F2 6.14
 471 FX -5.81 FY 3.81 F2 6.54
 473 FX -11.58 FY 2.39 F2 5.13
 474 FX -11.3 FY 7.06 F2 12.02
 475 FX -11.81 FY 1.12 F2 10.81
 477 FX -11.33 FY 3.17 F2 10.29
 478 FX -16.19 FY 4.05 F2 12.78
 479 FX -14.56 FY 0.28 F2 9.82

Page: 36

A32

Q326-KSP-R4b-Deg.std
 112 FX 10.37 FY 1.93 F2 2.08
 113 FX 8.16 FY 1.57 F2 1.6
 114 FX 7.78 FY 1.48 F2 1.36
 115 FX 6.34 FY 1.1 F2 1.02
 116 FX 9.63 FY 0.77 F2 0.66
 ***RS-INT-3-WU
 274 FX -222.02 FY 99.82 F2 91.63
 312 FX -221.81 FY -99.81 F2 91.67
 157 FX 221.74 FY 99.95 F2 91.75
 195 FX 221.94 FY -99.96 F2 91.76
 275 FX -9.49 FY -0.77 F2 0.71
 276 FX -6.36 FY -1.1 F2 1.01
 277 FX -7.75 FY -1.47 F2 1.39
 278 FX -8.16 FY -1.57 F2 1.62
 279 FX -10.39 FY -1.91 F2 2.08
 280 FX -10.97 FY -1.91 F2 2.34
 281 FX -12.4 FY -2 F2 2.67
 282 FX -14.15 FY -2.09 F2 3.1
 283 FX -14.28 FY -1.9 F2 3.23
 284 FX -15.06 FY -1.79 F2 3.45
 285 FX -16.25 FY -1.7 F2 3.73
 286 FX -16.47 FY -1.5 F2 3.85
 287 FX -16.59 FY -1.28 F2 3.92
 288 FX -16.91 FY -1.08 F2 4.03
 289 FX -17.08 FY -0.87 F2 4.09
 290 FX -17.81 FY -0.67 F2 4.22
 291 FX -17.41 FY 2.17 F2 4.22
 292 FX -17.46 FY -0.23 F2 4.22
 293 FX -17.5 FY 0 F2 4.22
 294 FX -17.46 FY 0.23 F2 4.22
 295 FX -17.46 FY 0.43 F2 4.22
 296 FX -17.8 FY 0.67 F2 4.26
 297 FX -17.08 FY 0.87 F2 4.09
 298 FX -16.91 FY 1.08 F2 4.03
 299 FX -16.59 FY 1.27 F2 3.92
 300 FX -16.48 FY 1.49 F2 3.84
 301 FX -16.23 FY 1.7 F2 3.75
 302 FX -15.05 FY 1.79 F2 3.45
 303 FX -14.28 FY 1.9 F2 3.23
 304 FX -14.18 FY 2.08 F2 3.09
 305 FX -12.41 FY 2.01 F2 2.69
 306 FX -11 FY 1.9 F2 2.32
 307 FX -10.37 FY 1.92 F2 2.09
 308 FX -9.16 FY 1.97 F2 1.62
 309 FX -7.78 FY 1.46 F2 1.37
 310 FX -6.34 FY 1.13 F2 1.08
 311 FX -9.76 FY 0.81 F2 0.73
 312 FX -8.16 FY -1.57 F2 1.6
 313 FX -7.76 FY -1.48 F2 1.37
 314 FX 10.39 FY -1.93 F2 2.08
 315 FX 10.97 FY -1.91 F2 2.34
 316 FX 12.42 FY -2.01 F2 2.68
 317 FX 14.27 FY -1 F2 3.12
 318 FX 14.31 FY -1.9 F2 3.23
 319 FX 15.06 FY -1.79 F2 3.45
 320 FX 16.25 FY -1.7 F2 3.74
 321 FX 16.47 FY -1.49 F2 3.85
 322 FX 16.59 FY -1.28 F2 3.92
 323 FX 16.91 FY -1.08 F2 4.03
 324 FX 17.08 FY -0.87 F2 4.09
 325 FX 17.81 FY -0.67 F2 4.22
 326 FX 17.41 FY -0.43 F2 4.2
 327 FX 17.46 FY -0.23 F2 4.21
 328 FX 17.5 FY 0 F2 4.22
 329 FX 17.46 FY 0.23 F2 4.21
 330 FX 17.45 FY 0.44 F2 4.2
 331 FX 18.16 FY 1.07 F2 4.22
 332 FX 17.08 FY 0.87 F2 4.09
 333 FX 16.91 FY 1.08 F2 4.03
 334 FX 16.59 FY 1.27 F2 3.92
 335 FX 16.48 FY 1.49 F2 3.84
 336 FX 16.24 FY 1.7 F2 3.74
 337 FX 15.05 FY 1.79 F2 3.44

Page: 33

A36

Q326-KSP-R4b-Deg.std
 481 FX -16.4 FY -0.48 F2 10.96
 482 FX -18.4 FY -0.52 F2 12.64
 483 FX -16.39 FY 0.46 F2 11.63
 485 FX -17.58 FY -0.32 F2 12.01
 486 FX -19.55 FY -0.17 F2 13.67
 487 FX -17.45 FY -0.07 F2 11.99
 489 FX -17.45 FY 0.07 F2 11.99
 490 FX -19.56 FY 0.17 F2 13.68
 491 FX -16.34 FY 0.46 F2 11.63
 493 FX -16.35 FY -1.78 F2 11.61
 494 FX -15.45 FY 0.52 F2 12.62
 495 FX -16.36 FY 0.48 F2 10.95
 497 FX -14.59 FY -0.28 F2 9.79
 498 FX -16.05 FY -0.44 F2 12.76
 499 FX -13.27 FY -3.17 F2 10.25
 501 FX -11.07 FY -4.11 F2 9.97
 502 FX -11.09 FY 7.04 F2 11.94
 503 FX -11.42 FY -2.39 F2 9.66
 505 FX -5.24 FY -3.78 F2 8.45
 506 FX -5.4 FY -4.88 F2 5.93
 507 FX -3.51 FY -5.19 F2 6.74

 LOAD 7 LOADTYPE Wind TITLE LOAD CASE 7 - WP
 JOINT LOAD
 ***RS-EDGE-DOOR-WP
 1 FX -0.12 FY 0.64 F2 0.34
 39 FX -0.12 FY -0.64 F2 0.33
 511 FX 7.93 FY 1.62 F2 3.27
 515 FX 11.8 FY 0.47 F2 3.6
 519 FX 13.59 FY 1.1 F2 3.96
 523 FX 15.08 FY 0.09 F2 3.88
 527 FX 15.61 FY 0 F2 4.05
 531 FX 15.1 FY -0.09 F2 3.89
 535 FX 13.63 FY -1.1 F2 3.99
 539 FX 11.85 FY -0.46 F2 3.63
 543 FX 1.42 FY -1.62 F2 3.34
 2 FX -5.19 FY 0.11 F2 -3.2
 3 FX -5.71 FY 0.18 F2 -3.42
 4 FX -11.96 FY 0.37 F2 -7.41
 10 FX -11.54 FY 0.34 F2 -7.26
 11 FX -12.11 FY 0.33 F2 -7.64
 12 FX -13.12 FY 0.31 F2 -8.28
 13 FX -13.22 FY 0.28 F2 -8.41
 14 FX -13.27 FY 0.25 F2 -8.51
 15 FX -13.33 FY 0.22 F2 -8.64
 16 FX -13.73 FY 0.17 F2 -8.79
 17 FX -14.58 FY 0.14 F2 -9.39
 18 FX -18.7 FY 0.09 F2 -9.57
 19 FX -14.12 FY 0.05 F2 -9.12
 20 FX -14.17 FY 0 F2 -9.11
 21 FX -14.12 FY -0.05 F2 -9.12
 22 FX -14.2 FY -0.09 F2 -9.19
 24 FX -13.75 FY -0.17 F2 -8.81
 25 FX -13.56 FY -0.22 F2 -8.7
 26 FX -12.47 FY -0.25 F2 -8.19
 27 FX -13.24 FY -0.27 F2 -8.41
 28 FX -13.17 FY -0.31 F2 -8.31
 29 FX -12.47 FY -0.4 F2 -7.59
 30 FX -11.59 FY -0.34 F2 -7.29
 31 FX -12.02 FY -0.36 F2 -7.44
 32 FX -10.61 FY -0.24 F2 6.68
 33 FX -9.67 FY -0.35 F2 -5.93
 34 FX -10.38 FY -0.37 F2 -6.21
 35 FX -9.58 FY -0.35 F2 -6.13
 36 FX -8.07 FY -0.26 F2 -4.69
 37 FX -11.81 FY -0.12 F2 10.81
 38 FX -5.26 FY -0.1 F2 -3.22
 508 FX 3.91 FY 2.19 F2 3.66
 509 FX 8.82 FY 1.49 F2 3.61

Page: 37

A33

Q326-KSP-R4b-Deg.std
 186 FX 14.31 FY 1.9 F2 3.23
 187 FX 14.31 FY 2.11 F2 3.12
 188 FX 12.41 FY 2.01 F2 2.68
 189 FX 10.98 FY 1.91 F2 2.32
 190 FX 10.37 FY 1.93 F2 2.08
 191 FX 9.63 FY 0.77 F2 0.66
 192 FX 7.78 FY 1.48 F2 1.36
 193 FX 6.34 FY 1.1 F2 1.02
 194 FX 9.63 FY 0.77 F2 0.66
 ***RS-INT-4-WU
 352 FX -222.02 FY 99.82 F2 91.63
 390 FX -221.81 FY -99.81 F2 91.67
 235 FX 221.74 FY 99.95 F2 91.75
 275 FX -9.49 FY -0.77 F2 0.71
 276 FX -6.36 FY -1.1 F2 1.01
 277 FX -7.75 FY -1.47 F2 1.39
 278 FX -8.16 FY -1.57 F2 1.62
 279 FX -10.39 FY -1.91 F2 2.08
 280 FX -10.97 FY -1.91 F2 2.34
 281 FX -12.4 FY -2 F2 2.67
 282 FX -14.15 FY -2.09 F2 3.1
 283 FX -14.28 FY -1.9 F2 3.23
 284 FX -15.06 FY -1.79 F2 3.45
 285 FX -16.25 FY -1.7 F2 3.73
 286 FX -16.47 FY -1.5 F2 3.85
 287 FX -16.59 FY -1.28 F2 3.92
 288 FX -16.91 FY -1.08 F2 4.03
 289 FX -17.08 FY -0.87 F2 4.09
 290 FX -17.81 FY -0.67 F2 4.22
 291 FX -17.41 FY 2.17 F2 4.22
 292 FX -17.46 FY -0.23 F2 4.22
 293 FX -17.5 FY 0 F2 4.22
 294 FX -17.46 FY 0.23 F2 4.22
 295 FX -17.46 FY 0.43 F2 4.22
 296 FX -17.8 FY 0.67 F2 4.26
 297 FX -17.08 FY 0.87 F2 4.09
 298 FX -16.91 FY 1.08 F2 4.03
 299 FX -16.59 FY 1.27 F2 3.92
 300 FX -16.48 FY 1.49 F2 3.84
 301 FX -16.23 FY 1.7 F2 3.75
 302 FX -15.05 FY 1.79 F2 3.45
 303 FX -14.28 FY 1.9 F2 3.23
 304 FX -14.18 FY 2.08 F2 3.09
 305 FX -12.41 FY 2.01 F2 2.69
 306 FX -11 FY 1.9 F2 2.32
 307 FX -10.37 FY 1.92 F2 2.09
 308 FX -9.16 FY 1.97 F2 1.62
 309 FX -7.78 FY 1.46 F2 1.37
 310 FX -6.34 FY 1.13 F2 1.08
 311 FX -9.76 FY 0.81 F2 0.73
 312 FX -8.16 FY -1.57 F2 1.6
 313 FX -7.76 FY -1.48 F2 1.37
 314 FX 10.39 FY -1.93 F2 2.08
 315 FX 10.97 FY -1.91 F2 2.34
 316 FX 12.42 FY -2.01 F2 2.68
 317 FX 14.27 FY -1 F2 3.12
 318 FX 14.31 FY -1.9 F2 3.23
 319 FX 15.06 FY -1.79 F2 3.45
 320 FX 16.25 FY -1.7 F2 3.74
 321 FX 16.47 FY -1.49 F2 3.85
 322 FX 16.59 FY -1.28 F2 3.92
 323 FX 16.91 FY -1.08 F2 4.03
 324 FX 17.08 FY -0.87 F2 4.09
 325 FX 17.81 FY -0.67 F2 4.22
 326 FX 17.41 FY -0.43 F2 4.2
 327 FX 17.46 FY -0.23 F2 4.21
 328 FX 17.5 FY 0 F2 4.22
 329 FX 17.46 FY 0.23 F2 4.21
 330 FX 17.45 FY 0.44 F2 4.2
 331 FX 18.16 FY 1.07 F2 4.22
 332 FX 17.08 FY 0.87 F2 4.09
 333 FX 16.91 FY 1.08 F2 4.03
 334 FX 16.59 FY 1.27 F2 3.92
 335 FX 16.48 FY 1.49 F2 3.84
 336 FX 16.24 FY 1.7 F2 3.74
 337 FX 15.05 FY 1.79 F2 3.44

Page: 34

A37

Q326-KSP-R4b-Deg.std
 510 FX 5.83 FY 1.03 F2 2.76
 512 FX 10.91 FY 0.88 F2 3.91
 513 FX -16.39 FY 0.46 F2 11.63
 514 FX 11.06 FY 1.34 F2 4.12
 516 FX 12.09 FY 1.42 F2 4.15
 517 FX 13.86 FY 0.07 F2 14.28
 518 FX 13.37 FY 1.28 F2 4.29
 520 FX 14.47 FY 0.18 F2 4.25
 521 FX 15.44 FY 0.34 F2 4.4
 522 FX 14.72 FY 2.52 F2 4.57
 523 FX 15.65 F2 5.89 F2 4.37
 525 FX 16.36 FY 0.06 F2 4.71
 526 FX 15.53 FY 0.04 F2 4.3
 528 FX 15.53 FY 0.04 F2 4.3
 529 FX 16.37 FY -0.06 F2 4.72
 530 FX 15.64 FY -0.08 F2 4.37
 532 FX 15.76 FY -0.15 F2 4.38
 533 FX 15.43 FY -0.45 F2 4.62
 534 FX 14.48 FY -0.18 F2 4.25
 536 FX 14.31 FY -1.28 F2 4.3
 537 FX 13.7 FY -0.59 F2 4.45
 538 FX 12.41 FY -1.1 F2 4.19
 540 FX 11.13 FY -1.34 F2 4.16
 541 FX 9.74 FY -0.96 F2 3.83
 542 FX 10.14 FY -0.87 F2 3.88
 544 FX 5.93 FY -1.01 F2 2.83
 545 FX 5.77 FY -1.49 F2 3.59
 546 FX 4 FY -2.19 F2 3.69
 ***RS-INT-1-WP
 118 FX -26.18 FY 15.94 F2 9.12
 156 FX -26.17 FY -15.92 F2 9.11
 40 FX 26.23 FY 16.65 F2 9.69
 78 FX 26.23 FY -16.66 F2 9.69
 119 FX -11.39 FY 0.8 F2 -1.95
 120 FX -16.36 FY 1.05 F2 -3.15
 121 FX 21.23 FY 1.17 F2 -4.56
 122 FX -18.7 FY 0.93 F2 -4.19
 123 FX -21.75 FY 0.92 F2 -5.06
 124 FX 18.59 FY 0.74 F2 -4.36
 125 FX -19 FY 0.69 F2 -4.49
 126 FX -20.12 FY 0.66 F2 -4.76
 127 FX -18.36 FY 0.55 F2 -4.31
 128 FX -18.45 FY 0.51 F2 -4.3
 129 FX -19.44 FY 0.47 F2 -4.49
 130 FX -18.96 FY 0.4 F2 -4.36
 131 FX -18.51 FY 0.35 F2 -4.2
 132 FX -18.58 FY 0.29 F2 -4.19
 133 FX -18.63 FY 0.24 F2 -4.17
 134 FX -19.52 FY 0.19 F2 -4.35
 135 FX 18.82 FY 0.12 F2 -4.18
 136 FX -18.7 FY 0.06 F2 -4.14
 137 FX -18.71 FY 0 F2 -4.14
 138 FX -18.7 FY -0.06 F2 -4.14
 139 FX -18.82 FY -0.11 F2 -4.17
 140 FX -19.51 FY -0.19 F2 -4.35
 141 FX -18.63 FY -0.24 F2 -4.17
 142 FX -18.58 FY -0.29 F2 -4.19
 143 FX -18.51 FY -0.35 F2 -4.12
 144 FX -18.96 FY -0.4 F2 -4.34
 145 FX -19.44 FY -0.47 F2 -4.5
 146 FX -18.45 FY -0.51 F2 -4.3
 147 FX -18.36 FY -0.55 F2 -4.31
 148 FX -20.12 FY -0.65 F2 -4.76
 149 FX -18.82 FY -0.69 F2 -4.59
 150 FX -18.59 FY -0.74 F2 -4.36
 151 FX -21.74 FY -0.

Q326-KSP-R4b-Deg.std

040

81	FX	16.36	FY	1.04	FZ	-3.2
82	FX	21.23	FY	1.15	FZ	-4.61
83	FX	18.7	FY	0.93	FZ	-4.21
84	FX	21.74	FY	0.93	FZ	-5.11
85	FX	18.59	FY	0.75	FZ	-4.38
86	FX	19.7	FY	0.69	FZ	-4.51
87	FX	20.12	FY	0.66	FZ	-4.8
88	FX	18.36	FY	0.56	FZ	-4.33
89	FX	18.45	FY	0.51	FZ	-4.32
90	FX	19.44	FY	0.48	FZ	-4.53
91	FX	18.96	FY	0.4	FZ	-4.37
92	FX	18.51	FY	0.35	FZ	-4.22
93	FX	18.58	FY	0.3	FZ	-4.21
94	FX	18.63	FY	0.24	FZ	-4.2
95	FX	18.52	FY	0.19	FZ	-4.38
96	FX	18.82	FY	0.12	FZ	-4.2
97	FX	18.7	FY	0.06	FZ	-4.16
98	FX	18.71	FY	0	FZ	-4.16
99	FX	18.82	FY	-0.12	FZ	-4.16
100	FX	18.82	FY	-0.12	FZ	-4.2
101	FX	19.51	FY	-0.19	FZ	-4.38
102	FX	16.63	FY	-0.24	FZ	-4.2
103	FX	16.58	FY	-0.1	FZ	-4.21
104	FX	16.51	FY	-0.35	FZ	-4.23
105	FX	16.96	FY	-0.41	FZ	-4.37
106	FX	19.44	FY	-0.48	FZ	-4.53
107	FX	16.53	FY	-0.52	FZ	-4.32
108	FX	16.36	FY	-0.56	FZ	-4.32
109	FX	20.12	FY	-0.66	FZ	-4.79
110	FX	18.99	FY	-0.7	FZ	-4.51
111	FX	18.59	FY	-0.75	FZ	-4.38
112	FX	21.74	FY	-0.93	FZ	-5.11
113	FX	18.7	FY	-0.93	FZ	-4.21
114	FX	21.24	FY	-1.15	FZ	-4.61
115	FX	16.35	FY	-1.04	FZ	-3.19
116	FX	11.37	FY	-0.77	FZ	-2
***KSP-INT-WP						
274	FX	-26.18	FY	15.94	FZ	9.12
312	FX	-26.17	FY	-15.92	FZ	9.11
157	FX	26.23	FY	16.65	FZ	9.69
155	FX	26.23	FY	-16.66	FZ	9.69
275	FX	-11.39	FY	1.57	FZ	-3.85
276	FX	-16.36	FY	1.05	FZ	-3.15
277	FX	-21.23	FY	1.17	FZ	-4.56
278	FX	-18.7	FY	0.93	FZ	-4.21
279	FX	-21.75	FY	0.92	FZ	-5.06
280	FX	-18.59	FY	0.74	FZ	-4.36
281	FX	-19	FY	0.69	FZ	-4.49
282	FX	-20.12	FY	0.66	FZ	-4.76
283	FX	-16.36	FY	0.55	FZ	-4.31
284	FX	-18.45	FY	0.51	FZ	-4.3
285	FX	-19.44	FY	0.47	FZ	-4.49
286	FX	-18.56	FY	0.4	FZ	-4.34
287	FX	-18.51	FY	0.35	FZ	-4.2
288	FX	-18.58	FY	0.29	FZ	-4.19
289	FX	-18.52	FY	0.24	FZ	-4.17
290	FX	-19.52	FY	0.19	FZ	-4.35
291	FX	-18.82	FY	0.12	FZ	-4.18
292	FX	-18.7	FY	0.06	FZ	-4.14
293	FX	-18.71	FY	0	FZ	-4.14
294	FX	-18.7	FY	-0.06	FZ	-4.14
295	FX	-18.82	FY	-0.11	FZ	-4.17
296	FX	-19.51	FY	-0.19	FZ	-4.35
297	FX	-16.63	FY	-0.24	FZ	-4.17
298	FX	-16.58	FY	-0.29	FZ	-4.19
299	FX	-18.51	FY	-0.35	FZ	-4.2
300	FX	-19.52	FY	-0.4	FZ	-4.34
301	FX	-19.44	FY	-0.47	FZ	-4.5
302	FX	-18.45	FY	-0.51	FZ	-4.3
303	FX	-18.36	FY	-0.55	FZ	-4.31
304	FX	-20.12	FY	-0.66	FZ	-4.76
305	FX	-18.59	FY	-0.7	FZ	-4.49
306	FX	-18.59	FY	-0.75	FZ	-4.38
307	FX	-21.74	FY	-0.93	FZ	-5.06
308	FX	-18.7	FY	-0.93	FZ	-4.19

Page: 40

Q326-KSP-R4b-Deg.std

041

309	FX	-21.24	FY	-1.16	FZ	-4.56
310	FX	-16.36	FY	-1.06	FZ	-3.16
311	FX	-13.42	FY	-0.82	FZ	-1.98
312	FX	-10.34	FY	0	FZ	-0.64
313	FX	-16.36	FY	1.04	FZ	-3.2
314	FX	-21.23	FY	1.1	FZ	-4.63
315	FX	-18.7	FY	0.93	FZ	-4.21
316	FX	-21.74	FY	0.93	FZ	-5.11
317	FX	-18.59	FY	0.75	FZ	-4.38
318	FX	-19.7	FY	0.69	FZ	-4.51
319	FX	-20.12	FY	0.66	FZ	-4.8
320	FX	-18.36	FY	0.56	FZ	-4.33
321	FX	-18.45	FY	0.51	FZ	-4.32
322	FX	-19.44	FY	0.48	FZ	-4.53
323	FX	-18.96	FY	0.4	FZ	-4.37
324	FX	-18.51	FY	0.35	FZ	-4.22
325	FX	-18.58	FY	0.3	FZ	-4.21
326	FX	-18.63	FY	0.24	FZ	-4.2
327	FX	-19.52	FY	0.19	FZ	-4.38
328	FX	-18.82	FY	0.12	FZ	-4.2
329	FX	-18.7	FY	0.06	FZ	-4.16
330	FX	-18.71	FY	0	FZ	-4.16
331	FX	-18.82	FY	-0.06	FZ	-4.16
332	FX	-19.51	FY	-0.19	FZ	-4.38
333	FX	-16.63	FY	-0.24	FZ	-4.2
334	FX	-16.58	FY	-0.29	FZ	-4.22
335	FX	-18.51	FY	-0.35	FZ	-4.21
336	FX	-18.45	FY	-0.4	FZ	-4.32
337	FX	-19.44	FY	-0.48	FZ	-4.53
338	FX	-18.56	FY	-0.4	FZ	-4.37
339	FX	-18.51	FY	-0.47	FZ	-4.34
340	FX	-19.52	FY	-0.56	FZ	-4.79
341	FX	-16.36	FY	-0.66	FZ	-4.76
342	FX	-16.36	FY	-0.7	FZ	-4.51
343	FX	-18.51	FY	-0.75	FZ	-4.38
344	FX	-19.52	FY	-0.82	FZ	-4.8
345	FX	-18.36	FY	-0.82	FZ	-4.33
346	FX	-18.45	FY	-0.87	FZ	-4.32
347	FX	-19.44	FY	-0.93	FZ	-4.53
348	FX	-18.96	FY	-0.93	FZ	-4.37
349	FX	-21.74	FY	-1.15	FZ	-4.61
350	FX	-18.59	FY	-1.04	FZ	-3.19
351	FX	-19	FY	0.69	FZ	-4.49
352	FX	-20.12	FY	0.66	FZ	-4.76
353	FX	-16.36	FY	0.55	FZ	-4.31
354	FX	-18.45	FY	0.51	FZ	-4.3
355	FX	-19.44	FY	0.47	FZ	-4.49
356	FX	-18.56	FY	0.4	FZ	-4.34
357	FX	-18.51	FY	0.35	FZ	-4.2
358	FX	-18.58	FY	0.29	FZ	-4.19
359	FX	-18.52	FY	0.24	FZ	-4.17
360	FX	-19.52	FY	0.19	FZ	-4.35
361	FX	-18.82	FY	0.12	FZ	-4.18
362	FX	-18.7	FY	0.06	FZ	-4.14
363	FX	-18.71	FY	0	FZ	-4.14
364	FX	-18.7	FY	-0.06	FZ	-4.14
365	FX	-18.82	FY	-0.11	FZ	-4.17
366	FX	-19.51	FY	-0.19	FZ	-4.35
367	FX	-16.63	FY	-0.24	FZ	-4.17
368	FX	-16.58	FY	-0.29	FZ	-4.19
369	FX	-18.51	FY	-0.35	FZ	-4.2
370	FX	-19.52	FY	-0.4	FZ	-4.34
371	FX	-19.44	FY	-0.47	FZ	-4.5
372	FX	-18.45	FY	-0.51	FZ	-4.3
373	FX	-18.36	FY	-0.55	FZ	-4.31
374	FX	-20.12	FY	-0.66	FZ	-4.76

Page: 41

Q326-KSP-R4b-Deg.std

042

375	FX	-21.24	FY	-1.16	FZ	-4.56
376	FX	-16.36	FY	-1.06	FZ	-3.16
377	FX	-13.42	FY	-0.82	FZ	-1.98
378	FX	-10.34	FY	0	FZ	-0.64
379	FX	-16.36	FY	1.04	FZ	-3.2
380	FX	-21.23	FY	1.1	FZ	-4.63
381	FX	-18.7	FY	0.93	FZ	-4.21
382	FX	-21.74	FY	0.93	FZ	-5.11
383	FX	-18.59	FY	0.75	FZ	-4.38
384	FX	-19.7	FY	0.69	FZ	-4.51
385	FX	-20.12	FY	0.66	FZ	-4.8
386	FX	-18.36	FY	0.56	FZ	-4.33
387	FX	-18.45	FY	0.51	FZ	-4.32
388	FX	-19.44	FY	0.48	FZ	-4.53
389	FX	-18.96	FY	0.4	FZ	-4.37
390	FX	-18.51	FY	0.35	FZ	-4.22
391	FX	-18.58	FY	0.3	FZ	-4.21
392	FX	-18.63	FY	0.24	FZ	-4.2
393	FX	-19.52	FY	0.19	FZ	-4.38
394	FX	-18.82	FY	0.12	FZ	-4.2
395	FX	-18.7	FY	0.06	FZ	-4.16
396	FX	-18.71	FY	0	FZ	-4.16
397	FX	-18.82	FY	-0.06	FZ	-4.16
398	FX	-19.51	FY	-0.19	FZ	-4.38
399	FX	-16.63	FY	-0.24	FZ	-4.2
400	FX	-16.58	FY	-0.29	FZ	-4.22
401	FX	-18.51	FY	-0.35	FZ	-4.21
402	FX	-18.45	FY	-0.4	FZ	-4.32
403	FX	-19.44	FY	-0.48	FZ	-4.53
404	FX	-18.56	FY	-0.4	FZ	-4.37
405	FX	-18.51	FY	-0.47	FZ	-4.34
406	FX	-19.52	FY	-0.56	FZ	-4.79
407	FX	-16.36	FY	-0.66	FZ	-4.76
408	FX	-16.36	FY	-0.7	FZ	-4.51
409	FX	-18.51	FY	-0.75	FZ	-4.38
410	FX	-19.52	FY	-0.82	FZ	-4.8
411	FX	-18.36	FY	-0.82	FZ	-4.33
412	FX	-18.45	FY	-0.87	FZ	-4.32
413	FX	-19.44	FY	-0.93	FZ	-4.53
414	FX	-18.96	FY	-0.93	FZ	-4.37
415	FX	-21.74	FY	-1.15	FZ	-4.61
416	FX	-18.59	FY	-1.04	FZ	-3.19
417	FX	-19	FY	0.69	FZ	-4.49
418	FX	-20.12	FY	0.66	FZ	-4.76
419	FX	-16.36	FY	0.55	FZ	-4.31
420	FX	-18.45	FY	0.51	FZ	-4.3
421	FX	-19.44	FY	0.47	FZ	-4.49
422	FX	-18.56	FY	0.4	FZ	-4.34
423	FX	-18.51	FY	0.35	FZ	-4.2
424	FX	-18.58	FY	0.29	FZ	-4.19
425	FX	-18.52	FY	0.24	FZ	-4.17
426	FX	-19.52	FY	0.19	FZ	-4.35
427	FX	-18.82	FY	0.12	FZ	-4.18
428	FX	-18.7	FY	0.06	FZ	-4.14
429	FX	-18.71	FY	0	FZ	-4.14
430	FX	-18.7	FY	-0.06	FZ	-4.14
431	FX	-18.82	FY	-0.11	FZ	-4.17
432	FX	-19.51	FY	-0.19	FZ	-4.35
433	FX	-16.63	FY	-0.24	FZ	-4.17
434	FX	-16.58	FY	-0.29	FZ	-4.19
435	FX	-18.51	FY	-0.35	FZ	-4.2
436	FX	-19.52	FY	-0.4	FZ	-4.34
437	FX	-19.44	FY	-0.47	FZ	-4.5
438	FX	-18.45	FY	-0.51	FZ	-4.3
439	FX	-18.36	FY	-0.55	FZ	-4.31
440	FX	-20.12	FY	-0.66	FZ	-4.76
441	FX	-16.36	FY	-0.66	FZ	-4.76
442	FX	-16				

Q326-KSP-R4b-Deg.std 278 FX -20.65 FY 1.53 FZ -4.72 ... 390 FX -158.66 FY -69.81 FZ 68.08

Page: 48

Q326-KSP-R4b-Deg.std 498 FX -16.8 FX -2.39 FZ 12.63 ... 390 FX -158.66 FY -69.81 FZ 68.08

Page: 52

Q326-KSP-R4b-Deg.std 273 FX 158.79 FY -70.11 FZ 68.31 ... 390 FX -158.66 FY -69.81 FZ 68.08

Page: 49

Q326-KSP-R4b-Deg.std 528 FX 11.25 FY -0.25 FZ 3.3 ... 390 FX -158.66 FY -69.81 FZ 68.08

Page: 53

Q326-KSP-R4b-Deg.std 430 FX -107.25 FY 56.44 FZ 32.89 ... 390 FX -158.66 FY -69.81 FZ 68.08

Page: 50

Q326-KSP-R4b-Deg.std 59 FX 2.39 FY -0.25 FZ 0.46 ... 390 FX -158.66 FY -69.81 FZ 68.08

Page: 54

Q326-KSP-R4b-Deg.std 347 FX 14.78 FY 2.85 FZ 2.45 ... 390 FX -158.66 FY -69.81 FZ 68.08

Page: 51

Q326-KSP-R4b-Deg.std 94 FX 22.58 FY -2.73 FZ 4.92 ... 390 FX -158.66 FY -69.81 FZ 68.08

Page: 55



Table with 2 columns: Data values and reference ID '456'. Rows include various numerical data points with units like 'FY' and 'FZ'.

456

Table with 2 columns: Data values and reference ID '457'. Rows include various numerical data points with units like 'FY' and 'FZ'.

457

Table with 2 columns: Data values and reference ID '458'. Rows include various numerical data points with units like 'FY' and 'FZ'.

458

Table with 2 columns: Data values and reference ID '459'. Rows include various numerical data points with units like 'FY' and 'FZ'.

459

Table with 2 columns: Data values and reference ID '460'. Rows include various numerical data points with units like 'FY' and 'FZ'.

460

Table with 2 columns: Data values and reference ID '461'. Rows include various numerical data points with units like 'FY' and 'FZ'.

461

Table with 2 columns: Data values and reference ID '462'. Rows include various numerical data points with units like 'FY' and 'FZ'.

462

Table with 2 columns: Data values and reference ID '463'. Rows include various numerical data points with units like 'FY' and 'FZ'.

463

Q326-KSP-R4b-Deg.std
255 FX 18.7 FY -0.06 FZ -4.16
256 FX 18.82 FY -0.12 FZ -4.2

Q326-KSP-R4b-Deg.std
329 FX 19.52 FY 0.19 FZ -4.38
330 FX 18.82 FY 0.15 FZ -4.2

Q326-KSP-R4b-Deg.std
474 FX -9.76 FY 1.25 FZ 3.89
475 FX -11.11 FY 1.05 FZ 3.93

Q326-KSP-R4b-Deg.std
394 FX 8.09 FY 0.27 FZ -4.6
395 FX 5.76 FY 0.15 FZ -3.37

Q326-KSP-R4b-Deg.std
32 FX -12.83 FY 0.92 FZ -3.73
33 FX -13.78 FY 0.93 FZ -4.39

Q326-KSP-R4b-Deg.std
152 FX -8.16 FY 2.08 FZ 1.62
153 FX -7.78 FY 1.46 FZ 1.37

Q326-KSP-R4b-Deg.std
226 FX -14.18 FY 2.08 FZ 3.09
227 FX -12.41 FY 2.01 FZ 2.69

Q326-KSP-R4b-Deg.std
300 FX -16.48 FY 1.49 FZ 3.84
301 FX -16.23 FY 1.7 FZ 3.75

Q326-KSP-R4b-Deg.std
374 FX -17.8 FY 0.67 FZ 4.26
375 FX -17.08 FY 0.87 FZ 4.08
376 FX -16.91 FY 1.08 FZ 4.03
377 FX -16.58 FY 1.27 FZ 3.92
378 FX -16.18 FY 1.49 FZ 3.84
379 FX -16.23 FY 1.7 FZ 3.75
380 FX -15.03 FY 1.79 FZ 3.45
381 FX -14.28 FY 1.79 FZ 3.23
382 FX -14.18 FY 2.08 FZ 3.09
383 FX -12.11 FY 2.01 FZ 2.69
384 FX -11 FY 1.9 FZ 2.32
385 FX -10.37 FY 1.52 FZ 2.09
386 FX -8.16 FY 1.57 FZ 1.62
387 FX -7.78 FY 1.46 FZ 1.37
388 FX -6.34 FY 1.13 FZ 1.05
389 FX -9.76 FY 0.81 FZ 0.73
236 FX 9.77 FY -0.84 FZ 0.73
237 FX 8.36 FY -1.13 FZ 1.02
238 FX 7.76 FY -1.48 FZ 1.37
239 FX 8.16 FY -1.57 FZ 1.6
240 FX 10.39 FY -1.93 FZ 2.08
241 FX 10.97 FY -1.93 FZ 2.03
242 FX 12.42 FY -2.01 FZ 2.68
243 FX 14.27 FY -2.1 FZ 3.12
244 FX 14.31 FY -1.9 FZ 3.23
245 FX 15.06 FY -1.79 FZ 3.45
246 FX 16.25 FY -1.7 FZ 3.74
247 FX 16.47 FY -1.49 FZ 3.85
248 FX 16.58 FY -1.27 FZ 3.92
249 FX 16.93 FY -1.07 FZ 4.02
250 FX 17.08 FY -0.87 FZ 4.09
251 FX 17.81 FY -0.67 FZ 4.25
252 FX 17.44 FY -0.43 FZ 4.2
253 FX 17.46 FY -0.21 FZ 4.21
254 FX 17.5 FY 0 FZ 4.22
255 FX 17.46 FY 0.21 FZ 4.21
256 FX 17.45 FY 0.44 FZ 4.2
257 FX 17.46 FY 0.67 FZ 4.26
258 FX 17.08 FY 0.87 FZ 4.09
259 FX 16.91 FY 1.08 FZ 4.02
260 FX 16.58 FY 1.27 FZ 3.92
261 FX 16.48 FY 1.49 FZ 3.84
262 FX 16.24 FY 1.7 FZ 3.74
263 FX 15.05 FY 1.79 FZ 3.44
264 FX 14.31 FY 1.9 FZ 3.23
265 FX 14.31 FY 2.11 FZ 3.12
266 FX 12.41 FY 2.01 FZ 2.68
267 FX 10.98 FY 1.91 FZ 2.32
268 FX 10.37 FY 1.52 FZ 2.08
269 FX 8.16 FY 1.57 FZ 1.6
270 FX 7.78 FY 1.48 FZ 1.36
271 FX 6.34 FY 1.13 FZ 1.02
272 FX 9.63 FY 0.77 FZ 0.66
***RS=INT=SU
430 FX =92.02 FY 99.82 FZ 91.63
460 FX =221.81 FY =99.81 FZ 91.67
313 FX 221.74 FY 99.55 FZ 91.75
351 FX 221.94 FY =99.96 FZ 91.45
431 FX =9.49 FY -0.77 FZ 0.71
432 FX =6.16 FY -1.1 FZ 1.61
433 FX =7.75 FY -1.47 FZ 1.39
434 FX =8.16 FY -1.57 FZ 1.62
435 FX =10.39 FY -1.93 FZ 2.08
436 FX =10.97 FY -1.93 FZ 2.03
437 FX =12.42 FY -2.01 FZ 2.67
438 FX =14.15 FY -2.09 FZ 3.1
439 FX =14.28 FY -1.9 FZ 3.23
440 FX =15.06 FY -1.79 FZ 3.45
441 FX =16.25 FY -1.7 FZ 3.74
442 FX =16.47 FY -1.49 FZ 3.85
443 FX =16.58 FY -1.27 FZ 3.92
444 FX =16.93 FY -1.07 FZ 4.02
445 FX =17.08 FY -0.87 FZ 4.09
446 FX =17.81 FY -0.67 FZ 4.25
447 FX =17.44 FY -0.43 FZ 4.2
448 FX =17.46 FY -0.21 FZ 4.21
449 FX =17.5 FY 0 FZ 4.22
450 FX =17.46 FY 0.21 FZ 4.21
451 FX =17.45 FY 0.44 FZ 4.2
452 FX =17.46 FY 0.67 FZ 4.26
453 FX =17.08 FY 0.87 FZ 4.09
454 FX =16.91 FY 1.08 FZ 4.02
455 FX =16.58 FY 1.27 FZ 3.92
456 FX =16.48 FY 1.49 FZ 3.84
457 FX =16.24 FY 1.7 FZ 3.74
458 FX =15.05 FY 1.79 FZ 3.44
459 FX =14.31 FY 1.9 FZ 3.23
460 FX =14.31 FY 2.11 FZ 3.12
461 FX =12.41 FY 2.01 FZ 2.68
462 FX =10.98 FY 1.91 FZ 2.32
463 FX =10.37 FY 1.52 FZ 2.08
464 FX =8.16 FY 1.57 FZ 1.6
465 FX =7.78 FY 1.48 FZ 1.36
466 FX =6.34 FY 1.13 FZ 1.02
467 FX =9.63 FY 0.77 FZ 0.66

LOAD 13 LOADTYPE Wind TITLE LOAD CASE 13 - WSB_U
Joints: 1000
***RS=EDGE-SBOARD=SU
429 FX 0.21 FY 0.08 FZ 0.01
491 FX 0.21 FY -0.08 FZ 0.01
472 FX -6.22 FY 6.83 FZ 8.17
476 FX -10.47 FY 3.61 FZ 8.28
481 FX -14.15 FY -2.49 FZ 8.3
484 FX -14.8 FY 1.5 FZ 9.82
488 FX -15.45 FY 0 FZ 10.18
492 FX -16.71 FY -1.51 FZ 9.82
496 FX -12.75 FY -4.56 FZ 9.59
500 FX -10.15 FY -3.51 FZ 8.25
504 FX -6.05 FY -6.12 FZ 8.14
428 FX 5.31 FY 0.23 FZ -2.58
427 FX 6.39 FY 0.43 FZ -2.51
426 FX 8.21 FY 0.6 FZ -2.86
Page: 80

Q326-KSP-R4b-Deg.std
448 FX -17.46 FY -0.21 FZ 2.32
449 FX -17.5 FY 0.43 FZ 2.09
450 FX -17.46 FY 0.21 FZ 4.22
451 FX -17.45 FY 0.43 FZ 4.19
452 FX -17.48 FY 0.67 FZ 4.26
453 FX -17.08 FY 0.87 FZ 4.09
454 FX -16.91 FY 1.08 FZ 4.03
455 FX -16.58 FY 1.27 FZ 3.92
456 FX -16.48 FY 1.49 FZ 3.84
457 FX -16.23 FY 1.7 FZ 3.75
458 FX -15.03 FY 1.79 FZ 3.45
459 FX -14.28 FY 1.9 FZ 3.23
460 FX -14.18 FY 2.08 FZ 3.09
461 FX -12.11 FY 2.01 FZ 2.69
462 FX -11 FY 1.9 FZ 2.32
463 FX -10.37 FY 1.92 FZ 2.09
464 FX -8.16 FY 1.57 FZ 1.62
465 FX -7.78 FY 1.46 FZ 1.37
466 FX -6.34 FY 1.13 FZ 1.05
467 FX -9.76 FY 0.81 FZ 0.73
314 FX 9.77 FY -0.84 FZ 0.73
315 FX 8.36 FY -1.13 FZ 1.02
316 FX 7.76 FY -1.48 FZ 1.37
317 FX 8.16 FY -1.57 FZ 1.6
318 FX 10.39 FY -1.93 FZ 2.08
319 FX 10.97 FY -1.93 FZ 2.03
320 FX 12.42 FY -2.01 FZ 2.68
321 FX 14.27 FY -2.1 FZ 3.12
322 FX 14.31 FY -1.9 FZ 3.23
323 FX 15.06 FY -1.79 FZ 3.45
324 FX 16.25 FY -1.7 FZ 3.74
325 FX 16.47 FY -1.49 FZ 3.85
326 FX 16.58 FY -1.27 FZ 3.92
327 FX 16.93 FY -1.07 FZ 4.02
328 FX 17.08 FY -0.87 FZ 4.09
329 FX 17.81 FY -0.67 FZ 4.25
330 FX 17.44 FY -0.43 FZ 4.2
331 FX 17.46 FY -0.21 FZ 4.21
332 FX 17.5 FY 0 FZ 4.22
333 FX 17.46 FY 0.21 FZ 4.21
334 FX 17.45 FY 0.44 FZ 4.2
335 FX 17.46 FY 0.67 FZ 4.26
336 FX 17.08 FY 0.87 FZ 4.09
337 FX 16.91 FY 1.08 FZ 4.02
338 FX 16.58 FY 1.27 FZ 3.92
339 FX 16.48 FY 1.49 FZ 3.84
340 FX 16.24 FY 1.7 FZ 3.74
341 FX 15.05 FY 1.79 FZ 3.44
342 FX 14.31 FY 1.9 FZ 3.23
343 FX 14.31 FY 2.11 FZ 3.12
344 FX 12.41 FY 2.01 FZ 2.68
345 FX 10.98 FY 1.91 FZ 2.32
346 FX 10.37 FY 1.52 FZ 2.08
347 FX 8.16 FY 1.57 FZ 1.6
348 FX 7.78 FY 1.48 FZ 1.36
349 FX 6.34 FY 1.13 FZ 1.02
350 FX 9.63 FY 0.77 FZ 0.66

LOAD 13 LOADTYPE Wind TITLE LOAD CASE 13 - WSB_U
Joints: 1000
***RS=EDGE-SBOARD=SU
429 FX 0.21 FY 0.08 FZ 0.01
491 FX 0.21 FY -0.08 FZ 0.01
472 FX -6.22 FY 6.83 FZ 8.17
476 FX -10.47 FY 3.61 FZ 8.28
481 FX -14.15 FY -2.49 FZ 8.3
484 FX -14.8 FY 1.5 FZ 9.82
488 FX -15.45 FY 0 FZ 10.18
492 FX -16.71 FY -1.51 FZ 9.82
496 FX -12.75 FY -4.56 FZ 9.59
500 FX -10.15 FY -3.51 FZ 8.25
504 FX -6.05 FY -6.12 FZ 8.14
428 FX 5.31 FY 0.23 FZ -2.58
427 FX 6.39 FY 0.43 FZ -2.51
426 FX 8.21 FY 0.6 FZ -2.86
Page: 81

Q326-KSP-R4b-Deg.std
425 FX 9.93 FY 0.72 FZ -3.23
426 FX 14.63 FY 0.36 FZ -4.87
427 FX 13.68 FY 0.92 FZ -4.24
428 FX 12.67 FY 0.91 FZ -3.57
429 FX 16.36 FY 1.03 FZ -4.63
430 FX 18.02 FY 1.02 FZ -5.05
431 FX 18.27 FY 0.97 FZ -4.93
432 FX 16.98 FY 1.27 FZ 3.92
433 FX 19.74 FY 0.85 FZ -5.05
434 FX 16.23 FY 1.7 FZ 3.75
435 FX 16.58 FY 1.79 FZ 3.45
436 FX 15.05 FY 1.9 FZ 3.23
437 FX 14.18 FY 2.08 FZ 3.09
438 FX 12.11 FY 2.01 FZ 2.69
439 FX 10.98 FY 1.92 FZ 2.09
440 FX 10.37 FY 1.92 FZ 2.32
441 FX 8.16 FY 1.57 FZ 1.62
442 FX 7.78 FY 1.46 FZ 1.37
443 FX 6.34 FY 1.13 FZ 1.05
444 FX 9.76 FY -0.81 FZ 0.73
445 FX 9.77 FY -0.84 FZ 0.73
446 FX 8.36 FY -1.13 FZ 1.02
447 FX 7.76 FY -1.48 FZ 1.37
448 FX 8.16 FY -1.57 FZ 1.6
449 FX 10.39 FY -1.93 FZ 2.08
450 FX 10.97 FY -1.91 FZ 2.33
451 FX 12.42 FY -2.01 FZ 2.68
452 FX 14.27 FY -2.1 FZ 3.12
453 FX 14.31 FY -1.9 FZ 3.23
454 FX 15.06 FY -1.79 FZ 3.45
455 FX 16.25 FY -1.7 FZ 3.74
456 FX 16.47 FY -1.49 FZ 3.85
457 FX 16.58 FY -1.27 FZ 3.92
458 FX 16.93 FY -1.07 FZ 4.02
459 FX 17.08 FY -0.87 FZ 4.09
460 FX 17.81 FY -0.67 FZ 4.25
461 FX 17.44 FY -0.43 FZ 4.2
462 FX 17.46 FY -0.21 FZ 4.21
463 FX 17.5 FY 0 FZ 4.22
464 FX 17.46 FY 0.21 FZ 4.21
465 FX 17.45 FY 0.44 FZ 4.2
466 FX 17.46 FY 0.67 FZ 4.26
467 FX 17.08 FY 0.87 FZ 4.09
468 FX 16.91 FY 1.08 FZ 4.02
469 FX 16.58 FY 1.27 FZ 3.92
470 FX 16.48 FY 1.49 FZ 3.84
471 FX 16.24 FY 1.7 FZ 3.74
472 FX 15.05 FY 1.79 FZ 3.44
473 FX 14.31 FY 1.9 FZ 3.23
474 FX 14.31 FY 2.11 FZ 3.12
475 FX 12.41 FY 2.01 FZ 2.68
476 FX 10.98 FY 1.91 FZ 2.32
477 FX 10.37 FY 1.52 FZ 2.08
478 FX 8.16 FY 1.57 FZ 1.6
479 FX 7.78 FY 1.48 FZ 1.36
480 FX 6.34 FY 1.13 FZ 1.02
481 FX 9.63 FY 0.77 FZ 0.66

LOAD 13 LOADTYPE Wind TITLE LOAD CASE 13 - WSB_U
Joints: 1000
***RS=EDGE-SBOARD=SU
429 FX 0.21 FY 0.08 FZ 0.01
491 FX 0.21 FY -0.08 FZ 0.01
472 FX -6.22 FY 6.83 FZ 8.17
476 FX -10.47 FY 3.61 FZ 8.28
481 FX -14.15 FY -2.49 FZ 8.3
484 FX -14.8 FY 1.5 FZ 9.82
488 FX -15.45 FY 0 FZ 10.18
492 FX -16.71 FY -1.51 FZ 9.82
496 FX -12.75 FY -4.56 FZ 9.59
500 FX -10.15 FY -3.51 FZ 8.25
504 FX -6.05 FY -6.12 FZ 8.14
428 FX 5.31 FY 0.23 FZ -2.58
427 FX 6.39 FY 0.43 FZ -2.51
426 FX 8.21 FY 0.6 FZ -2.86
Page: 82

Q326-KSP-R4b-Deg.std
543 FX 7.42 FY -1.62 FZ 3.34
544 FX -5 FY 0 FZ 0
545 FX -5.71 FY 0.18 FZ -3.42
546 FX -7.93 FY 0.25 FZ -4.61
547 FX -7 FY 0.28 FZ -5.53
548 FX -10.06 FY 0.36 FZ -6.13
549 FX -9.62 FY 0.35 FZ -6.91
550 FX -14.74 FY 0.44 FZ -7.46
551 FX -11.96 FY 0.37 FZ -7.41
552 FX -11.54 FY 0.37 FZ -8.26
553 FX -12.11 FY 0.33 FZ -7.64
554 FX -13.12 FY 0.31 FZ -8.28
555 FX -13.22 FY 0.28 FZ -8.41
556 FX -13.27 FY 0.25 FZ -8.51
557 FX -13.53 FY 0.22 FZ -8.68
558 FX -13.73 FY 0.17 FZ -8.75
559 FX -14.58 FY 0.14 FZ -9.39
560 FX -14.19 FY 0.09 FZ -9.19
561 FX -14.12 FY 0.05 FZ -9.12
562 FX -14.17 FY 0 FZ -9.11
563 FX -14.12 FY -0.05 FZ -9.12
564 FX -14.27 FY -0.09 FZ -9.19
565 FX -14.57 FY -0.14 FZ -9.39
566 FX -13.75 FY -0.17 FZ -9.81
567 FX -13.56 FY -0.22 FZ -8.7
568 FX -13.27 FY -0.25 FZ -8.51
569 FX -13.24 FY -0.27 FZ -8.41
570 FX -13.17 FY -0.31 FZ -8.31
571 FX -12.12 FY -0.33 FZ -7.65
572 FX -11.98 FY -0.34 FZ -7.29
573 FX -12.02 FY -0.36 FZ -7.44
574 FX -10.63 FY -0.34 FZ -6.5
575 FX -9.87 FY -0.35 FZ -6.92
576 FX -10.18 FY -0.37 FZ -6.21
577 FX -8.77 FY -0.25 FZ -6.6
578 FX -8.07 FY -0.26 FZ -4.69
579 FX -9.69 FY -0.2 FZ -3.43
580 FX -11.13 FY -0.13 FZ 3.23
581 FX 9.91 FY 2.19 FZ 3.66
582 FX 9.83 FY 1.49 FZ 3.61
583 FX 9.83 FY 1.49 FZ 3.61
584 FX 10.01 FY 0.88 FZ 3.91
585 FX 9.66 FY 0.96 FZ 3.78
586 FX 11.05 FY 0.34 FZ 4.12
587 FX 12.09 FY 1.42 FZ 4.15
588 FX 13.66 FY 0.59 FZ 4.43
589 FX 13.77 FY 0.59 FZ 4.43
590 FX 14.67 FY 0.18 FZ 4.25
591 FX 15.47 FY 0.45 FZ 4.55
592 FX 14.72 FY 2.52 FZ 4.57
593 FX 15.65 FY 0.08 FZ 4.37
594 FX 16.16 FY 0.34 FZ 4.71
595 FX 15.53 FY 0.04 FZ 4.3
596 FX 15.53 FY -0.04 FZ 4.3
597 FX 16.37 FY 0.06 FZ 4.72
598 FX 15.64 FY -0.08 FZ 4.27
599 FX 14.76 FY -2.53 FZ 4.6
600 FX 15.41 FY -0.45 FZ 4.62
601 FX 14.48 FY -0.18 FZ 4.25
602 FX 13.47 FY -0.14 FZ 4.19
603 FX 13.7 FY -0.59 FZ 4.45
604 FX 12.16 FY -1.41 FZ 4.19
605 FX 12.13 FY -1.34 FZ 4.16
606 FX 9.74 FY -0.96 FZ 3.83
607 FX 10.14 FY -0.87 FZ 3.98
608 FX 9.83 FY -0.81 FZ 4.03
609 FX 5.77 FY -1.49 FZ 3.59
610 FX 4 FY -2.19 FZ 3.69

IMP=SU
118 FX -26.18 FY 15.94 FZ 9.12
119 FX -26.17 FY -15.92 FZ 9.11
120 FX 26.23 FY 16.65 FZ 9.69
40 FX 26.23 FY 16.65 FZ 9.69
118 FX -26.18 FY 15.94 FZ 9.12
119 FX -26.17 FY -15.92 FZ 9.11
120 FX 26.23 FY 16.65 FZ 9.69
Page: 83

Q326-KSP-R4b-Deg.std
121 FX -21.23 FY 1.17 FZ -4.56
122 FX -18.7 FY 0.93 FZ -4.19
123 FX -21.75 FY 0.92 FZ -5.06
124 FX -18.59 FY 0.74 FZ -4.36
125 FX -18 FY 0.69 FZ -4.49
126 FX -20.12 FY 0.66 FZ -4.76
127 FX -18.36 FY 0.55 FZ -4.31
128 FX -18.45 FY 0.51 FZ -4.3
129 FX -19.44 FY 0.47 FZ -4.49
130 FX -18.96 FY 0.4 FZ -4.34
131 FX -18.51 FY 0.35 FZ -4.2
132 FX -18.58 FY 0.29 FZ -4.19
133 FX -18.63 FY 0.24 FZ -4.17
134 FX -19.52 FY 0.19 FZ -4.35
135 FX -18.82 FY 0.12 FZ -4.18
136 FX -18.7 FY 0.06 FZ -4.14
137 FX -18.71 FY 0 FZ -4.14
138 FX -18.7 FY -0.06 FZ -4.14
139 FX -18.82 FY -0.11 FZ -4.17
140 FX -19.51 FY -0.19 FZ -4.35
141 FX -18.63 FY -0.24 FZ -4.17
142 FX -18.58 FY -0.29 FZ -4.19
143 FX -18.51 FY -0.35 FZ -4.2
144 FX -18.96 FY -0.4 FZ -4.34
145 FX -19.44 FY -0.47 FZ -4.5
146 FX -18.45 FY -0.51 FZ -4.3
147 FX -18.36 FY -0.55 FZ -4.31
148 FX -20.12 FY -0.65 FZ -4.76
149 FX -18.99 FY -0.69 FZ -4.49
150 FX -18.59 FY -0.74 FZ -4.36
151 FX -21.74 FY -0.93 FZ -5.06
152 FX -18.7 FY -0.93 FZ -4.19
153 FX -21.24 FY -1.16 FZ -4.56
154 FX -16.36 FY -1.06 FZ -3.16
155 FX -11.42 FY -0.82 FZ -1.98
41 FX 11.34 FY 0.8 FZ -2.04
42 FX 16.36 FY 1.04 FZ -3.2
43 FX 21.23 FY 1.15 FZ 4.61
44 FX 18.7 FY 0.93 FZ -4.21
45 FX 21.74 FY 0.93 FZ -5.11
46 FX 18.59 FY 0.75 FZ -4.38
47 FX 19 FY 0.69 FZ -4.51
48 FX 20.12 FY 0.66 FZ -4.8
49 FX 18.36 FY 0.56 FZ -4.33
50 FX 18.45 FY 0.51 FZ -4.32
51 FX 18.44 FY 0.48 FZ -4.53
52 FX 18.96 FY 0.4 FZ -4.37
53 FX 18.51 FY 0.35 FZ -4.22
54 FX 18.58 FY 0.3 FZ -4.21
55 FX 18.63 FY 0.24 FZ -4.2
56 FX 19.52 FY 0.15 FZ -4.38
57 FX 18.7 FY 0.12 FZ -4.2
58 FX 18.7 FY 0.06 FZ -4.16
59 FX 18.71 FY 0 FZ -4.14
60 FX 18.7 FY -0.06 FZ -4.16
61 FX 18.82 FY -0.12 FZ -4.2
62 FX 19.51 FY -0.19 FZ -4.38
63 FX 18.63 FY -0.24 FZ -4.2
64 FX 18.58 FY -0.3 FZ -4.21
65 FX 18.51 FY -0.35 FZ -4.23
66 FX 18.96 FY -0.41 FZ -4.37
67 FX 19.44 FY -0.48 FZ -4.53
68 FX 18.45 FY -0.52 FZ -4.32
69 FX 18.36 FY -0.56 FZ -4.33
70 FX 20.12 FY -0.66 FZ -4.79
71 FX 18.99 FY -0.7 FZ -4.51
72 FX 18.59 FY -0.75 FZ -4.38
73 FX 21.74 FY -0.93 FZ -5.11
74 FX 18.7 FY -0.93 FZ -4.21
75 FX 21.24 FY -1.15 FZ -4.61
76 FX 16.35 FY -1.04 FZ -3.19
77 FX 11.37 FY -0.77 FZ -2

IMP=SU
196 FX -26.18 FY 15.94 FZ 9.12
234 FX -26.17 FY -15.92 FZ 9.11
Page: 84

Q326-KSP-R4b-Deg.std
79 FX 26.23 FY 16.65 FZ 9.69
121 FX -21.23 FY 1.17 FZ -4.56
122 FX -18.7 FY 0.93 FZ -4.19
123 FX -21.75 FY 0.92 FZ -5.06
124 FX -18.59 FY 0.74 FZ -4.36
125 FX -18 FY 0.69 FZ -4.49
126 FX -20.12 FY 0.66 FZ -4.76
127 FX -18.36 FY 0.55 FZ -4.31
128 FX -18.45 FY 0.51 FZ -4.3
129 FX -19.44 FY 0.47 FZ -4.49
130 FX -18.96 FY 0.4 FZ -4.34
131 FX -18.51 FY 0.35 FZ -4.2
132 FX -18.58 FY 0.29 FZ -4.19
133 FX -18.63 FY 0.24 FZ -4.17
134 FX -19.52 FY 0.19 FZ -4.35
135 FX -18.82 FY 0.12 FZ -4.18
136 FX -18.7 FY 0.06 FZ -4.14
137 FX -18.71 FY 0 FZ -4.14
138 FX -18.7 FY -0.06 FZ -4.14
139 FX -18.82 FY -0.11 FZ -4.17
140 FX -19.51 FY -0.19 FZ -4.35
141 FX -18.63 FY -0.24 FZ -4.17
142 FX -18.58 FY -0.29 FZ -4.19
143 FX -18.51 FY -0.35 FZ -4.2
144 FX -18.96 FY -0.4 FZ -4.34
145 FX -19.44 FY -0.47 FZ -4.5
146 FX -18.45 FY -0.51 FZ -4.3
147 FX -18.36 FY -0.55 FZ -4.31
148 FX -20.12 FY -0.65 FZ -4.76
149 FX -18.99 FY -0.69 FZ -4.49
150 FX -18.59 FY -0.74 FZ -4.36
151 FX -21.74 FY -0.93 FZ -5.06
152 FX -18.7 FY -0.93 FZ -4.19
153 FX -21.24 FY -1.16 FZ -4.56
154 FX -16.36 FY -1.06 FZ -3.16
155 FX -11.42 FY -0.82 FZ -1.98
41 FX 11.34 FY 0.8 FZ -2.04
42 FX 16.36 FY 1.04 FZ -3.2
43 FX 21.23 FY 1.15 FZ 4.61
44 FX 18.7 FY 0.93 FZ -4.21
45 FX 21.74 FY 0.93 FZ -5.11
46 FX 18.59 FY 0.75 FZ -4.38
47 FX 19 FY 0.69 FZ -4.51
48 FX 20.12 FY 0.66 FZ -4.8
49 FX 18.36 FY 0.56 FZ -4.33
50 FX 18.45 FY 0.51 FZ -4.32
51 FX 18.44 FY 0.48 FZ -4.53
52 FX 18.96 FY 0.4 FZ -4.37
53 FX 18.51 FY 0.35 FZ -4.22
54 FX 18.58 FY 0.3 FZ -4.21
55 FX 18.63 FY 0.24 FZ -4.2
56 FX 19.52 FY 0.15 FZ -4.38
57 FX 18.7 FY 0.12 FZ -4.2
58 FX 18.7 FY 0.06 FZ -4.16
59 FX 18.71 FY 0 FZ -4.14
60 FX 18.7 FY -0.06 FZ -4.16
61 FX 18.82 FY -0.12 FZ -4.2
62 FX 19.51 FY -0.19 FZ -4.38
63 FX 18.63 FY -0.24 FZ -4.2
64 FX 18.58 FY -0.3 FZ -4.21
65 FX 18.51 FY -0.35 FZ -4.23
66 FX 18.96 FY -0.41 FZ -4.37
67 FX 19.44 FY -0.48 FZ -4.53
68 FX 18.45 FY -0.52 FZ -4.32
69 FX 18.36 FY -0.56 FZ -4.33
70 FX 20.12 FY -0.66 FZ -4.79
71 FX 18.99 FY -0.7 FZ -4.51
72 FX 18.59 FY -0.75 FZ -4.38
73 FX 21.74 FY -0.93 FZ -5.11
74 FX 18.7 FY -0.93 FZ -4.21
75 FX 21.24 FY -1.15 FZ -4.61
76 FX 16.35 FY -1.04 FZ -3.19
77 FX 11.37 FY -0.77 FZ -2

IMP=SU
196 FX -26.18 FY 15.94 FZ 9.12
234 FX -26.17 FY -15.92 FZ 9.11
Page: 85

Q326-KSP-R4b-Deg.std
116 FX -11.37 FY -0.77 FZ -2
117 FX 26.23 FY -16.66 FZ 9.69
274 FX -26.18 FY 15.94 FZ 9.12
312 FX -26.17 FY -15.92 FZ 9.11
157 FX 26.23 FY 16.65 FZ 9.69
195 FX 26.23 FY -16.66 FZ 9.69
235 FX -11.38 FY 0.8 FZ -2.95
276 FX -16.36 FY 1.05 FZ -4.63
277 FX -21.23 FY 1.17 FZ -4.56
278 FX -18.7 FY 0.93 FZ -4.19
279 FX -21.75 FY 0.92 FZ -5.06
280 FX -18.59 FY 0.74 FZ -4.36
281 FX -18.45 FY 0.69 FZ -4.49
282 FX -20.12 FY 0.66 FZ -4.76
283 FX -18.36 FY 0.55 FZ -4.31
284 FX -18.45 FY 0.51 FZ -4.3
285 FX -19.44 FY 0.47 FZ -4.49
286 FX -18.96 FY 0.4 FZ -4.34
287 FX -18.51 FY 0.35 FZ -4.2
288 FX -18.58 FY 0.29 FZ -4.19
289 FX -18.63 FY 0.24 FZ -4.17
290 FX -19.52 FY 0.19 FZ -4.35
291 FX -18.82 FY 0.12 FZ -4.18
292 FX -18.7 FY 0.06 FZ -4.14
293 FX -18.71 FY 0 FZ -4.14
294 FX -18.7 FY -0.06 FZ -4.14
295 FX -18.82 FY -0.11 FZ -4.17
296 FX -19.51 FY -0.19 FZ -4.35
297 FX -18.63 FY -0.24 FZ -4.17
298 FX -18.58 FY -0.29 FZ -4.19
299 FX -18.51 FY -0.35 FZ -4.2
300 FX -18.96 FY -0.4 FZ -4.34
301 FX -19.44 FY -0.47 FZ -4.5
302 FX -18.45 FY -0.51 FZ -4.3
303 FX -18

Q326-KSP-R4b-Deg.std
263 FX 18.45 FY -0.52 FZ -4.32
264 FX 18.36 FY -0.56 FZ -4.33
265 FX 20.12 FY -0.56 FZ -4.33
266 FX 18.39 FY 0.7 FZ -4.31

Q326-KSP-R4b-Deg.std
337 FX 18.58 FY -0.3 FZ -4.21
338 FX 18.51 FY -0.35 FZ -4.23
339 FX 18.96 FY -0.41 FZ -4.37
340 FX 18.44 FY -0.48 FZ -4.33

Q326-KSP-R4b-Deg.std
LOAD COMB 209 1.0 (SW+DCN)+1.4 (WSB_U)
1.0 2.0 2.0 1.0 1.4
PERFORM ANALYSIS PRINT STATICS CHECK

Job No TPL40581 Sheet No a 91 Rev R4b-FAB
Job Title Wisma Bella Swimming Pool
Job Information table with columns: Engineer, Checker, Approved.

Reactions table with columns: Node, LC, Horizontal (FX, FY, FZ), Vertical (VX, VY, VZ), Moment (MX, MY, MZ), RE.
776 11LOAD CASE -2.95 -42.87 27.729 8.232 4.429

Reactions Cont... table with columns: Node, LC, Horizontal (FX, FY, FZ), Vertical (VX, VY, VZ), Moment (MX, MY, MZ), RE.
11LOAD CASE -2.95 -42.87 27.729 8.232 4.429

Reactions Cont... table with columns: Node, LC, Horizontal (FX, FY, FZ), Vertical (VX, VY, VZ), Moment (MX, MY, MZ), RE.
11LOAD CASE -2.95 -42.87 27.729 8.232 4.429

Reactions Cont... table with columns: Node, LC, Horizontal (FX, FY, FZ), Vertical (VX, VY, VZ), Moment (MX, MY, MZ), RE.
11LOAD CASE -2.95 -42.87 27.729 8.232 4.429

Job No: TPL40581, Sheet No: a 120, Rev: R4b-FAB2
 Project: Wisma Bella Swimming Pool
 Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - IN MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	REACT/	CRITICAL COMP/	ANZ/	LOADING/
NO	NO	MEMBER	NO	NO	LOCATION
443 ST P192734.0	PAS2	NS-4.8.2.2	0.925	202	
472.45 T	-31.40	0.00	0.00		
444 ST P192734.0	PAS2	NS-4.8.2.2	0.930	202	
489.74 T	-43.13	0.00	1.78		
445 ST P192734.0	PAS2	NS-4.8.2.2	0.752	202	
224.40 T	-21.97	0.00	0.00		
446 ST P192734.0	PAS2	NS-4.8.2.2	0.568	202	
197.40 T	-22.98	0.00	1.78		
447 ST P192734.0	PAS2	NS-4.8.2.2	0.508	202	
181.80 T	-22.95	0.00	0.00		
448 ST P192734.0	PAS2	ANNEX 1.1	0.870	204	
7.70 C	-42.91	0.00	0.00		
449 ST P192734.0	PAS2	ANNEX 1.1	0.870	204	
216.00 C	-24.09	0.00	-		
470 ST P192734.0	PAS2	NS-4.8.2.2	0.562	202	
213.37 T	-28.24	0.00	1.78		
471 ST P192734.0	PAS2	NS-4.8.2.2	0.562	202	
213.14 T	-28.14	0.00	0.00		
472 ST P192734.0	PAS2	NS-4.8.2.2	0.528	204	
335.40 T	-23.17	0.00	0.00		
473 ST P192734.0	PAS2	ANNEX 1.1	0.840	205	
6.00 C	-48.19	0.00	-		
474 ST P192734.0	PAS2	NS-4.8.2.2	0.522	202	
138.85 T	-22.14	0.00	1.78		
475 ST P192734.0	PAS2	NS-4.8.2.2	0.522	202	
131.17 T	-22.14	0.00	0.00		
476 ST P192734.0	PAS2	ANNEX 1.1	0.848	207	
48.20 C	-31.91	0.00	-		
477 ST P192734.0	PAS2	ANNEX 1.1	0.848	207	
88.45 C	-22.84	0.00	-		
478 ST P192734.0	PAS2	NS-4.8.2.2	0.508	202	
131.13 T	-22.14	0.00	1.78		
479 ST P192734.0	PAS2	ANNEX 1.1	0.748	205	
0.00 C	-44.87	0.00	-		
480 ST P192734.0	PAS2	ANNEX 1.1	0.856	205	
1.25 C	-42.12	0.00	-		
481 ST P192734.0	PAS2	NS-4.8.2.2	0.636	205	
124.42 T	-38.87	0.00	0.00		
482 ST P192734.0	PAS2	NS-4.8.2.2	0.508	202	
212.28 T	-22.33	0.00	1.78		
483 ST P192734.0	PAS2	NS-4.8.2.2	0.508	202	
210.27 T	-22.33	0.00	0.00		
484 ST P192734.0	PAS2	ANNEX 1.1	0.871	207	
31.05 C	-22.63	0.00	-		

Job No: TPL40581, Sheet No: a 121, Rev: R4b-FAB2
 Project: Wisma Bella Swimming Pool
 Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - IN MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	REACT/	CRITICAL COMP/	ANZ/	LOADING/
NO	NO	MEMBER	NO	NO	LOCATION
445 ST P192734.0	PAS2	ANNEX 1.1	0.925	208	
184.80 T	-44.13	0.00	-		
446 ST P192734.0	PAS2	NS-4.8.2.2	0.580	202	
180.76 T	-42.80	0.00	1.78		
447 ST P192734.0	PAS2	NS-4.8.2.2	0.588	202	
184.80 T	-42.80	0.00	0.00		
448 ST P192734.0	PAS2	NS-4.8.2.2	0.518	202	
188.20 T	-44.92	0.00	1.78		
449 ST P192734.0	PAS2	NS-4.8.2.2	0.487	202	
471.70 T	-44.20	0.00	0.00		
450 ST P192734.0	PAS2	NS-4.8.2.2	0.499	204	
479.47 T	-42.21	0.00	1.78		
451 ST P192734.0	PAS2	NS-4.8.2.2	0.610	202	
486.45 T	-32.85	0.00	0.00		
452 ST P192734.0	PAS2	NS-4.8.2.2	0.489	202	
485.20 T	-44.94	0.00	1.78		
453 ST P192734.0	PAS2	NS-4.8.2.2	0.489	202	
371.07 T	-30.59	0.00	0.00		
454 ST P192734.0	PAS2	NS-4.8.2.2	0.539	202	
379.76 T	-34.78	0.00	0.00		
455 ST P192734.0	PAS2	NS-4.8.2.2	0.537	202	
378.40 T	-32.78	0.00	1.14		
456 ST P192734.0	PAS2	NS-4.8.2.2	0.520	202	
184.20 T	-32.78	0.00	0.00		
457 ST P192734.0	PAS2	NS-4.8.2.2	0.520	202	
184.20 T	-32.43	0.00	0.00		
458 ST P192734.0	PAS2	NS-4.8.2.2	0.538	202	
184.20 T	-32.17	0.00	1.14		
459 ST P192734.0	PAS2	NS-4.8.2.2	0.539	202	
170.40 T	-32.80	0.00	1.14		
500 ST P192734.0	PAS2	NS-4.8.2.2	0.488	202	
189.37 T	-30.45	0.00	1.14		
501 ST P192734.0	PAS2	NS-4.8.2.2	0.489	202	
484.42 T	-62.64	0.00	0.00		
502 ST P192734.0	PAS2	NS-4.8.2.2	0.487	202	
481.15 T	-52.49	0.00	1.19		
503 ST P192734.0	PAS2	NS-4.8.2.2	0.480	202	
478.20 T	-20.40	0.00	0.00		
504 ST P192734.0	PAS2	NS-4.8.2.2	0.480	202	
480.21 T	-50.31	0.00	1.78		
505 ST P192734.0	PAS2	NS-4.8.2.2	0.727	204	
382.51 T	-48.00	0.00	0.00		
506 ST P192734.0	PAS2	NS-4.8.2.2	0.504	202	
188.20 T	-42.44	0.00	1.19		

Job No: TPL40581, Sheet No: a 122, Rev: R4b-FAB2
 Project: Wisma Bella Swimming Pool
 Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - IN MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	REACT/	CRITICAL COMP/	ANZ/	LOADING/
NO	NO	MEMBER	NO	NO	LOCATION
507 ST P192734.0	PAS2	NS-4.8.2.2	0.558	202	
184.80 T	-42.44	0.00	0.00		
508 ST P192734.0	PAS2	ANNEX 1.1	0.847	206	
7.70 C	-41.84	0.00	-		
509 ST P192734.0	PAS2	NS-4.8.2.2	0.472	204	
123.70 T	-47.84	0.00	0.00		
510 ST P192734.0	PAS2	NS-4.8.2.2	0.388	202	
213.76 T	-28.87	0.00	1.78		
511 ST P192734.0	PAS2	NS-4.8.2.2	0.548	202	
218.14 T	-28.87	0.00	0.00		
512 ST P192734.0	PAS2	NS-4.8.2.2	0.437	204	
184.44 T	-32.48	0.00	1.78		
513 ST P192734.0	PAS2	ANNEX 1.1	0.847	206	
216.00 C	-42.91	0.00	-		
514 ST P192734.0	PAS2	NS-4.8.2.2	0.431	207	
125.24 T	-22.79	0.00	1.78		
515 ST P192734.0	PAS2	NS-4.8.2.2	0.471	202	
134.00 T	-42.70	0.00	0.00		
516 ST P192734.0	PAS2	ANNEX 1.1	0.840	209	
68.10 C	-42.19	0.00	-		
517 ST P192734.0	PAS2	ANNEX 1.1	0.840	209	
68.10 C	-42.19	0.00	-		
518 ST P192734.0	PAS2	NS-4.8.2.2	0.428	207	
134.20 T	-42.44	0.00	1.78		
519 ST P192734.0	PAS2	NS-4.8.2.2	0.428	207	
133.28 T	-42.44	0.00	0.00		
520 ST P192734.0	PAS2	NS-4.8.2.2	0.583	202	
183.40 T	-37.20	0.00	0.00		
521 ST P192734.0	PAS2	NS-4.8.2.2	0.656	205	
122.84 T	-32.00	0.00	0.00		
522 ST P192734.0	PAS2	NS-4.8.2.2	0.588	202	
214.80 T	-30.40	0.00	1.78		
523 ST P192734.0	PAS2	NS-4.8.2.2	0.588	202	
213.60 T	-30.40	0.00	0.00		
524 ST P192734.0	PAS2	ANNEX 1.1	0.843	209	
18.10 C	-42.48	0.00	-		
525 ST P192734.0	PAS2	ANNEX 1.1	0.850	204	
8.42 C	-42.12	0.00	-		
526 ST P192734.0	PAS2	NS-4.8.2.2	0.480	202	
197.58 T	-42.81	0.00	1.78		
527 ST P192734.0	PAS2	NS-4.8.2.2	0.385	202	
197.24 T	-42.42	0.00	0.00		
528 ST P192734.0	PAS2	NS-4.8.2.2	0.725	204	
184.20 T	-47.91	0.00	1.78		

Job No: TPL40581, Sheet No: a 123, Rev: R4b-FAB2
 Project: Wisma Bella Swimming Pool
 Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - IN MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	REACT/	CRITICAL COMP/	ANZ/	LOADING/
NO	NO	MEMBER	NO	NO	LOCATION
529 ST P192734.0	PAS2	NS-4.8.2.2	0.483	202	
478.65 T	-43.24	0.00	0.00		
530 ST P192734.0	PAS2	NS-4.8.2.2	0.588	202	
478.20 T	-28.67	0.00	1.78		
531 ST P192734.0	PAS2	NS-4.8.2.2	0.412	202	
482.45 T	-28.87	0.00	0.00		
532 ST P192734.0	PAS2	NS-4.8.2.2	0.392	202	
484.81 T	-28.87	0.00	1.78		
533 ST P192734.0	PAS2	NS-4.8.2.2	0.458	202	
370.13 T	-31.20	0.00	0.00		
534 ST P192734.0	PAS2	NS-4.8.2.2	0.588	202	
180.24 T	-34.82	0.00	0.00		
535 ST P192734.0	PAS2	NS-4.8.2.2	0.521	202	
180.80 T	-22.20	0.00	0.00		
536 ST P192734.0	PAS2	NS-4.8.2.2	0.528	202	
165.43 T	-22.61	0.00	1.78		
537 ST P192734.0	PAS2	NS-4.8.2.2	0.548	202	
201.20 T	-34.44	0.00	0.00		
538 ST P192734.0	PAS2	NS-4.8.2.2	0.588	202	
18.10 C	-42.48	0.00	-		
539 ST P192734.0	PAS2	NS-4.8.2.2	0.532	204	
18.10 C	-42.48	0.00	-		
540 ST P192734.0	PAS2	NS-4.8.2.2	0.481	202	
16.21 T	-31.24	0.00	1.78		
541 ST P192734.0	PAS2	NS-4.8.2.2	0.384	202	
14.20 T	-31.82	0.00	1.78		
542 ST P192734.0	PAS2	NS-4.8.2.2	0.588	202	
18.10 C	-42.48	0.00	-		
543 ST P192734.0	PAS2	NS-4.8.2.2	0.614	204	
18.10 C	-37.20	0.00	1.78		
544 ST P192734.0	PAS2	NS-4.8.2.2	0.588	202	
18.10 C	-42.48	0.00	-		
545 ST P192734.0	PAS2	NS-4.8.2.2	0.646	207	
20.92 T	-32.80	0.00	0.00		
546 ST P192734.0	PAS2	NS-4.8.2.2	0.470	207	
18.10 C	-42.48	0.00	-		
547 ST P192734.0	PAS2	ANNEX 1.1	0.840	204	
1.25 C	-42.12	0.00	-		
548 ST					

Job No: TPL40581		Sheet No: a 128		Rev: R4b-FAB2	
Software Used in This Project: TBS					
Project Name: Wisma Bella Swimming Pool					
Client: Majlis Perbandaran Kuantan					
Date: 10-Jul-2012 16:43					

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MP NOTE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/FE	CRITICAL COMP/MP	RATIO/MP	LOADING/LOCATION
439 ST	P2099.124.0	PAJG	NS-4.2.2	0.164	207
440 ST	P2099.124.0	PAJG	NS-4.2.2	0.168	207
441 ST	P2099.124.0	PAJG	NS-4.2.2	0.170	207
442 ST	P2099.124.0	PAJG	NS-4.2.2	0.173	207
443 ST	P2099.124.0	PAJG	NS-4.2.2	0.176	207
444 ST	P2099.124.0	PAJG	NS-4.2.2	0.179	207
445 ST	P2099.124.0	PAJG	NS-4.2.2	0.182	207
446 ST	P2099.124.0	PAJG	NS-4.2.2	0.185	207
447 ST	P2099.124.0	PAJG	NS-4.2.2	0.188	207
448 ST	P2099.124.0	PAJG	NS-4.2.2	0.191	207
449 ST	P2099.124.0	PAJG	NS-4.2.2	0.194	207
450 ST	P2099.124.0	PAJG	NS-4.2.2	0.197	207
451 ST	P2099.124.0	PAJG	NS-4.2.2	0.200	207
452 ST	P2099.124.0	PAJG	NS-4.2.2	0.203	207
453 ST	P2099.124.0	PAJG	NS-4.2.2	0.206	207
454 ST	P2099.124.0	PAJG	NS-4.2.2	0.209	207
455 ST	P2099.124.0	PAJG	NS-4.2.2	0.212	207
456 ST	P2099.124.0	PAJG	NS-4.2.2	0.215	207
457 ST	P2099.124.0	PAJG	NS-4.2.2	0.218	207
458 ST	P2099.124.0	PAJG	NS-4.2.2	0.221	207
459 ST	P2099.124.0	PAJG	NS-4.2.2	0.224	207
460 ST	P2099.124.0	PAJG	NS-4.2.2	0.227	207

Job No: TPL40581		Sheet No: a 129		Rev: R4b-FAB2	
Software Used in This Project: TBS					
Project Name: Wisma Bella Swimming Pool					
Client: Majlis Perbandaran Kuantan					
Date: 10-Jul-2012 16:43					

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MP NOTE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/FE	CRITICAL COMP/MP	RATIO/MP	LOADING/LOCATION
461 ST	P2099.124.0	PAJG	NS-4.2.2	0.149	205
462 ST	P2099.124.0	PAJG	NS-4.2.2	0.152	205
463 ST	P2099.124.0	PAJG	NS-4.2.2	0.155	205
464 ST	P2099.124.0	PAJG	NS-4.2.2	0.158	205
465 ST	P2099.124.0	PAJG	NS-4.2.2	0.161	205
466 ST	P2099.124.0	PAJG	NS-4.2.2	0.164	205
467 ST	P2099.124.0	PAJG	NS-4.2.2	0.167	205
468 ST	P2099.124.0	PAJG	NS-4.2.2	0.170	205
469 ST	P2099.124.0	PAJG	NS-4.2.2	0.173	205
470 ST	P2099.124.0	PAJG	NS-4.2.2	0.176	205
471 ST	P2099.124.0	PAJG	NS-4.2.2	0.179	205
472 ST	P2099.124.0	PAJG	NS-4.2.2	0.182	205
473 ST	P2099.124.0	PAJG	NS-4.2.2	0.185	205
474 ST	P2099.124.0	PAJG	NS-4.2.2	0.188	205
475 ST	P2099.124.0	PAJG	NS-4.2.2	0.191	205
476 ST	P2099.124.0	PAJG	NS-4.2.2	0.194	205
477 ST	P2099.124.0	PAJG	NS-4.2.2	0.197	205
478 ST	P2099.124.0	PAJG	NS-4.2.2	0.200	205
479 ST	P2099.124.0	PAJG	NS-4.2.2	0.203	205
480 ST	P2099.124.0	PAJG	NS-4.2.2	0.206	205
481 ST	P2099.124.0	PAJG	NS-4.2.2	0.209	205
482 ST	P2099.124.0	PAJG	NS-4.2.2	0.212	205
483 ST	P2099.124.0	PAJG	NS-4.2.2	0.215	205
484 ST	P2099.124.0	PAJG	NS-4.2.2	0.218	205
485 ST	P2099.124.0	PAJG	NS-4.2.2	0.221	205
486 ST	P2099.124.0	PAJG	NS-4.2.2	0.224	205
487 ST	P2099.124.0	PAJG	NS-4.2.2	0.227	205
488 ST	P2099.124.0	PAJG	NS-4.2.2	0.230	205
489 ST	P2099.124.0	PAJG	NS-4.2.2	0.233	205
490 ST	P2099.124.0	PAJG	NS-4.2.2	0.236	205

Job No: TPL40581		Sheet No: a 130		Rev: R4b-FAB2	
Software Used in This Project: TBS					
Project Name: Wisma Bella Swimming Pool					
Client: Majlis Perbandaran Kuantan					
Date: 10-Jul-2012 16:43					

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MP NOTE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/FE	CRITICAL COMP/MP	RATIO/MP	LOADING/LOCATION
491 ST	P2099.124.0	PAJG	NS-4.2.2	0.139	203
492 ST	P2099.124.0	PAJG	NS-4.2.2	0.142	203
493 ST	P2099.124.0	PAJG	NS-4.2.2	0.145	203
494 ST	P2099.124.0	PAJG	NS-4.2.2	0.148	203
495 ST	P2099.124.0	PAJG	NS-4.2.2	0.151	203
496 ST	P2099.124.0	PAJG	NS-4.2.2	0.154	203
497 ST	P2099.124.0	PAJG	NS-4.2.2	0.157	203
498 ST	P2099.124.0	PAJG	NS-4.2.2	0.160	203
499 ST	P2099.124.0	PAJG	NS-4.2.2	0.163	203
500 ST	P2099.124.0	PAJG	NS-4.2.2	0.166	203
501 ST	P2099.124.0	PAJG	NS-4.2.2	0.169	203
502 ST	P2099.124.0	PAJG	NS-4.2.2	0.172	203
503 ST	P2099.124.0	PAJG	NS-4.2.2	0.175	203
504 ST	P2099.124.0	PAJG	NS-4.2.2	0.178	203
505 ST	P2099.124.0	PAJG	NS-4.2.2	0.181	203
506 ST	P2099.124.0	PAJG	NS-4.2.2	0.184	203
507 ST	P2099.124.0	PAJG	NS-4.2.2	0.187	203
508 ST	P2099.124.0	PAJG	NS-4.2.2	0.190	203
509 ST	P2099.124.0	PAJG	NS-4.2.2	0.193	203
510 ST	P2099.124.0	PAJG	NS-4.2.2	0.196	203
511 ST	P2099.124.0	PAJG	NS-4.2.2	0.199	203
512 ST	P2099.124.0	PAJG	NS-4.2.2	0.202	203
513 ST	P2099.124.0	PAJG	NS-4.2.2	0.205	203
514 ST	P2099.124.0	PAJG	NS-4.2.2	0.208	203
515 ST	P2099.124.0	PAJG	NS-4.2.2	0.211	203
516 ST	P2099.124.0	PAJG	NS-4.2.2	0.214	203
517 ST	P2099.124.0	PAJG	NS-4.2.2	0.217	203
518 ST	P2099.124.0	PAJG	NS-4.2.2	0.220	203
519 ST	P2099.124.0	PAJG	NS-4.2.2	0.223	203
520 ST	P2099.124.0	PAJG	NS-4.2.2	0.226	203

Job No: TPL40581		Sheet No: a 131		Rev: R4b-FAB2	
Software Used in This Project: TBS					
Project Name: Wisma Bella Swimming Pool					
Client: Majlis Perbandaran Kuantan					
Date: 10-Jul-2012 16:43					

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MP NOTE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/FE	CRITICAL COMP/MP	RATIO/MP	LOADING/LOCATION
521 ST	P2099.124.0	PAJG	NS-4.2.2	0.130	201
522 ST	P2099.124.0	PAJG	NS-4.2.2	0.133	201
523 ST	P2099.124.0	PAJG	NS-4.2.2	0.136	201
524 ST	P2099.124.0	PAJG	NS-4.2.2	0.139	201
525 ST	P2099.124.0	PAJG	NS-4.2.2	0.142	201
526 ST	P2099.124.0	PAJG	NS-4.2.2	0.145	201
527 ST	P2099.124.0	PAJG	NS-4.2.2	0.148	201
528 ST	P2099.124.0	PAJG	NS-4.2.2	0.151	201
529 ST	P2099.124.0	PAJG	NS-4.2.2	0.154	201
530 ST	P2099.124.0	PAJG	NS-4.2.2	0.157	201
531 ST	P2099.124.0	PAJG	NS-4.2.2	0.160	201
532 ST	P2099.124.0	PAJG	NS-4.2.2	0.163	201
533 ST	P2099.124.0	PAJG	NS-4.2.2	0.166	201
534 ST	P2099.124.0	PAJG	NS-4.2.2	0.169	201
535 ST	P2099.124.0	PAJG	NS-4.2.2	0.172	201
536 ST	P2099.124.0	PAJG	NS-4.2.2	0.175	201
537 ST	P2099.124.0	PAJG	NS-4.2.2	0.178	201
538 ST	P2099.124.0	PAJG	NS-4.2.2	0.181	201
539 ST	P2099.124.0	PAJG	NS-4.2.2	0.184	201
540 ST	P2099.124.0	PAJG	NS-4.2.2	0.187	201
541 ST	P2099.124.0	PAJG	NS-4.2.2	0.190	201
542 ST	P2099.124.0	PAJG	NS-4.2.2	0.193	201
543 ST	P2099.124.0	PAJG	NS-4.2.2	0.196	201
544 ST	P2099.124.0	PAJG	NS-4.2.2	0.199	201
545 ST	P2099.124.0	PAJG	NS-4.2.2	0.202	201
546 ST	P2099.124.0	PAJG	NS-4.2.2	0.205	201
547 ST	P2099.124.0	PAJG	NS-4.2.2	0.208	201
548 ST	P2099.124.0	PAJG	NS-4.2.2	0.211	201
549 ST	P2099.124.0	PAJG	NS-4.2.2	0.214	201
550 ST	P2099.124.0	PAJG	NS-4.2.2	0.217	201

Job No: TPL40581		Sheet No: a 132		Rev: R4b-FAB2	
Software Used in This Project: TBS					
Project Name: Wisma Bella Swimming Pool					
Client: Majlis Perbandaran Kuantan					
Date: 10-Jul-2012 16:43					

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MP NOTE (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/FE	CRITICAL COMP/MP	RATIO/MP	LOADING/LOCATION
551 ST	P2099.124.0	PAJG	NS-4.2.2	0.110	200
552 ST	P2099.124.0	PAJG	NS-4.2.2	0.113	200
553 ST	P2099.124.0	PAJG	NS-4.2.2	0.116	200
554 ST	P2099.124.0	PAJG	NS-4.2.2	0.119	200
555 ST	P2099.124.0	PAJG	NS-4.2.2	0.122	200
556 ST	P2099.124.0	PAJG	NS-4.2.2	0.125	200
557 ST	P2099.124.0	PAJG	NS-4.2.2	0.128	200
558 ST	P2099.124.0	PAJG	NS-4.2.2	0.131	200
559 ST	P2099.124.0	PAJG	NS-4.2.2	0.134	200
560 ST	P2099.124.0	PAJG	NS-4.2.2	0.137	200
561 ST	P2099.124.0	PAJG	NS-4.2.2	0.140	200
562 ST	P2099.124.0	PAJG	NS-4.2.2	0.143	200
563 ST	P2099.124.0	PAJG	NS-4.2.2	0.146	200
564 ST	P2099.124.0	PAJG	NS-4.2.2	0.149	200
565 ST	P2099.124.0	PAJG	NS-4.2.2	0.152	200
566 ST	P2099.124.0	PAJG	NS-4.2.2	0.155	200
567 ST	P2099.124.0	PAJG	NS-4.2.2	0.158	200
568 ST	P2099.124.0	PAJG	NS-4.2.2	0.161	200
569 ST	P2099.124.0	PAJG	NS-4.2.2	0.164	200
570 ST	P2099.124.0	PAJG	NS-4.2.2	0.167	200
571 ST	P2099.124.0	PAJG	NS-4.2.2	0.170	200
572 ST	P2099.124.0	PAJG	NS-4.2.2	0.173	200
573 ST	P2099.124.0	PAJG	NS-4.2.2	0.176	200
574 ST	P2099.124.0	PAJG	NS-4.2.2	0.179	200
575 ST	P2099.124.0	PAJG	NS-4.2.2	0.182	200
576 ST	P2099.124.0	PAJG	NS-4.2.2	0.185	200
577 ST	P2099.124.0	PAJG	NS-4.2.2	0.188	200
578 ST	P2099.124.0	PAJG	NS-4.2.2	0.191	200
579 ST	P2099.124.0	PAJG	NS-4.2.2	0.194	200
580 ST	P2099.124.0	PAJG	NS-4.2.2	0.197	200

Job No:	
---------	--

NO	ITEM	AMOUNT	CURRANT	UNIT	QTY	PRICE	TOTAL
111	ST	P121194.0	PAGE	RS-4.2.2	0.200	204	40.80
112	ST	P121194.0	PAGE	AMCC 2.1	0.200	204	40.80
113	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
114	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
115	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
116	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
117	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
118	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
119	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
120	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88

NO	ITEM	AMOUNT	CURRANT	UNIT	QTY	PRICE	TOTAL
121	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
122	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
123	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
124	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
125	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
126	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
127	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
128	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
129	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
130	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88

NO	ITEM	AMOUNT	CURRANT	UNIT	QTY	PRICE	TOTAL
131	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
132	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
133	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
134	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
135	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
136	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
137	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
138	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
139	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
140	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88

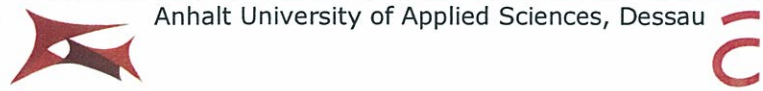
NO	ITEM	AMOUNT	CURRANT	UNIT	QTY	PRICE	TOTAL
141	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
142	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
143	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
144	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
145	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
146	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
147	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
148	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
149	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
150	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88

NO	ITEM	AMOUNT	CURRANT	UNIT	QTY	PRICE	TOTAL
151	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
152	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
153	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
154	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
155	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
156	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
157	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
158	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
159	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
160	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88

NO	ITEM	AMOUNT	CURRANT	UNIT	QTY	PRICE	TOTAL
161	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
162	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
163	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
164	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
165	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
166	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
167	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
168	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
169	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
170	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88

NO	ITEM	AMOUNT	CURRANT	UNIT	QTY	PRICE	TOTAL
171	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
172	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
173	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
174	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
175	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
176	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
177	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
178	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
179	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
180	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88

NO	ITEM	AMOUNT	CURRANT	UNIT	QTY	PRICE	TOTAL
181	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
182	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
183	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
184	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
185	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
186	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
187	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
188	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
189	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88
190	ST	P121194.0	PAGE	RS-4.2.2	0.220	204	44.88



Job No: TPL40581, Sheet No: a 160, Rev: R48-FAB2

Software Used: Staad.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont.

MEMBER	TABLE	REQD/FE	CRITICAL COMP/FE	PATIO/FE	LOADING/LOCATION
1341 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1342 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1343 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1344 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1345 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	

Job No: TPL40581, Sheet No: a 161, Rev: R48-FAB2

Software Used: Staad.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont.

MEMBER	TABLE	REQD/FE	CRITICAL COMP/FE	PATIO/FE	LOADING/LOCATION
1346 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1347 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1348 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1349 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1350 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	

Job No: TPL40581, Sheet No: a 162, Rev: R48-FAB2

Software Used: Staad.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont.

MEMBER	TABLE	REQD/FE	CRITICAL COMP/FE	PATIO/FE	LOADING/LOCATION
1351 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1352 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1353 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1354 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1355 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	

Job No: TPL40581, Sheet No: a 163, Rev: R48-FAB2

Software Used: Staad.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont.

MEMBER	TABLE	REQD/FE	CRITICAL COMP/FE	PATIO/FE	LOADING/LOCATION
1356 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1357 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1358 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1359 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1360 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	

Job No: TPL40581, Sheet No: a 164, Rev: R48-FAB2

Software Used: Staad.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont.

MEMBER	TABLE	REQD/FE	CRITICAL COMP/FE	PATIO/FE	LOADING/LOCATION
1361 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1362 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1363 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1364 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1365 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	

Job No: TPL40581, Sheet No: a 165, Rev: R48-FAB2

Software Used: Staad.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont.

MEMBER	TABLE	REQD/FE	CRITICAL COMP/FE	PATIO/FE	LOADING/LOCATION
1366 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1367 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1368 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1369 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1370 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	

Job No: TPL40581, Sheet No: a 166, Rev: R48-FAB2

Software Used: Staad.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont.

MEMBER	TABLE	REQD/FE	CRITICAL COMP/FE	PATIO/FE	LOADING/LOCATION
1371 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1372 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1373 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1374 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1375 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	

Job No: TPL40581, Sheet No: a 167, Rev: R48-FAB2

Software Used: Staad.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont.

MEMBER	TABLE	REQD/FE	CRITICAL COMP/FE	PATIO/FE	LOADING/LOCATION
1376 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1377 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1378 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1379 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	
1380 ST PIPER.124.8 PAIR	80-4.2,2	0.120	2.00	1.35	



Job No: TPL40581, Sheet No: a 168, Rev: R4b-FAB2

Software Used in this Project: STAAD.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	RESULT/FX	CRITICAL COMP/ F1	NATURAL/ F2	LOADING/ LOCATION
1519	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.242	3
		43.88 C	-0.23	0.23	
1520	ST P1P14-204.5	PAGE	BS-4-2.2	0.228	205
		39.34 T	-0.23	0.23	
1521	ST P1P14-204.5	PAGE	BS-4-2.2	0.216	201
		37.28 T	-0.23	0.23	
1522	ST P1P14-204.5	PAGE	BS-4-2.2	0.222	201
		37.28 T	-0.23	0.23	
1523	ST P1P14-204.5	PAGE	BS-4-2.2	0.247	205
		39.84 T	-0.23	0.23	
1524	ST P1P14-204.5	PAGE	BS-4-2.2	0.208	201
		19.87 T	-0.23	0.23	
1525	ST P1P14-204.5	PAGE	BS-4-2.2	0.191	201
		21.65 T	-0.23	0.23	
1526	ST P1P14-204.5	PAGE	BS-4-2.2	0.202	201
		22.47 C	-0.23	0.23	
1527	ST P1P14-204.5	PAGE	BS-4-2.2	0.232	201
		40.27 T	-0.23	0.23	
1528	ST P1P14-204.5	PAGE	BS-4-2.2	0.193	201
		42.25 T	-0.23	0.23	
1529	ST P1P14-204.5	PAGE	BS-4-2.2	0.138	201
		62.89 T	-0.23	0.23	
1530	ST P1P14-204.5	PAGE	BS-4-2.2	0.132	201
		67.83 C	-0.24	0.24	
1531	ST P1P14-204.5	PAGE	BS-4-2.2	0.140	201
		68.27 T	-0.23	0.23	
1532	ST P1P14-204.5	PAGE	BS-4-2.2	0.114	204
		79.45 T	-0.23	0.23	
1533	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.203	204
		132.82 C	-0.23	0.23	
1534	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	201
		47.84 C	-0.23	0.23	
1535	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.274	2
		85.86 C	-0.23	0.23	
1536	ST P1P14-204.5	PAGE	BS-4-2.2	0.229	204
		88.27 T	-0.23	0.23	
1537	ST P1P14-204.5	PAGE	BS-4-2.2	0.204	204
		78.86 T	-0.23	0.23	
1538	ST P1P14-204.5	PAGE	BS-4-2.2	0.221	204
		79.70 T	-0.23	0.23	
1539	ST P1P14-204.5	PAGE	BS-4-2.2	0.242	204
		86.80 C	-0.23	0.23	
1540	ST P1P14-204.5	PAGE	BS-4-2.2	0.214	204
		76.86 T	-0.23	0.23	

Job No: TPL40581, Sheet No: a 169, Rev: R4b-FAB2

Software Used in this Project: STAAD.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	RESULT/FX	CRITICAL COMP/ F1	NATURAL/ F2	LOADING/ LOCATION
1541	ST P1P14-204.5	PAGE	BS-4-2.2	0.255	204
		88.65 C	-0.23	0.23	
1542	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.148	8
		28.98 C	-0.24	0.24	
1543	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1544	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1545	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1546	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1547	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1548	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1549	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1550	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1551	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1552	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1553	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		45.84 T	-0.23	0.23	
1554	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.219	104
		63.92 C	-0.24	0.24	
1555	ST P1P14-204.5	PAGE	BS-4-2.2	0.222	203
		73.95 C	-0.24	0.24	
1556	ST P1P14-204.5	PAGE	BS-4-2.2	0.216	4
		38.84 C	-0.24	0.24	
1557	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.236	205
		48.33 C	-0.24	0.24	
1558	ST P1P14-204.5	PAGE	BS-4-2.2	0.179	8
		38.90 C	-0.23	0.23	
1559	ST P1P14-204.5	PAGE	BS-4-2.2	0.166	204
		43.71 T	-0.24	0.24	
1560	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.216	202
		43.32 T	-0.23	0.23	
1561	ST P1P14-204.5	PAGE	BS-4-2.2	0.175	202
		43.32 T	-0.23	0.23	
1562	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.191	4
		37.84 C	-0.23	0.23	

Job No: TPL40581, Sheet No: a 170, Rev: R4b-FAB2

Software Used in this Project: STAAD.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	RESULT/FX	CRITICAL COMP/ F1	NATURAL/ F2	LOADING/ LOCATION
1563	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.193	201
		31.80 C	-0.23	0.23	
1564	ST P1P14-204.5	PAGE	BS-4-2.2	0.193	209
		46.59 T	-0.23	0.23	
1565	ST P1P14-204.5	PAGE	BS-4-2.2	0.183	203
		19.20 T	-0.24	0.24	
1566	ST P1P14-204.5	PAGE	BS-4-2.2	0.152	204
		43.41 T	-0.21	0.21	
1567	ST P1P14-204.5	PAGE	BS-4-2.2	0.137	205
		32.48 T	-0.22	0.22	
1568	ST P1P14-204.5	PAGE	BS-4-2.2	0.229	204
		62.16 T	-0.23	0.23	
1569	ST P1P14-204.5	PAGE	BS-4-2.2	0.184	204
		44.93 C	-0.27	0.28	
1570	ST P1P14-204.5	PAGE	BS-4-2.2	0.248	204
		79.69 T	-0.23	0.23	
1571	ST P1P14-204.5	PAGE	BS-4-2.2	0.221	204
		71.58 T	-0.23	0.23	
1572	ST P1P14-204.5	PAGE	BS-4-2.2	0.204	204
		61.31 T	-0.23	0.23	
1573	ST P1P14-204.5	PAGE	BS-4-2.2	0.278	204
		49.16 C	-0.47	0.48	
1574	ST P1P14-204.5	PAGE	BS-4-2.2	0.197	204
		44.64 T	-0.23	0.23	
1575	ST P1P14-204.5	PAGE	BS-4-2.2	0.232	204
		59.56 T	-0.23	0.23	
1576	ST P1P14-204.5	PAGE	BS-4-2.2	0.242	204
		62.88 T	-0.23	0.23	
1577	ST P1P14-204.5	PAGE	BS-4-2.2	0.242	204
		62.88 T	-0.23	0.23	
1578	ST P1P14-204.5	PAGE	BS-4-2.2	0.242	204
		62.88 T	-0.23	0.23	
1579	ST P1P14-204.5	PAGE	BS-4-2.2	0.189	201
		37.89 T	-0.23	0.23	
1580	ST P1P14-204.5	PAGE	BS-4-2.2	0.147	201
		32.88 T	-0.23	0.23	
1581	ST P1P14-204.5	PAGE	BS-4-2.2	0.242	205
		62.88 T	-0.23	0.23	
1582	ST P1P14-204.5	PAGE	BS-4-2.2	0.188	204
		44.81 T	-0.23	0.23	
1583	ST P1P14-204.5	PAGE	BS-4-2.2	0.144	201
		38.57 C	-0.23	0.23	
1584	ST P1P14-204.5	PAGE	BS-4-2.2	0.178	201
		44.25 C	-0.23	0.23	

Job No: TPL40581, Sheet No: a 171, Rev: R4b-FAB2

Software Used in this Project: STAAD.Pro for Windows 20.07.02.15

Job Title: Wisma Bella Swimming Pool

Client: Majlis Perbandaran Kuantan

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MM UNLESS OTHERWISE NOTED


MEMBER	TABLE	RESULT/FX	CRITICAL COMP/ F1	NATURAL/ F2	LOADING/ LOCATION
1585	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.278	9
		56.93 C	-0.23	0.23	
1586	ST P1P14-204.5	PAGE	BS-4-2.2	0.202	204
		41.86 C	-0.23	0.23	
1587	ST P1P14-204.5	PAGE	BS-4-2.2	0.215	204
		48.24 T	-0.23	0.23	
1588	ST P1P14-204.5	PAGE	BS-4-2.2	0.202	204
		46.92 T	-0.23	0.23	
1589	ST P1P14-204.5	PAGE	BS-4-2.2	0.202	204
		46.92 T	-0.23	0.23	
1590	ST P1P14-204.5	PAGE	BS-4-2.2	0.220	201
		46.92 T	-0.23	0.23	
1591	ST P1P14-204.5	PAGE	BS-4-2.2	0.220	201
		46.92 T	-0.23	0.23	
1592	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.276	204
		46.92 T	-0.23	0.23	
1593	ST P1P14-204.5	PAGE	BS-4-2.2	0.173	204
		46.92 T	-0.23	0.23	
1594	ST P1P14-204.5	PAGE	BS-4-2.2	0.200	201
		46.92 T	-0.23	0.23	
1595	ST P1P14-204.5	PAGE	BS-4-2.2	0.214	201
		46.92 T	-0.23	0.23	
1596	ST P1P14-204.5	PAGE	BS-4-2.2	0.201	201
		46.92 T	-0.23	0.23	
1597	ST P1P14-204.5	PAGE	BS-4-2.2	0.202	201
		46.92 T	-0.23	0.23	
1598	ST P1P14-204.5	PAGE	BS-4-2.2	0.201	201
		46.92 T	-0.23	0.23	
1599	ST P1P14-204.5	PAGE	BS-4-2.2	0.201	201
		46.92 T	-0.23	0.23	
1600	ST P1P14-204.5	PAGE	BS-4-2.2	0.201	201
		46.92 T	-0.23	0.23	
1601	ST P1P14-204.5	PAGE	BS-4-2.2	0.201	201
		46.92 T	-0.23	0.23	
1602	ST P1P14-204.5	PAGE	BS-4-2.2.3	0.278	9
		56.93 C	-0.23	0.23	
1603	ST P1P14-204.5	PAGE	BS-4-2.2	0.220	201
		46.92 T	-0.23	0.23	
1604	ST P1P14-204.5	PAGE	BS-4-2.2	0.244	201
		46.92 T	-0.23	0.23	
1605	ST P1P14-204.5	PAGE	BS-4-2.2	0.200	201
		46.92 T	-0.23	0.23	
1606	ST P1P14-204.5	PAGE	BS-4-2.2	0.200	201
		46.92 T	-0.23	0.23	

B Software licensed to Tansone Pte Ltd		Job No TP140581	Sheet No a 184	Rev R4b-FAB2	
Job Title Wisma Bella Swimming Pool Client Majlis Perbandaran Kuantan		P*Wind speed 32.5 m/s R# Fabric RS By TSM Date 17-Dec-11 Chk TSM P# Q326-KSP-R4b-Deg.ald Date/Tm 10-Jul-2012 16:43			
Steel Design (Track 0) Checks Cont. ALL UNITS ARE - IN METE (UNLESS OTHERWISE NOTED)					
MEMBER	TABLE	RESULT/ FX	CRITICAL COMP/ MY	MATIO/ W	LOADING/ LOCATION
1873 ST P31235.0	PAGE	88-4.7	(CI)	0.486	204
189.81 C		-0.93		0.00	1.85
1872 ST P31235.0	PAGE	88-4.2,2		0.493	204
181.48 T		-1.13		0.00	0.40
1873 ST P31235.0	PAGE	88-4.7	(CI)	0.497	204
181.48 T		-1.13		0.00	1.35
1874 ST P31235.0	PAGE	88-4.2,2		0.238	204
94.84 T		-1.13		0.00	1.35
1874 ST P31235.0	PAGE	88-4.2,2		0.473	204
44.00 C		-1.94		0.43	-
1874 ST P31235.0	PAGE	88-4.2,2		0.201	204
44.00 C		-1.94		0.00	-
1875 ST P31235.0	PAGE	88-4.2,2		0.350	204
25.28 T		-1.29		0.00	2.22
1876 ST P31235.0	PAGE	88-4.7	(CI)	0.228	204
55.12 C		-1.10		0.00	0.00
1877 ST P31235.0	PAGE	88-4.7	(CI)	0.176	204
3.24 C		-1.44		0.16	216
1880 ST P31235.0	PAGE	88-4.2,2		0.240	204
45.77 T		-1.40		0.00	3.49
1881 ST P31235.0	PAGE	88-4.7	(CI)	0.471	204
158.28 T		-1.59		0.00	-
1882 ST P31235.0	PAGE	88-4.2		0.209	204
42.00 C		-1.28		0.16	-
1882 ST P31235.0	PAGE	88-4.2		0.236	204
169.87 C		-2.07		0.40	-
1884 ST P31235.0	PAGE	88-4.2,2		0.208	204
4.97 T		-1.22		0.00	1.11
1885 ST P31235.0	PAGE	88-4.7	(CI)	0.304	204
45.76 C		-1.25		0.00	-
1886 ST P31235.0	PAGE	88-4.7	(CI)	0.256	204
168.90 C		-2.07		0.40	-
1887 ST P31235.0	PAGE	88-4.7	(CI)	0.478	204
154.77 C		-1.40		0.00	-
1888 ST P31235.0	PAGE	88-4.7	(CI)	0.351	204
6.76 C		-1.49		0.00	-
1889 ST P31235.0	PAGE	88-4.7	(CI)	0.347	204
91.40 C		-1.13		0.00	1.23
1890 ST P31235.0	PAGE	88-4.7	(CI)	0.159	204
38.41 C		-1.74		1.87	-
1891 ST P31235.0	PAGE	88-4.7	(CI)	0.169	204
6.80 C		-1.24		0.00	-
1892 ST P31235.0	PAGE	88-4.7	(CI)	0.160	204
82.20 C		-1.97		0.00	1.93

B Software licensed to Tansone Pte Ltd		Job No TP140581	Sheet No a 185	Rev R4b-FAB2	
Job Title Wisma Bella Swimming Pool Client Majlis Perbandaran Kuantan		P*Wind speed 32.5 m/s R# Fabric RS By TSM Date 17-Dec-11 Chk TSM P# Q326-KSP-R4b-Deg.ald Date/Tm 10-Jul-2012 16:43			
Steel Design (Track 0) Checks Cont. ALL UNITS ARE - IN METE (UNLESS OTHERWISE NOTED)					
MEMBER	TABLE	RESULT/ FX	CRITICAL COMP/ MY	MATIO/ W	LOADING/ LOCATION
1893 ST P31235.0	PAGE	88-4.2,2		0.223	204
45.17 C		-1.19		0.00	1.27
1894 ST P31235.0	PAGE	88-4.2,2		0.117	204
12.70 T		-1.20		0.00	2.24
1895 ST P31235.0	PAGE	88-4.7	(CI)	0.276	204
31.24 C		-1.27		0.00	1.97
1896 ST P31235.0	PAGE	88-4.7	(CI)	0.274	204
95.24 C		-1.30		0.00	1.97
1897 ST P31235.0	PAGE	88-4.7	(CI)	0.142	207
64.93 C		-1.30		0.74	-
1898 ST P31235.0	PAGE	88-4.7	(CI)	0.193	207
89.27 C		-1.28		0.00	1.02
1899 ST P31235.0	PAGE	88-4.7	(CI)	0.280	207
31.40 C		-1.44		0.00	0.00
1900 ST P31235.0	PAGE	88-4.7	(CI)	0.230	207
74.23 C		-1.40		0.00	1.97
1901 ST P31235.0	PAGE	88-4.2,2		0.120	205
44.29 C		-1.20		0.00	-
1902 ST P31235.0	PAGE	88-4.7	(CI)	0.120	204
6.00 C		-1.24		0.00	-
1903 ST P31235.0	PAGE	88-4.7	(CI)	0.220	204
114.41 C		-1.44		0.00	1.97
1904 ST P31235.0	PAGE	88-4.7	(CI)	0.216	204
122.80 C		-1.20		0.00	1.97
1905 ST P31235.0	PAGE	88-4.7	(CI)	0.137	207
39.22 C		-1.26		0.40	-
1906 ST P31235.0	PAGE	88-4.7	(CI)	0.146	204
78.48 C		-1.40		0.00	1.00
1907 ST P31235.0	PAGE	88-4.7	(CI)	0.146	204
74.93 C		-1.30		0.00	0.00
1908 ST P31235.0	PAGE	88-4.7	(CI)	0.134	204
84.80 C		-1.34		0.40	-
1909 ST P31235.0	PAGE	88-4.7	(CI)	0.110	207
34.80 C		-1.49		0.00	-
1910 ST P31235.0	PAGE	88-4.7	(CI)	0.113	205
42.27 C		-1.49		0.00	-
1911 ST P31235.0	PAGE	88-4.7	(CI)	0.180	204
19.83 C		-1.32		0.00	1.97
1912 ST P31235.0	PAGE	88-4.7	(CI)	0.191	204
89.07 C		-1.15		0.00	1.97
1913 ST P31235.0	PAGE	88-4.7	(CI)	0.168	204
6.80 C		-1.21		0.00	1.87
1914 ST P31235.0	PAGE	88-4.7	(CI)	0.113	207
42.27 C		-1.40		0.00	2.21

B Software licensed to Tansone Pte Ltd		Job No TP140581	Sheet No a 186	Rev R4b-FAB2	
Job Title Wisma Bella Swimming Pool Client Majlis Perbandaran Kuantan		P*Wind speed 32.5 m/s R# Fabric RS By TSM Date 17-Dec-11 Chk TSM P# Q326-KSP-R4b-Deg.ald Date/Tm 10-Jul-2012 16:43			
Steel Design (Track 0) Checks Cont. ALL UNITS ARE - IN METE (UNLESS OTHERWISE NOTED)					
MEMBER	TABLE	RESULT/ FX	CRITICAL COMP/ MY	MATIO/ W	LOADING/ LOCATION
1915 ST P31235.0	PAGE	88-4.7	(CI)	0.117	204
36.28 C		-1.77		2.90	-
1916 ST P31235.0	PAGE	88-4.7	(CI)	0.165	204
13.72 T		-1.34		0.00	0.24
1917 ST P31235.0	PAGE	88-4.2,2		0.184	204
37.51 C		-1.44		0.00	-
1918 ST P31235.0	PAGE	88-4.7	(CI)	0.135	207
150.46 C		-1.26		0.00	1.27
1919 ST P31235.0	PAGE	88-4.7	(CI)	0.174	204
153.72 C		-1.34		0.11	-
1920 ST P31235.0	PAGE	88-4.7	(CI)	0.174	204
153.72 C		-1.34		0.00	1.97
1921 ST P31235.0	PAGE	88-4.7	(CI)	0.229	204
42.84 C		-1.29		0.47	-
1922 ST P31235.0	PAGE	88-4.2,2		0.400	204
158.28 T		-1.24		0.00	2.17
1923 ST P31235.0	PAGE	88-4.2,2		0.311	204
74.86 T		-1.24		0.00	1.97
1924 ST P31235.0	PAGE	88-4.2,2		0.230	204
42.84 T		-1.34		0.00	1.17
1925 ST P31235.0	PAGE	88-4.7	(CI)	0.230	204
42.84 T		-1.34		0.00	0.16
1926 ST P31235.0	PAGE	88-4.7	(CI)	0.461	204
168.00 C		-1.60		0.21	-
1927 ST P31235.0	PAGE	88-4.7	(CI)	0.462	204
154.44 C		-1.61		0.10	-
1928 ST P31235.0	PAGE	88-4.2,2		0.216	204
155.20 T		-1.29		0.00	1.97
1929 ST P31235.0	PAGE	88-4.7	(CI)	0.520	204
122.97 C		-1.34		0.00	0.16
1930 ST P31235.0	PAGE	88-4.7	(CI)	0.599	204
75.84 T		0.00		0.00	0.00
1931 ST P31235.0	PAGE	88-4.7	(CI)	0.447	204
145.31 C		-1.40		0.00	1.25
1932 ST P31235.0	PAGE	88-4.7	(CI)	0.460	204
54.76 T		-1.49		0.00	0.00
1933 ST P31235.0	PAGE	88-4.7	(CI)	0.249	205
288.29 T		0.00		0.40	0.00
1934 ST P31235.0	PAGE	88-4.7	(CI)	0.117	204
39.28 C		-1.20		0.00	0.11
1935 ST P31235.0	PAGE	88-4.7	(CI)	0.436	204
142.80 C		-1.12		0.00	1.87
1936 ST P31235.0	PAGE	88-4.7	(CI)	0.467	204
54.85 T		0.00		0.00	0.00


B Software licensed to Tansone Pte Ltd		Job No TP140581	Sheet No a 187	Rev R4b-FAB2	
Job Title Wisma Bella Swimming Pool Client Majlis Perbandaran Kuantan		P*Wind speed 32.5 m/s R# Fabric RS By TSM Date 17-Dec-11 Chk TSM P# Q326-KSP-R4b-Deg.ald Date/Tm 10-Jul-2012 16:43			
Steel Design (Track 0) Checks Cont. ALL UNITS ARE - IN METE (UNLESS OTHERWISE NOTED)					
MEMBER	TABLE	RESULT/ FX	CRITICAL COMP/ MY	MATIO/ W	LOADING/ LOCATION
1937 ST P31235.0	PAGE	88-4.7	(CI)	0.244	204
284.20 T		0.00		0.00	0.20
1938 ST P31235.0	PAGE	88-4.7	(CI)	0.320	204
122.20 C		0.00		0.00	0.16
1939 ST P31235.0	PAGE	88-4.7	(CI)	0.590	204
76.70 T		0.00		0.00	0.00
1940 ST P31235.0	PAGE	88-4.7	(CI)	0.448	204
164.70 C		0.00		0.00	1.20
1941 ST P31235.0	PAGE	88-4.7	(CI)	0.544	204
54.20 T		0.00		0.00	-
1942 ST P31235.0	PAGE	88-4.7	(CI)	0.240	204
264.20 T		0.00		0.40	0.00
1943 ST P31235.0	PAGE	88-4.7	(CI)	0.113	204
38.88 C		0.00		0.00	0.00
1944 ST P31235.0	PAGE	88-4.7	(CI)	0.437	204
145.37 C		0.00		0.00	1.20
1945 ST P31235.0	PAGE	88-4.7	(CI)	0.460	204
54.77 T		0.00		0.00	0.00
1946 ST P31235.0	PAGE	88-4.7	(CI)	0.240	204
284.77 T		0.00		0.00	0.00
1947 ST P31235.0	PAGE	88-4.7	(CI)	0.470	207
118.20 C		0.00		0.00	0.24
1948 ST P31235.0	PAGE	88-4.7	(CI)	0.599	204
139.70 C		0.00		0.00	3.20
1949 ST P31235.0	PAGE	88-4.7	(CI)	0.424	207
143.20 C		0.00		0.00	0.25
1950 ST P31235.0	PAGE	88-4.7	(CI)	0.460	204
411.85 C		0.00		0.00	0.16
1951 ST P31235.0	PAGE	88-4.7	(CI)	0.444	207
107.35 C		0.00		0.00	10.24
1952 ST P31235.0	PAGE	88-4.7	(CI)	0.473	204
147.31 C		0.00		0.00	0.00
1953 ST P31235.0	PAGE	88-4.7	(CI)	0.478	204
164.20 C		0.00			

 Subsea Seacoast to Tensarac Pte Ltd Job Title: Wisma Bella Swimming Pool Client: Majlis Perbandaran Kuantan	Job No TP140581	Sheet No a 192	Rev R4b-FAB2
	PWind speed 32.5 m/s Ref Fabric RS By TSM Date 09/17-Dec-11 DateTime 10-Jul-2012 16:43		

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MM UNLESS OTHERWISE NOTED


MEMBER	TABLE	RESULT / PER	CRITICAL COMB / FX	MAYIS/ MT	LOADING / LOCATION
2647 ST PIP1644.0	PAGE	BS-4.7 (C)	0.107	258	
103.28 C		-1.89	0.00	0.00	
2648 ST PIP1644.0	PAGE	BS-4.7 (C)	0.207	264	
103.28 C		-4.23	0.00	0.00	
2649 ST PIP1644.0	PAGE	BS-4.7 (C)	0.155	262	
103.28 C		-4.60	0.00	0.00	
2650 ST PIP1644.0	PAGE	BS-4.7 (C)	0.137	260	
103.28 C		-4.13	0.00	0.00	
2651 ST PIP1644.0	PAGE	BS-4.7 (C)	0.124	259	
103.28 C		-4.14	0.00	0.00	
2652 ST PIP1644.0	PAGE	ANNEX 1.1	0.392	264	
89.60 C		-2.82	0.00	0.00	
2653 ST PIP1644.0	PAGE	BS-4.7 (C)	0.305	258	
103.28 C		-2.22	0.00	0.00	
2654 ST PIP1644.0	PAGE	BS-4.7 (C)	0.138	260	
103.28 C		-4.23	0.00	0.00	
2655 ST PIP1644.0	PAGE	BS-4.7 (C)	0.185	268	
174.28 C		-1.88	0.00	0.00	
2656 ST PIP1644.0	PAGE	BS-4.7 (C)	0.166	268	
89.23 C		-4.60	0.00	0.00	
2657 ST PIP1644.0	PAGE	BS-4.7 (C)	0.246	268	
103.28 C		-2.22	0.00	0.00	
2658 ST PIP1644.0	PAGE	BS-4.7 (C)	0.200	268	
103.28 C		-2.22	0.00	0.00	
2659 ST PIP1644.0	PAGE	ANNEX 1.1	0.295	258	
103.28 C		-2.89	0.00	0.00	
2660 ST PIP1644.0	PAGE	BS-4.7 (C)	0.230	268	
103.28 C		-4.23	0.00	0.00	
2661 ST PIP1644.0	PAGE	BS-4.7 (C)	0.160	268	
103.28 C		-4.23	0.00	0.00	
2662 ST CHS2189.0	PAGE	BS-4.7 (C)	0.260	262	
141.68 C		0.00	0.00	12.85	
2663 ST CHS2189.0	PAGE	BS-4.7 (C)	0.297	262	
149.28 C		0.00	0.00	13.85	
2664 ST CHS2189.0	PAGE	BS-4.7 (C)	0.332	262	
159.28 C		0.00	0.00	15.00	
2665 ST CHS2189.0	PAGE	BS-4.7 (C)	0.368	262	
171.28 C		0.00	0.00	16.45	
2666 ST CHS2189.0	PAGE	BS-4.7 (C)	0.405	262	
184.28 C		0.00	0.00	18.10	
2667 ST CHS2189.0	PAGE	BS-4.7 (C)	0.443	262	
200.28 C		0.00	0.00	20.00	
2668 ST CHS2189.0	PAGE	BS-4.7 (C)	0.482	262	
218.28 C		0.00	0.00	22.15	
2669 ST CHS2189.0	PAGE	BS-4.7 (C)	0.522	262	
238.28 C		0.00	0.00	24.55	
2670 ST CHS2189.0	PAGE	BS-4.7 (C)	0.563	262	
259.28 C		0.00	0.00	27.20	

 Subsea Seacoast to Tensarac Pte Ltd Job Title: Wisma Bella Swimming Pool Client: Majlis Perbandaran Kuantan	Job No TP140581	Sheet No a 193	Rev R4b-FAB2
	PWind speed 32.5 m/s Ref Fabric RS By TSM Date 09/17-Dec-11 DateTime 10-Jul-2012 16:43		

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MM UNLESS OTHERWISE NOTED


MEMBER	TABLE	RESULT / PER	CRITICAL COMB / FX	MAYIS/ MT	LOADING / LOCATION
2671 ST CHS2189.0	PAGE	BS-4.7 (C)	0.238	262	
171.28 C		0.00	0.00	15.65	
2672 ST CHS2189.0	PAGE	BS-4.7 (C)	0.278	262	
187.28 C		-1.64	0.00	18.20	
2673 ST CHS2189.0	PAGE	BS-4.7 (C)	0.319	262	
205.28 C		0.00	0.00	21.00	
2674 ST CHS2189.0	PAGE	BS-4.7 (C)	0.361	262	
225.28 C		0.00	0.00	24.15	
2675 ST CHS2189.0	PAGE	BS-4.7 (C)	0.405	262	
246.28 C		0.00	0.00	27.65	
2676 ST CHS2189.0	PAGE	BS-4.7 (C)	0.450	262	
268.28 C		0.00	0.00	31.50	
2677 ST CHS2189.0	PAGE	BS-4.7 (C)	0.497	262	
291.28 C		0.00	0.00	35.75	
2678 ST PIP1644.0	PAGE	BS-4.7 (C)	0.245	262	
103.28 C		-4.23	0.00	13.85	
2679 ST PIP1644.0	PAGE	BS-4.7 (C)	0.285	262	
113.28 C		-4.23	0.00	15.65	
2680 ST PIP1644.0	PAGE	BS-4.7 (C)	0.326	262	
123.28 C		-4.23	0.00	17.65	
2681 ST PIP1644.0	PAGE	BS-4.7 (C)	0.368	262	
133.28 C		-4.23	0.00	19.90	
2682 ST PIP1644.0	PAGE	BS-4.7 (C)	0.412	262	
143.28 C		-4.23	0.00	22.35	
2683 ST PIP1644.0	PAGE	BS-4.7 (C)	0.458	262	
153.28 C		-4.23	0.00	25.00	
2684 ST PIP1644.0	PAGE	BS-4.7 (C)	0.505	262	
163.28 C		-4.23	0.00	27.85	
2685 ST PIP1644.0	PAGE	BS-4.7 (C)	0.554	262	
173.28 C		-4.23	0.00	30.95	
2686 ST PIP1644.0	PAGE	BS-4.7 (C)	0.605	262	
183.28 C		-4.23	0.00	34.35	
2687 ST PIP1644.0	PAGE	BS-4.7 (C)	0.658	262	
193.28 C		-4.23	0.00	38.05	
2688 ST PIP1644.0	PAGE	BS-4.7 (C)	0.714	262	
203.28 C		-4.23	0.00	42.05	
2689 ST PIP1644.0	PAGE	BS-4.7 (C)	0.772	262	
213.28 C		-4.23	0.00	46.35	
2690 ST PIP1644.0	PAGE	BS-4.7 (C)	0.833	262	
223.28 C		-4.23	0.00	51.35	

 Subsea Seacoast to Tensarac Pte Ltd Job Title: Wisma Bella Swimming Pool Client: Majlis Perbandaran Kuantan	Job No TP140581	Sheet No a 194	Rev R4b-FAB2
	PWind speed 32.5 m/s Ref Fabric RS By TSM Date 09/17-Dec-11 DateTime 10-Jul-2012 16:43		

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	RESULT / PER	CRITICAL COMB / FX	MAYIS/ MT	LOADING / LOCATION
2691 ST PIP1644.0	PAGE	BS-4.7 (C)	0.242	262	
103.28 C		-4.23	0.00	13.85	
2692 ST PIP1644.0	PAGE	BS-4.7 (C)	0.282	262	
113.28 C		-4.23	0.00	15.65	
2693 ST PIP1644.0	PAGE	ANNEX 1.1	0.418	262	
147.28 C		-1.84	0.00	18.20	
2694 ST PIP1644.0	PAGE	ANNEX 1.1	0.464	262	
157.28 C		-1.84	0.00	21.00	
2695 ST PIP1644.0	PAGE	BS-4.7 (C)	0.510	262	
167.28 C		-1.84	0.00	24.15	
2696 ST PIP1644.0	PAGE	BS-4.7 (C)	0.558	262	
177.28 C		-1.84	0.00	27.65	
2697 ST PIP1644.0	PAGE	BS-4.7 (C)	0.607	262	
187.28 C		-1.84	0.00	31.50	
2698 ST PIP1644.0	PAGE	BS-4.7 (C)	0.657	262	
197.28 C		-1.84	0.00	35.75	
2699 ST PIP1644.0	PAGE	BS-4.7 (C)	0.708	262	
207.28 C		-1.84	0.00	40.35	
2700 ST PIP1644.0	PAGE	BS-4.7 (C)	0.761	262	
217.28 C		-1.84	0.00	45.35	
2701 ST PIP1644.0	PAGE	BS-4.7 (C)	0.816	262	
227.28 C		-1.84	0.00	50.75	
2702 ST PIP1644.0	PAGE	BS-4.7 (C)	0.873	262	
237.28 C		-1.84	0.00	56.75	
2703 ST PIP1644.0	PAGE	BS-4.7 (C)	0.932	262	
247.28 C		-1.84	0.00	63.45	
2704 ST PIP1644.0	PAGE	BS-4.7 (C)	0.993	262	
257.28 C		-1.84	0.00	70.95	
2705 ST PIP1644.0	PAGE	BS-4.7 (C)	1.057	262	
267.28 C		-1.84	0.00	79.35	
2706 ST PIP1644.0	PAGE	BS-4.7 (C)	1.124	262	
277.28 C		-1.84	0.00	88.65	
2707 ST PIP1644.0	PAGE	BS-4.7 (C)	1.194	262	
287.28 C		-1.84	0.00	98.95	
2708 ST PIP1644.0	PAGE	BS-4.7 (C)	1.267	262	
297.28 C		-1.84	0.00	110.25	
2709 ST PIP1644.0	PAGE	BS-4.7 (C)	1.343	262	
307.28 C		-1.84	0.00	122.65	
2710 ST PIP1644.0	PAGE	BS-4.7 (C)	1.422	262	
317.28 C		-1.84	0.00	136.25	
2711 ST PIP1644.0	PAGE	BS-4.7 (C)	1.504	262	
327.28 C		-1.84	0.00	151.15	
2712 ST PIP1644.0	PAGE	BS-4.7 (C)	1.590	262	
337.28 C		-1.84	0.00	167.45	
2713 ST PIP1644.0	PAGE	BS-4.7 (C)	1.681	262	
347.28 C		-1.84	0.00	185.25	
2714 ST PIP1644.0	PAGE	BS-4.7 (C)	1.777	262	
357.28 C		-1.84	0.00	204.65	
2715 ST PIP1644.0	PAGE	BS-4.7 (C)	1.878	262	
367.28 C		-1.84	0.00	225.75	
2716 ST PIP1644.0	PAGE	BS-4.7 (C)	1.984	262	
377.28 C		-1.84	0.00	248.65	
2717 ST PIP1644.0	PAGE	BS-4.7 (C)	2.095	262	
387.28 C		-1.84	0.00	273.45	
2718 ST PIP1644.0	PAGE	BS-4.7 (C)	2.213	262	
397.28 C		-1.84	0.00	300.25	
2719 ST PIP1644.0	PAGE	BS-4.7 (C)	2.337	262	
407.28 C		-1.84	0.00	329.15	
2720 ST PIP1644.0	PAGE	BS-4.7 (C)	2.468	262	
417.28 C		-1.84	0.00	360.35	
2721 ST PIP1644.0	PAGE	BS-4.7 (C)	2.606	262	
427.28 C		-1.84	0.00	393.95	

 Subsea Seacoast to Tensarac Pte Ltd Job Title: Wisma Bella Swimming Pool Client: Majlis Perbandaran Kuantan	Job No TP140581	Sheet No a 195	Rev R4b-FAB2
	PWind speed 32.5 m/s Ref Fabric RS By TSM Date 09/17-Dec-11 DateTime 10-Jul-2012 16:43		

Steel Design (Track 0) Checks Cont...

ALL UNITS ARE - MM UNLESS OTHERWISE NOTED

MEMBER	TABLE	RESULT / PER	CRITICAL COMB / FX	MAYIS/ MT	LOADING / LOCATION
2722 ST PIP1644.0	PAGE	BS-4.7 (C)	0.234	12	
149.28 C		-2.32	0.00	0.00	
2723 ST PIP1644.0	PAGE	BS-4.7 (C)	0.274	12	
159.28 C		-2.32	0.00	0.00	
2724 ST PIP1644.0	PAGE	BS-4.7 (C)	0.314	12	
169.28 C		-2.32	0.00	0.00	
2725 ST PIP1644.0	PAGE	BS-4.7 (C)	0.354	12	
179.28 C		-2.32	0.00	0.00	
2726 ST PIP1644.0	PAGE	BS-4.7 (C)	0.394	12	
189.28 C		-2.32	0.00	0.00	
2727 ST PIP1644.0	PAGE	BS-4.7 (C)	0.434	12	
199.28 C		-2.32	0.00	0.00	
2728 ST PIP1644.0	PAGE	BS-4.7 (C)	0.474	12	
209.28 C					

**APPENDIX B
FABRIC OUTPUT DATAS**

B1. EDGE PANEL NEXT TO DIVING POOL
FABRIC NODE NUMBER LAYOUT PLAN
- PRESTRESS LOAD CASE b1 - b4
- LIVE LOAD CASE b5 - b7
- WIND UPLIFT b8 - b10
- WIND PRESSURE b11 - b13
- WIND FROM ENTRANCE b14 - b16
- WIND FROM AUDIENCE STAND b17 - b19

B2. INTERNAL PANEL
FABRIC NODE NUMBER LAYOUT PLAN
- PRESTRESS LOAD CASE b20 - b23
- LIVE LOAD CASE b24 - b26
- WIND UPLIFT b27 - b29
- WIND PRESSURE b30 - b32
- WIND FROM ENTRANCE b33 - b35
- WIND FROM AUDIENCE STAND b36 - b38

B3. EDGE PANEL NEXT TO SCORE BOARD
FABRIC NODE NUMBER LAYOUT PLAN
- PRESTRESS LOAD CASE b39 - b42
- LIVE LOAD CASE b43 - b45
- WIND UPLIFT b46 - b48
- WIND PRESSURE b49 - b51
- WIND FROM ENTRANCE b52 - b54
- WIND FROM AUDIENCE STAND b55 - b57

Q326-Kuantan

Node No.	X-coordinate	Y-coordinate	Z-coordinate	U	V	W
9000001	-5.2329	4.6914	13.2514	0.0000	0.0000	0.0000
9000002	-4.8669	3.2914	14.2104	0.0000	0.0000	0.0000
9000003	-7.1348	11.6252	15.1797	0.0000	0.0000	0.0000
9000004	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000005	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000006	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000007	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000008	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000009	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000010	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000011	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000012	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000013	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000014	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000015	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000016	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000017	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000018	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000019	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000020	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000

Statik: Version 8.01 Done

b4

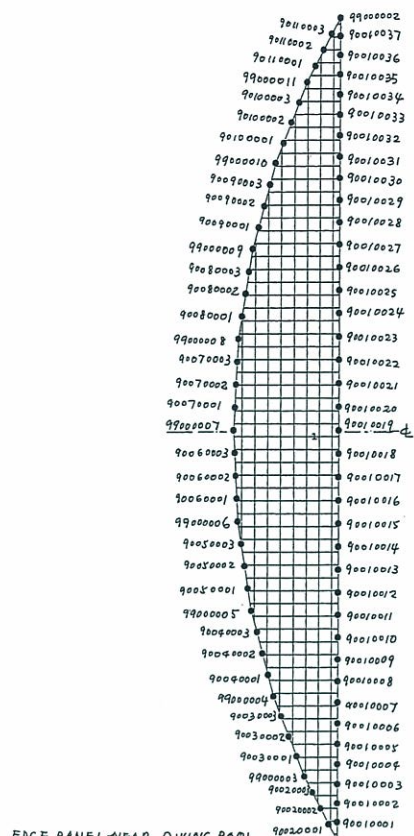
EDGE PANEL NEAR DIVING POOL - PRESTRESS

Warning! (051) Using default value: NR0B=0
Statik: Version 8.01 Done
Result from EASY Statistical analysis
Date = 12/21/2011 Time = 16:17:27
Values from IN-file
List for conjugate gradient
Minimum stiffness of a point
Maximum stiffness of a point
Maximum number of outer iterations
Maximum number of inner iterations
Kind of calculation

Line from EIB-file:
Statik: Statistical analysis...
Dimensions..... (MAX) 576 20000
Number of free points..... 498
Number of fully fixed points..... 78
Number of cable links..... 860
Number of links controlled by Hookes law..... 860
Number of links controlled by force density..... 142
Limit for convergence..... 20
Maximal number of iterations..... 0.1000E+00
Conjugate gradient.....

b5

Statik calculation with loads
Information to solve equations with the method of conjugate gradient
Number of inner iterations
0 201 0.000E+00 residual right side
1 201 0.754E-06 0.430E+01
2 201 0.182E-11 0.390E+02
3 110 400 0.268E-07 0.106E+00



EDGE PANEL NEAR DIVING POOL FABRIC NODE NUMBER LAYOUT

b1

b5

Statik: Statistical analysis...
Results from calculation of equilibrium
Date = 12/21/2011 Time = 16:17:28
Conjugate gradient..... 20
Maximum number of iterations..... 0.1000E+00
Conjugate gradient.....

b6

EDGE PANEL NEAR DIVING POOL - LIVE LOAD

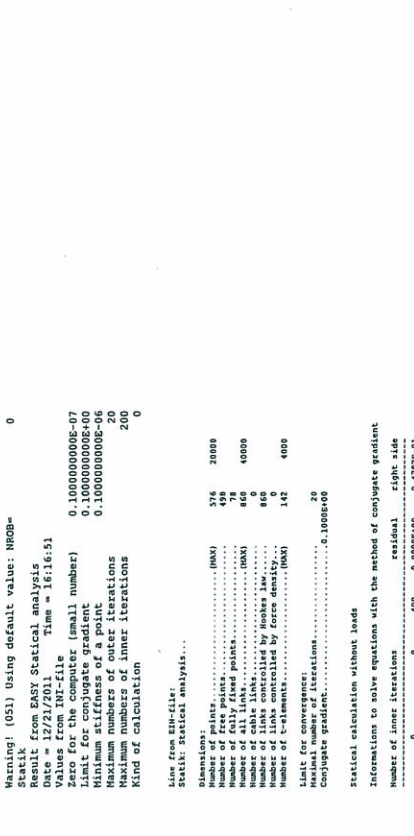
Node No.	X-coordinate	Y-coordinate	Z-coordinate	U	V	W
9000001	-5.2329	4.6914	13.2514	0.0000	0.0000	0.0000
9000002	-4.8669	3.2914	14.2104	0.0000	0.0000	0.0000
9000003	-7.1348	11.6252	15.1797	0.0000	0.0000	0.0000
9000004	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000005	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000006	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000007	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000008	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000009	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000010	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000011	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000012	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000013	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000014	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000015	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000016	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000017	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000018	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000019	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000020	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000

Statik: Version 8.01 Done

b1

b5

EDGE PANEL NEAR DIVING POOL - LIVE LOAD



EDGE PANEL NEAR DIVING POOL - PRESTRESS

Node No.	X-coordinate	Y-coordinate	Z-coordinate	U	V	W
9000001	-5.2329	4.6914	13.2514	0.0000	0.0000	0.0000
9000002	-4.8669	3.2914	14.2104	0.0000	0.0000	0.0000
9000003	-7.1348	11.6252	15.1797	0.0000	0.0000	0.0000
9000004	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000005	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000006	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000007	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000008	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000009	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000010	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000011	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000012	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000013	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000014	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000015	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000016	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000017	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000018	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000019	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000020	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000

Statik: Version 8.01 Done

b2

b6

EDGE PANEL NEAR DIVING POOL - LIVE LOAD

Node No.	X-coordinate	Y-coordinate	Z-coordinate	U	V	W
9000001	-5.2329	4.6914	13.2514	0.0000	0.0000	0.0000
9000002	-4.8669	3.2914	14.2104	0.0000	0.0000	0.0000
9000003	-7.1348	11.6252	15.1797	0.0000	0.0000	0.0000
9000004	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000005	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000006	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000007	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000008	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000009	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000010	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000011	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000012	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000013	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000014	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000015	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000016	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000017	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000018	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000019	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000020	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000

EDGE PANEL NEAR DIVING POOL - PRESTRESS

b2

b6

EDGE PANEL NEAR DIVING POOL - LIVE LOAD

Node No.	X-coordinate	Y-coordinate	Z-coordinate	U	V	W
9000001	-5.2329	4.6914	13.2514	0.0000	0.0000	0.0000
9000002	-4.8669	3.2914	14.2104	0.0000	0.0000	0.0000
9000003	-7.1348	11.6252	15.1797	0.0000	0.0000	0.0000
9000004	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000005	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000006	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000007	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000008	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000009	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000010	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000011	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000012	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000013	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000014	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000015	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000016	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000017	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000018	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000019	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000020	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000

Statik: Version 8.01 Done

b3

b7

EDGE PANEL NEAR DIVING POOL - LIVE LOAD

Node No.	X-coordinate	Y-coordinate	Z-coordinate	U	V	W
9000001	-5.2329	4.6914	13.2514	0.0000	0.0000	0.0000
9000002	-4.8669	3.2914	14.2104	0.0000	0.0000	0.0000
9000003	-7.1348	11.6252	15.1797	0.0000	0.0000	0.0000
9000004	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000005	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000006	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000007	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000008	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000009	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000010	-4.1881	14.4127	15.2416	0.0000	0.0000	0.0000
9000011						

616

Node	U	V	W
9000001	-0.4500	27.3745	10.1434
9000002	-1.4930	-3.7908	9.4312
9000003	-2.7751	-1.2589	10.8916
9000004	-4.2620	1.3238	12.1337
9000005	-5.2319	4.6914	13.2814
9000006	-6.0982	8.3935	14.7486
9000007	-7.1454	13.4722	16.2827
9000008	-8.1811	18.4327	18.1266
9000009	-9.2173	23.2973	19.7822
9000010	-10.2538	28.0716	21.1211
9000011	-11.2910	32.7529	22.1622
9000012	-12.3291	37.3399	22.9253
9000013	-13.3682	41.8335	23.4312
9000014	-14.4084	46.2358	23.7997
9000015	-15.4498	50.5500	24.0508
9000016	-16.4926	54.7801	24.1945
9000017	-17.5369	58.9301	24.2399
9000018	-18.5829	62.9964	24.1971
9000019	-19.6307	66.9764	24.0761
9000020	-20.6805	70.8675	23.8772
9000021	-21.7324	74.6684	23.6013
9000022	-22.7865	78.3790	23.2493
9000023	-23.8428	81.9994	22.8221
9000024	-24.9014	85.5308	22.3205
9000025	-25.9623	88.9736	21.7453
9000026	-27.0256	92.3294	21.0984
9000027	-28.0923	95.5998	20.3826
9000028	-29.1625	98.7864	19.5997
9000029	-30.2362	101.8909	18.7524
9000030	-31.3135	104.9151	17.8434
9000031	-32.3944	107.8611	16.8764
9000032	-33.4790	110.7308	15.8552
9000033	-34.5674	113.5272	14.7836
9000034	-35.6597	116.2535	13.6664
9000035	-36.7560	118.9129	12.5084
9000036	-37.8573	121.5097	11.3143
9000037	-38.9636	124.0484	10.0890
9000038	-40.0759	126.5337	8.8384
9000039	-41.1943	128.9705	7.5684
9000040	-42.3188	131.3639	6.2840
9000041	-43.4494	133.7191	5.0000
9000042	-44.5862	136.0414	3.7313
9000043	-45.7293	138.3361	2.4838
9000044	-46.8787	140.6087	1.2635
9000045	-48.0344	142.8651	0.0750
9000046	-49.1964	145.1019	-0.1676
9000047	-50.3647	147.3249	-0.4161
9000048	-51.5393	149.5301	-0.6700
9000049	-52.7203	151.7140	-0.9288
9000050	-53.9077	153.8744	-1.1921
9000051	-55.1016	156.0191	-1.4595
9000052	-56.3020	158.1461	-1.7307
9000053	-57.5089	160.2544	-2.0054
9000054	-58.7223	162.3431	-2.2833
9000055	-59.9422	164.4115	-2.5642
9000056	-61.1686	166.4590	-2.8480
9000057	-62.4015	168.4851	-3.1345
9000058	-63.6409	170.4896	-3.4235
9000059	-64.8868	172.4724	-3.7149
9000060	-66.1392	174.4345	-4.0087
9000061	-67.3981	176.3759	-4.3049
9000062	-68.6635	178.2969	-4.6034
9000063	-69.9354	180.1987	-4.9042
9000064	-71.2138	182.0828	-5.2073
9000065	-72.4987	183.9507	-5.5127
9000066	-73.7901	185.8040	-5.8203
9000067	-75.0880	187.6442	-6.1299
9000068	-76.3924	189.4729	-6.4416
9000069	-77.7033	191.2919	-6.7553
9000070	-79.0207	193.1028	-7.0711
9000071	-80.3446	194.9074	-7.3889
9000072	-81.6750	196.7075	-7.7087
9000073	-83.0219	198.5040	-8.0305
9000074	-84.3753	200.2979	-8.3542
9000075	-85.7352	202.0902	-8.6799
9000076	-87.1016	203.8820	-9.0075
9000077	-88.4745	205.6744	-9.3370
9000078	-89.8539	207.4675	-9.6683
9000079	-91.2407	209.2624	-10.0014
9000080	-92.6349	211.0601	-10.3372
9000081	-94.0365	212.8607	-10.6756
9000082	-95.4455	214.6643	-11.0165
9000083	-96.8620	216.4719	-11.3598
9000084	-98.2860	218.2837	-11.7055
9000085	-99.7174	220.0998	-12.0536
9000086	-101.1563	221.9213	-12.4041
9000087	-102.6027	223.7484	-12.7570
9000088	-104.0566	225.5813	-13.1124
9000089	-105.5180	227.4212	-13.4702
9000090	-106.9869	229.2694	-13.8305
9000091	-108.4633	231.1271	-14.1933
9000092	-109.9472	232.9946	-14.5585
9000093	-111.4386	234.8722	-14.9261
9000094	-112.9375	236.7603	-15.2961
9000095	-114.4439	238.6592	-15.6685
9000096	-115.9577	240.5694	-16.0433
9000097	-117.4790	242.4913	-16.4205
9000098	-118.9977	244.4254	-16.7999
9000099	-120.5239	246.3721	-17.1816
9000100	-122.0575	248.3319	-17.5656
9000101	-123.5986	250.3053	-17.9519
9000102	-125.1472	252.2928	-18.3404
9000103	-126.7033	254.2949	-18.7311
9000104	-128.2669	256.3121	-19.1241
9000105	-129.8381	258.3449	-19.5193
9000106	-131.4168	260.3929	-19.9167
9000107	-133.0031	262.4566	-20.3163
9000108	-134.5970	264.5366	-20.7181
9000109	-136.1985	266.6325	-21.1221
9000110	-137.8076	268.7449	-21.5283
9000111	-139.4243	270.8734	-21.9367
9000112	-141.0486	273.0186	-22.3473
9000113	-142.6805	275.1811	-22.7601
9000114	-144.3200	277.3607	-23.1751
9000115	-145.9671	279.5580	-23.5923
9000116	-147.6218	281.7737	-24.0117
9000117	-149.2841	283.9976	-24.4333
9000118	-150.9540	286.2404	-24.8571
9000119	-152.6414	288.5029	-25.2831
9000120	-154.3464	290.7858	-25.7113
9000121	-156.0689	293.0900	-26.1417
9000122	-157.8090	295.4164	-26.5743
9000123	-159.5667	297.7649	-27.0091
9000124	-161.3420	300.1364	-27.4460
9000125	-163.1349	302.5310	-27.8850
9000126	-164.9454	304.9496	-28.3261
9000127	-166.7735	307.3923	-28.7693
9000128	-168.6192	309.8600	-29.2146
9000129	-170.4825	312.3538	-29.6620
9000130	-172.3634	314.8747	-30.1115
9000131	-174.2618	317.4238	-30.5631
9000132	-176.1777	319.9921	-31.0167
9000133	-178.1111	322.5808	-31.4724
9000134	-180.0620	325.1911	-31.9301
9000135	-182.0304	327.8242	-32.3899
9000136	-184.0164	330.4903	-32.8518
9000137	-186.0200	333.1807	-33.3157
9000138	-188.0412	335.8968	-33.7817
9000139	-190.0799	338.6400	-34.2497
9000140	-192.1363	341.4125	-34.7197
9000141	-194.2104	344.2157	-35.1918
9000142	-196.3022	347.0500	-35.6659
9000143	-198.4118	349.9167	-36.1421
9000144	-200.5392	352.8163	-36.6204
9000145	-202.6844	355.7503	-37.1008
9000146	-204.8474	358.7202	-37.5833
9000147	-207.0283	361.7276	-38.0678
9000148	-209.2271	364.7740	-38.5543
9000149	-211.4439	367.8599	-39.0428
9000150	-213.6787	370.9869	-39.5333
9000151	-215.9315	374.1566	-40.0258
9000152	-218.2024	377.3707	-40.5203
9000153	-220.4914	380.6309	-41.0168
9000154	-222.8085	383.9388	-41.5153
9000155	-225.1438	387.2960	-42.0158
9000156	-227.5073	390.7043	-42.5183
9000157	-229.8990	394.1655	-43.0228
9000158	-232.3189	397.6814	-43.5293
9000159	-234.7671	401.2537	-44.0378
9000160	-237.2436	404.8842	-44.5483
9000161	-239.7485	408.5747	-45.0608
9000162	-242.2819	412.3271	-45.5753
9000163	-244.8438	416.1434	-46.0918
9000164	-247.4343	420.0264	-46.6103
9000165	-250.0534	423.9789	-47.1308
9000166	-252.7011	429.0038	-47.6533
9000167	-255.3774	434.1041	-48.1778
9000168	-258.0824	439.2828	-48.7043
9000169	-260.8162	444.5429	-49.2328
9000170	-263.5789	449.8874	-49.7633
9000171	-266.3706	455.3193	-50.2958
9000172	-269.1914	460.8407	-50.8303
9000173	-272.0414	466.4547	-51.3668
9000174	-274.9207	472.1643	-51.9053
9000175	-277.8294	477.9726	-52.4458
9000176	-280.7677	483.8828	-52.9883
9000177	-283.7357	489.8970	-53.5328
9000178	-286.7334	496.0184	-54.0793
9000179	-289.7609	502.2491	-54.6278
9000180	-292.8183	508.5922	-55.1783
9000181	-295.9057	515.0508	-55.7308
9000182	-299.0232	521.6281	-56.2853
9000183	-302.1708	528.3273	-56.8418
9000184	-305.3486	535.1516	-57.3993
9000185	-308.5567	542.0044	-57.9578
9000186	-311.7951	548.9890	-58.5173
9000187	-315.0640	556.0087	-59.0788
9000188	-318.3634	563.1668	-59.6413
9000189	-321.6934	570.4677	-60.2048
9000190	-325.0540	577.9149	-60.7693
9000191	-328.4453	585.5119	-61.3348
9000192	-331.8674	593.2622	-61.9013
9000193	-335.3204	601.1694	-62.4688
9000194	-338.8043	609.2371	-63.0373
9000195	-342.3192	617.4689	-63.6068
9000196	-345.8651	625.8684	-64.1773
9000197	-349.4420	634.4394	-64.7488
9000198	-353.0500	643.1855	-65.3213
9000199	-356.6891	652.1114	-65.8948
9000200	-360.3594	661.2210	-66.4693
9000201	-364.0610	670.5190	-67.0448
9000202	-367.7940	680.0094	-67.6213
9000203	-371.5584	689.6964	-68.1988
9000204	-375.3543	699.5842	-68.7773
9000205	-379.1818	709.6772	-69.3568
9000206	-383.0409	719.9809	-69.9373
9000207	-386.9318	730.4999	-70.5188
9000208	-390.8546	741.2390	-71.1013
9000209	-394.8094	752.1930	-71.6848
9000210	-398.7963	763.3671	-72.2693
9000211	-402.8154	774.7657	-72.8548
9000212	-406.8668	786.3938	-73.4413
9000213	-410.9506	798.2463	-74.0288
9000214	-415.0669	810.4284	-74.6173
9000215	-419.2158	822.9456	-75.2068
9000216	-423.3974	835.7933	-75.7973
9000217	-427.6118	848.9771	-76.3888
9000218	-431.8590	862.5026	-76.9813
9000219	-436.1392	876.3755	-77.5748
9000220	-440.4525	890.5914	-78.1693
9000221	-444.7990	905.1559	-78.7648
9000222	-449.1787	920.0747	-79.3613
9000223	-453.5917	935.3545	-79.9588
9000224	-458.0381	951.0011	-80.5573
9000225	-462.5181	967.0214	-81.1568
9000226	-4		

EDGE PANEL NEAR SCORE BOARD - WIND UPLIFT

Result: (S1) Using default value: WMO=0
Result from BAST Statistical analysis
Value from PDI-File Time = 11:31:55
Zero for the computer (small number) 0.10000000E-07
Minimum stiffness of a point 0.10000000E-06
Maximum number of inner iterations 200
Size of calculation 0

Table with columns: Nodes, Coordinates (X, Y, Z), Applied nodes, Residual forces. Contains data for nodes 1 through 142.

EDGE PANEL NEAR SCORE BOARD - WIND FROM ENTRANCE

Result: (S1) Using default value: WMO=0
Result from BAST Statistical analysis
Value from PDI-File Time = 11:31:50
Zero for the computer (small number) 0.10000000E-07
Minimum stiffness of a point 0.10000000E-06
Maximum number of inner iterations 200
Size of calculation 0

Table with columns: Nodes, Coordinates (X, Y, Z), Applied nodes, Residual forces. Contains data for nodes 1 through 142.

EDGE PANEL NEAR SCORE BOARD - WIND PRESSURE

Result: (S1) Using default value: WMO=0
Result from BAST Statistical analysis
Value from PDI-File Time = 11:31:55
Zero for the computer (small number) 0.10000000E-07
Minimum stiffness of a point 0.10000000E-06
Maximum number of inner iterations 200
Size of calculation 0

Table with columns: Nodes, Coordinates (X, Y, Z), Applied nodes, Residual forces. Contains data for nodes 1 through 142.

EDGE PANEL NEAR SCORE BOARD - WIND FROM ENTRANCE

Result: (S1) Using default value: WMO=0
Result from BAST Statistical analysis
Value from PDI-File Time = 11:31:46
Zero for the computer (small number) 0.10000000E-07
Minimum stiffness of a point 0.10000000E-06
Maximum number of inner iterations 200
Size of calculation 0

Table with columns: Nodes, Coordinates (X, Y, Z), Applied nodes, Residual forces. Contains data for nodes 1 through 142.

EDGE PANEL NEAR SCORE BOARD - WIND PRESSURE

Result: (S1) Using default value: WMO=0
Result from BAST Statistical analysis
Value from PDI-File Time = 11:31:56
Zero for the computer (small number) 0.10000000E-07
Minimum stiffness of a point 0.10000000E-06
Maximum number of inner iterations 200
Size of calculation 0

Table with columns: Nodes, Coordinates (X, Y, Z), Applied nodes, Residual forces. Contains data for nodes 1 through 142.

EDGE PANEL NEAR SCORE BOARD - WIND FROM ENTRANCE

Result: (S1) Using default value: WMO=0
Result from BAST Statistical analysis
Value from PDI-File Time = 11:31:46
Zero for the computer (small number) 0.10000000E-07
Minimum stiffness of a point 0.10000000E-06
Maximum number of inner iterations 200
Size of calculation 0

Table with columns: Nodes, Coordinates (X, Y, Z), Applied nodes, Residual forces. Contains data for nodes 1 through 142.

EDGE PANEL NEAR SCORE BOARD - WIND PRESSURE

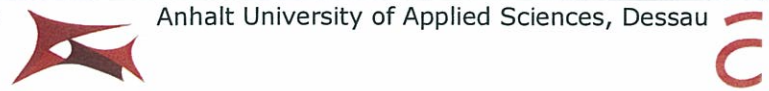
Result: (S1) Using default value: WMO=0
Result from BAST Statistical analysis
Value from PDI-File Time = 11:31:55
Zero for the computer (small number) 0.10000000E-07
Minimum stiffness of a point 0.10000000E-06
Maximum number of inner iterations 200
Size of calculation 0

Table with columns: Nodes, Coordinates (X, Y, Z), Applied nodes, Residual forces. Contains data for nodes 1 through 142.

EDGE PANEL NEAR SCORE BOARD - WIND FROM AUDIENCE STAND

Result: (S1) Using default value: WMO=0
Result from BAST Statistical analysis
Value from PDI-File Time = 11:31:46
Zero for the computer (small number) 0.10000000E-07
Minimum stiffness of a point 0.10000000E-06
Maximum number of inner iterations 200
Size of calculation 0

Table with columns: Nodes, Coordinates (X, Y, Z), Applied nodes, Residual forces. Contains data for nodes 1 through 142.



	Sediabera Sdn. Bhd. No. 11 Jalan Astaka U1/14, Seksyen U8 Bukit Jelutong 40150 Shah Alam Tel: (603)7847 3333 Fax: (603)7847 2222	Project No: TPL 40581 Date: 26 June 2011 Doc No: Q326-KSP-CAL-001 Rev 0	Page:
	Project: Upgrading of Aquatic Center Wisma Bala Isdera Mahkota, Kuantan Title: Swimming Pool Tensile Membrane Roof - Structural Analysis & Design		

APPENDIX C

TECHNICAL DATA

C1. CABLE	c1 - c2
C2. VERSEIDAG MEMBRANE PTFE B18089	c3 - c4

Q326-Kuantan

NANTONG WIRE ROPE (GROUP) CO., LTD.

MILL TEST CERTIFICATE

DATE: Oct. 27 2005

1. Manufacturer	NANTONG WIRE ROPE (GROUP) CO., LTD.
2. Ordering company	KENG WAH HARDWARE CO PTE LTD
3. S/C No.	KVNT-0504
4. Length of rope	300 M
5. Rope diameter	16 MM
6. Construction	1X19
7. Kind of core	
8. Surface of wire rope	Galv
9. Nominal tensile strength	1570 NMM2
10. Nominal breaking force	211.0 KN
11. Actual breaking force	215.5 KN
12. Type	R191L
13. Total weight	1.532 KGS
14. Amount of coil	1
15. State	DRY
16. Delivery date	Oct 28, 2005

The manufactured and delivered wire ropes of above indicated order correspond with the technical term of delivery according to BS 382.

CHEMICAL ANALYSIS OF WIRE ROD

Chemical composition (%)

C	Mn	S	P	Si
0.73	0.71	0.013	0.011	0.19



南通钢丝绳集团有限公司
NANTONG WIRE ROPE (GROUP) CO., LTD.

Manho Rope & Wire Ltd.

Registered by AMERICAN BUREAU OF SHIPPING LLOYD'S REGISTER OF SHIPPING

Manufacturers & Exporters
10A-1, WAKA WILUNG ROAD SUNGAI BUKAN, PERAK
P.O. BOX NO. 277 BUKAN
TELE: 05-8604041
HEAD OFFICE TEL: 330-3101 - SINGAPORE

Sheet No. 2007A-292-01-01
Date: SEP 30, 2007

MILL TEST CERTIFICATE

Customer: Messrs **KENG WAH HARDWARE CO PTE LTD**
Supplier: Messrs **MANHO ROPE & WIRE LTD.**

L/C No. _____ Order No. **MK2007-065**

Commodity: **PE COATED GALVANIZED STEEL WIRE ROPE**

Construction: **6X37 ZNRC** Grade: _____

Specification: **BS 382** Lubrication: _____

Order Quantity: **300** Reel No. **1**

Gross Weight: _____ Net Weight: **1092.50** Lbs/Kgs

TEST RESULT

Rope Dia	28X32 (Actual)	28X32	mm	Preforming	GOOD
Kind of Lay	RRRL		mm	Length of Lay	mm
Actual Breaking Strength of Wire Rope		51.300	Lbs/Kgs		
Nominal Dia. of Wire		mm			
Tensile Strength of Wires	Min	Max	MPa/Kg/mm ²		
Number of Torsion of Wires	Min	Max	Times		
Weight of Zinc Coating			g/m ² Oz/ft ²		

CHEMICAL ANALYSIS OF WIRE ROD

Heat No.	C	Si	Mn	P	S
66740	0.69	0.23	0.58	0.014	0.007

REMARKS: _____

Quality Control Dept.

MHS-B102-30 Manho Rope & Wire Ltd. (2007-200)

VERSEIDAG
COATING AND COMPOSITE

c3

B 18089

The reliable protection

duraskin®

c4

DE	Type III	B 18089
Trägergewebe		Glasfaser EC 3/4
Beschichtung		PTFE - Polytetrafluorethylen
Flächengewicht (g/m ²)	DIN EN ISO 22862	1150
Breite (cm)	DIN EN ISO 22861	470
Nichtdehnung (N/5 cm)	DIN 53354	7000/6000
Wahrerelast (N)	DIN 53363	500/500
Haftung (N/5 cm)	DIN 53357	80
Transparenz bei 550 nm (H)	DIN 5036	14
Brandverhalten	DIN 4102	B1

Note: Produkt ist nicht zu verbrennen, sondern mit Hitzefäden zu verschmelzen. Weitere Zertifikate erhältlich auf Anfrage. Änderungen, die dem technischen Fortschritt dienen, behalten wir uns vor. Wir übernehmen keine Haftung für Schäden an den Elementen mit einer Lebensdauer von 25 Jahren. Die Angaben entsprechen unserem heutigen Kenntnisstand und stellen keine Rechtsverbindlichkeit dar. Transparenz bezieht sich auf ausgeglichene Version.

UK	Type III	B 18089
Base fabric		Glass fibre EC 3/4
Coating		PTFE - polytetrafluoroethylene
Total weight (g/m ²)	DIN EN ISO 22862	1150
Width (cm)	DIN EN ISO 22861	470
Tensile strength (N/5 cm)	DIN 53354	warp/weft 7000/6000
Tear resistance (N)	DIN 53363	warp/weft 500/500
Adhesion (N/5 cm)	DIN 53357	80
Transparency at 550 nm (H)	DIN 5036	14
Flame retardancy	DIN 4102	B1

Note: Product must not be seen, but better welded. Additional certificates available on request. Subject to change regarding technical updates. Values indicated unless otherwise stated are nominal values with a tolerance range of ± 5%. All data presented here is given to the best of our current knowledge for guidance purposes and is not legally binding. Transparency refers to bleached version.

F	Type III	B 18089
Tissu support		Fibre de verre EC 3/4
Enduction de base		PTFE - Polytetrafluorethylene
Poids total (g/m ²)	DIN EN ISO 22862	1150
Longueur (cm)	DIN EN ISO 22861	470
Résistance à la rupture (N/5 cm)	DIN 53354	chaîne/trame 7000/6000
Résistance à la déchirure (N)	DIN 53363	chaîne/trame 500/500
Adhérence (N/5 cm)	DIN 53357	80
Transparence à 550 nm (H)	DIN 5036	14
Réaction au feu	DIN 4102	B1

Note: Le produit ne doit pas être vu, mais mieux soudé. D'autres certificats sont disponibles sur demande. Sous réserve de toutes modifications dans le cadre d'actualisations techniques. Les valeurs mentionnées sans précision sont des valeurs nominales avec une tolérance de ± 5%. Les données correspondantes à notre savoir actuel et sans obligation légale. La transparence se rapporte à la version blanche.

ESP	Type III	B 18089
Tejido base		Fibra de vidrio EC 3/4
Revestimiento		PTFE - Politetrafluoretileno
Peso total (g/m ²)	DIN EN ISO 22862	1150
Ancho (cm)	DIN EN ISO 22861	470
Resistencia a la rotura (N/5 cm)	DIN 53354	urdimbre/trama 7000/6000
Resistencia al desgarro (N)	DIN 53363	urdimbre/trama 500/500
Adherencia (N/5 cm)	DIN 53357	80
Transparencia en 550 nm (H)	DIN 5036	14
Ignifugación	DIN 4102	B1

Note: El producto no debe ser visto, sino soldado con buena calidad. Otros certificados obtenibles previa petición. Reservados el derecho a realizar modificaciones técnicas de actualización. Los valores de datos de información técnica y valores nominales con una tolerancia de ± 5%. Los datos se corresponden con nuestro estado actual de conocimiento y su finalidad es informativa sin vinculación legal. La transparencia hace referencia a la versión blanca.

The reliable protection